

DERUN LI

(1)

NOV. 6, 2000

Be window issues;

RF Heating on Be windows

$$\langle P \rangle = \frac{R_s}{2} \eta \left(\frac{\epsilon_0}{\mu_0} \right) E_0^2 \oint_S J_1^2(kr) ds$$

$\eta \sim$ duty factor

$E_0 \sim$ peak electric field
(pillbox model)

$$k = \frac{\omega}{c} = \frac{\mu_{01}}{a}$$

$\nearrow$
radius of pillbox cavity

Linear approximation,

$$\langle P \rangle = \oint_S \alpha r^2 ds$$

(2)

Nov. 6, 2000

$$\frac{dQ}{dt} = -\kappa A \frac{dT}{dr}$$

$\kappa = 200 \text{ W/mK}$ for Be at room temperature

$A \sim$ cross area

Temperature distribution,

$$T(r) = T(0) - \frac{\langle P \rangle}{8\pi\kappa d} \left(\frac{r}{R}\right)^4$$

$$\Delta T = \frac{\langle P \rangle}{8\pi\kappa d}$$

$d \sim$ thickness of a flat window

How to keep $T(0)$ low:

$\langle P \rangle \downarrow, \kappa \uparrow$

$d \uparrow$

(3)

Nov. 6, 2000

Numerical simulation shows,
foil deflection $\propto \Delta T$

Experiments conducted on a 805 MHz
Be window (8 cm radius, 5 mill
thick and pre-stressed)

$$F_{\text{lat}} < 40^\circ \text{K} = \Delta T$$



Thicker & stiffer windows

→ flat
→ tapered
→ step } windows



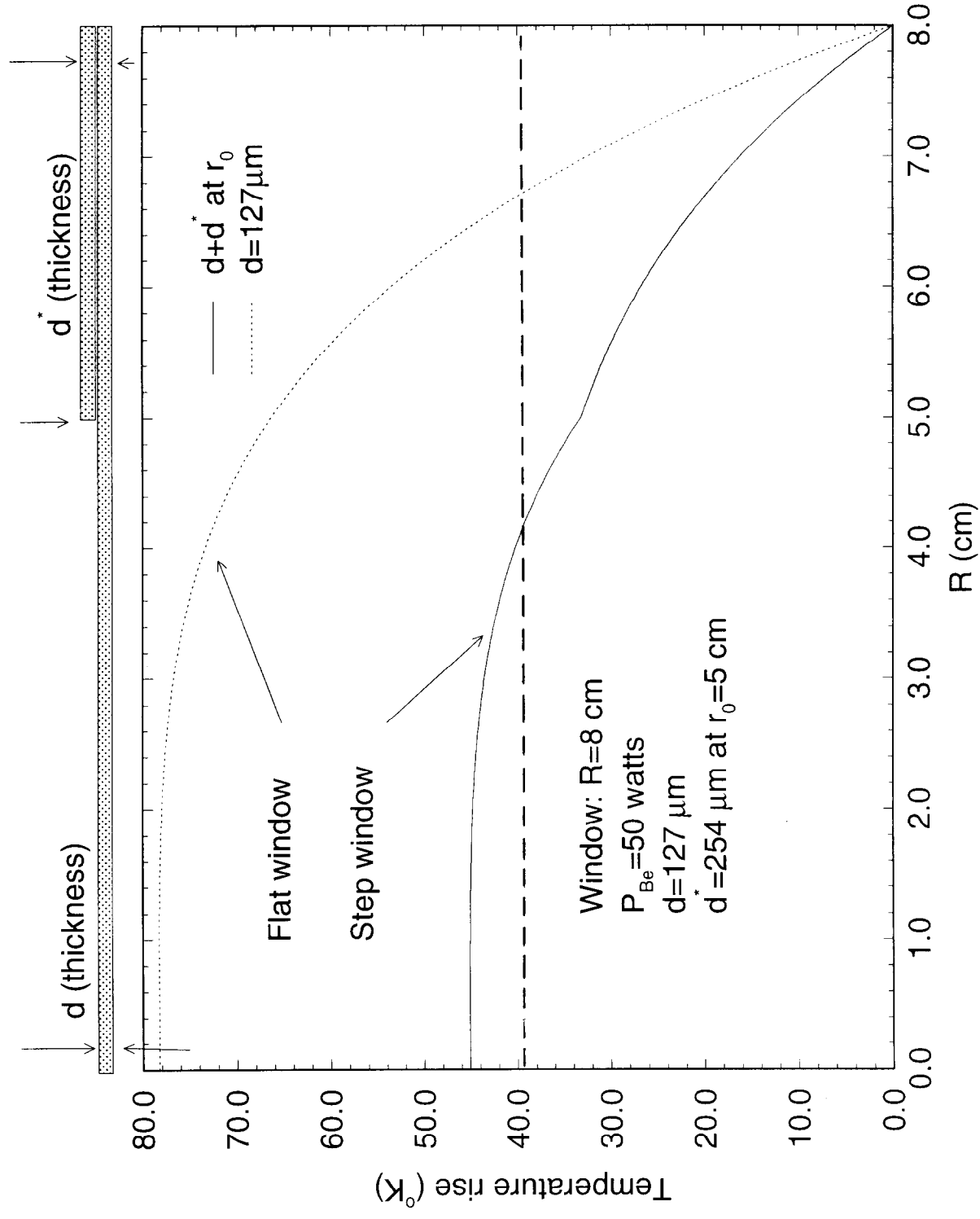
Muon Collaboration

Normal conducting RF systems - Feasibility study II parameters

- Optimize cell lengths for maximum efficiency given lattice constraints
 - Maximum multi-cell pillbox shunt impedance at 105° per cell
 - $23.5 \text{ M}\Omega\text{m}^{-1}$
 - Maximum single-cell pillbox shunt impedance at 160° per cell
 - $20 \text{ M}\Omega\text{m}^{-1}$

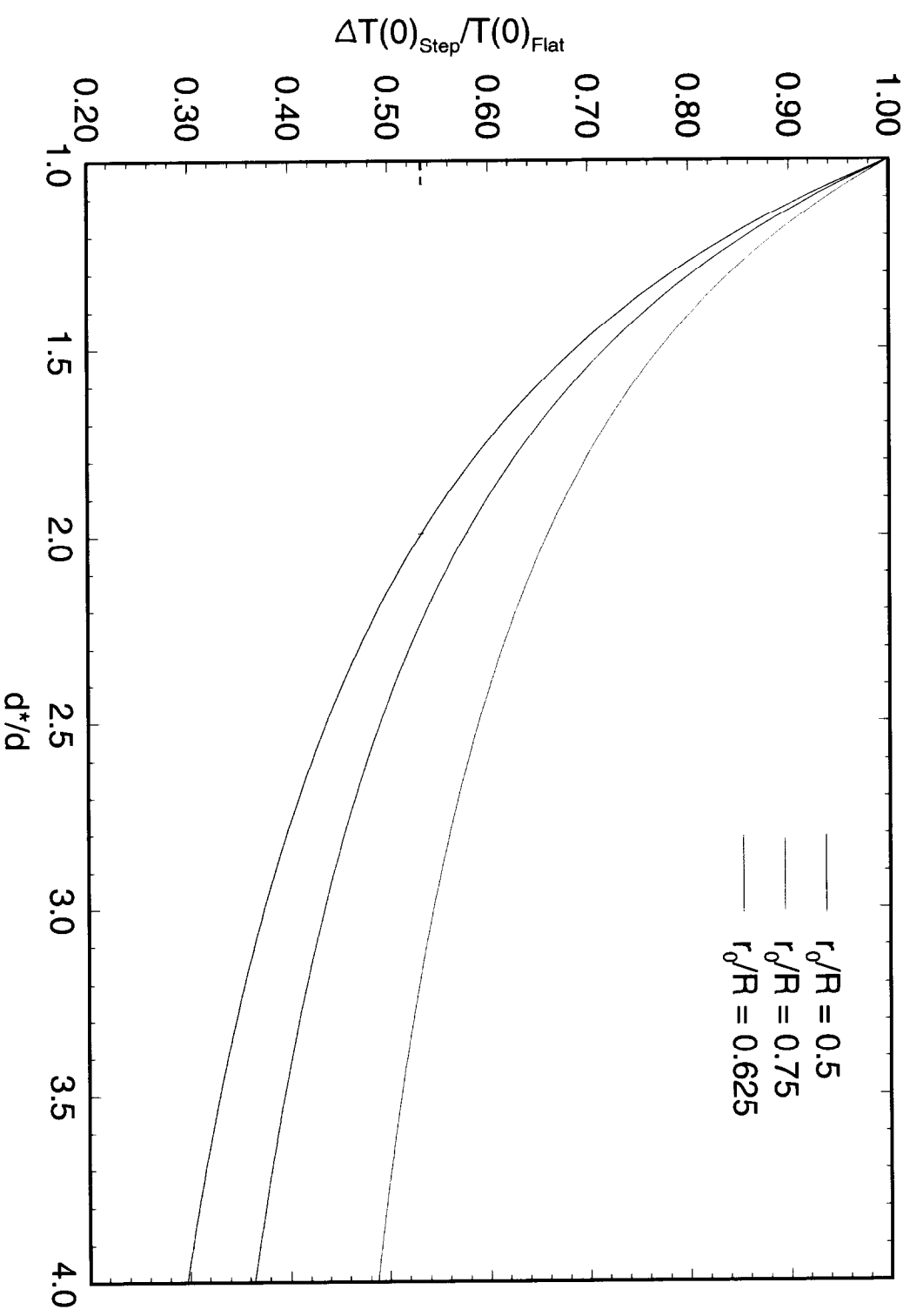
	Frequency GHz	Cell length cm	# cells per RF section	Gradient MV/m	Windows at ends of RF structures		Windows between cells		# sections	Total # RF cells	Shunt impedance $\text{M}\Omega/\text{m}$	RF input power per cell MW	Total RF power per cell type MW	Windows at ends of RF structures		Windows between cells	
					Thickness μm	Radius cm	Thickness μm	Radius cm						RF power W	Temp. $^\circ\text{C}$	RF power W	Temp. $^\circ\text{C}$
Buncher section	402.5	18.6	1	6.4	100	20	?	?	2	2	30.1	0.2	0.4	17	34	?	?
	402.5	18.6	1	6	100	20	?	?	4	4	30.1	0.17	0.63	15	30	?	?
	201.25	37.3	4	6.4	125	21	250	25	1	4	23.4	0.5	2	16	26	32	26
	201.25	37.3	4	6	125	21	250	25	2	8	23.4	0.43	3.44	14	22	28	22
	201.25	37.3	4	8	125	21	250	25	2	8	23.4	0.77	6.16	25	40	50	40
Cooling section [1,1; 1,2; 1,3]	201.25	46.6	4	16.29	125	21	250	25	6	24	22.6	3.5	84	118	189	448	359
	201.25	55.9	2	17.6	75	18	125	21	14	26	20.3	4.4	123.2	85	227	304	487
	201.25	55.9	2	17.6	75	18	75	18	10	20	20.3	4.4	83	85	227	170	453
	[2,2]	55.9	2	17.6	75	15	75	18	16	32	20.3	4.4	140.8	43	115	170	453
	[2,3a]	55.9	2	17.6	50	15	50	15	16	32	20.3	4.4	140.8	43	172	85	340
	[2,3b]	55.9	2	17.6	50	15	50	15	16	32	20.3	4.4	140.8	43	172	85	340

Step Window



Step window vs flat window

November, 2000



(4)

Nov. 6, 2000

Let's look at an example,

$$\Delta T = 487 \rightarrow \begin{cases} 5 \text{ mill thick} \\ 21 \text{ cm radius} \end{cases}$$

How can we bring ΔT below 40 K?

$$d: \text{ from } 125 \mu\text{m} \rightarrow \underline{0.5 \text{ mm}}$$

$$\Delta T \sim 122 \text{ K (linear)}$$

$$d^* = 4d \rightarrow \text{Step @ } \frac{r_0}{R} = 0.5$$

$$\Delta T \sim 37^\circ \text{K}$$

A factor 13.3 reduction!

This not optimized, and how bad the scattering is, needs to be studied.

(5)

Nov. 6, 2000

Step or tapered windows are better than flat ones

- adding thickness at $\frac{r_0}{R} < 0.5$ does not help much (may make windows stiffer)
- adding more material at larger radius helps a lot due to RF heating power distribution

Other issues:

- How to make the windows stiffer?
need new ideas, makeable
- Multi-pactoring, 2nd emission
- physical shock from beam
- EM force
- TUNER.