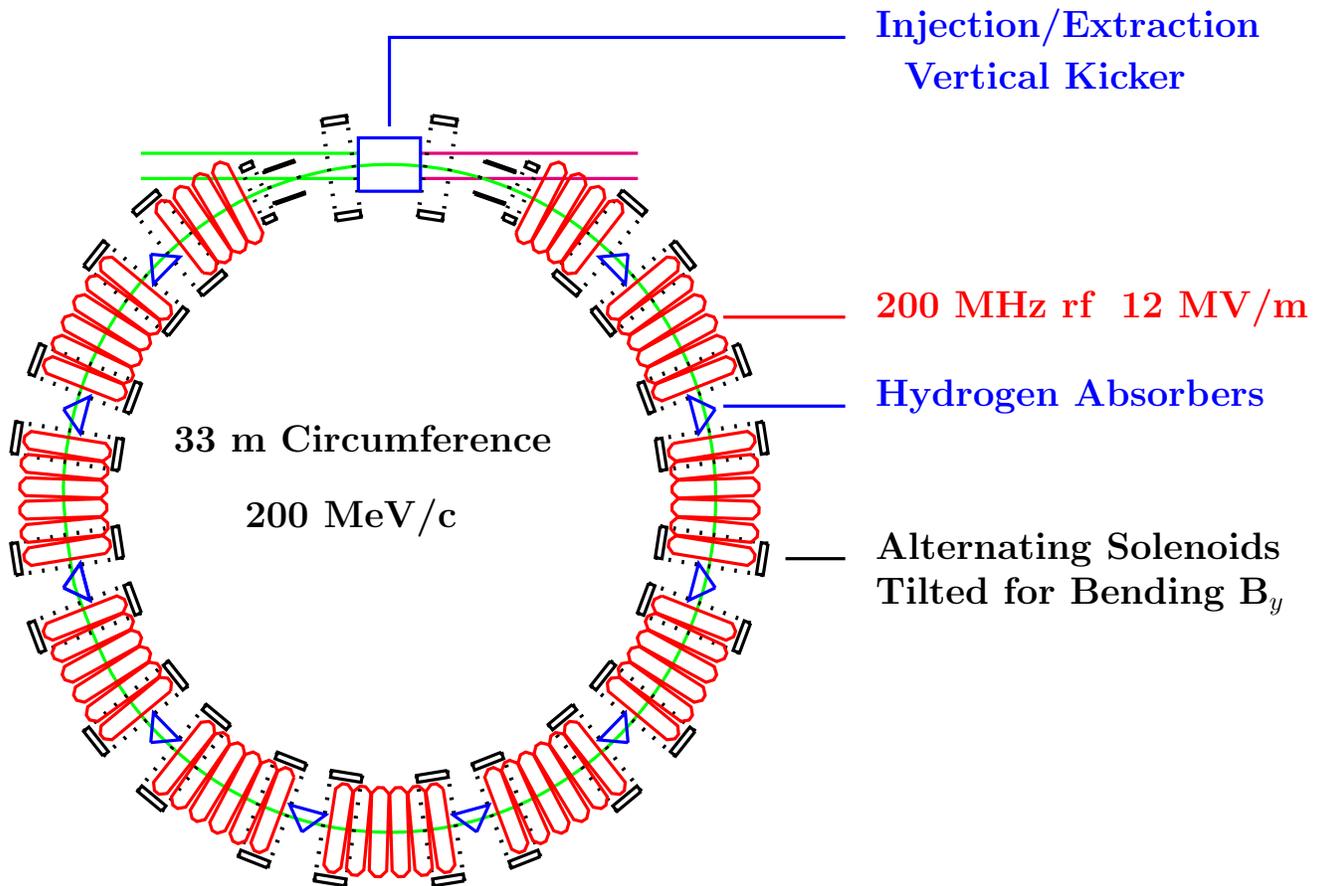


RFOFO Cooling Rings

J.S. Berg, R. Fernow, J. Gallardo, W. Lau,
R.B. Palmer, L. Reginato, D. Summers Y. Zhao

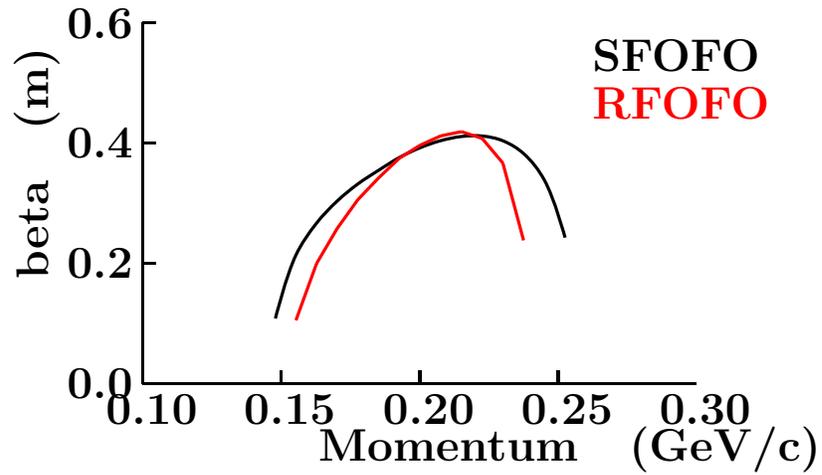
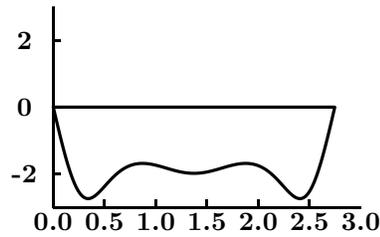
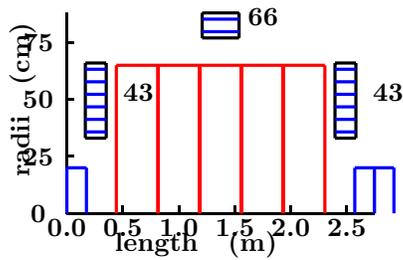
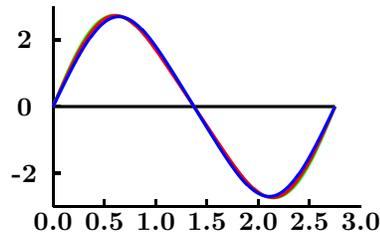
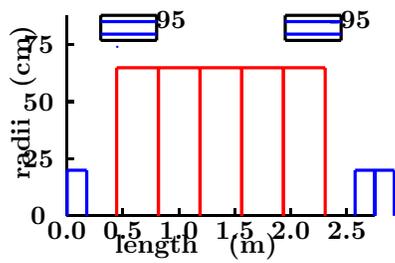
Shelter Island (May 2002)



Simple but Sinful:

- Rf in dispersive location
- Bending Field Index $n=0$
i.e. $\beta_x \neq \beta_y$

RFOFO vs SFOFO

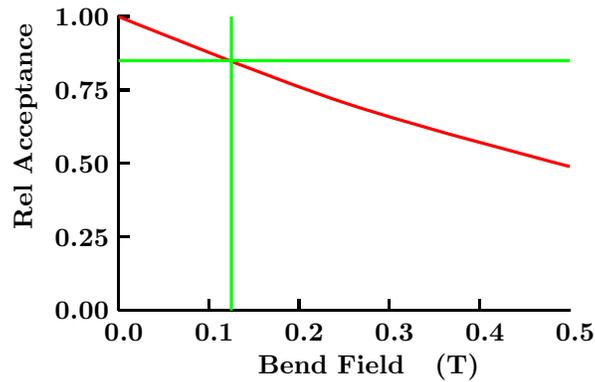
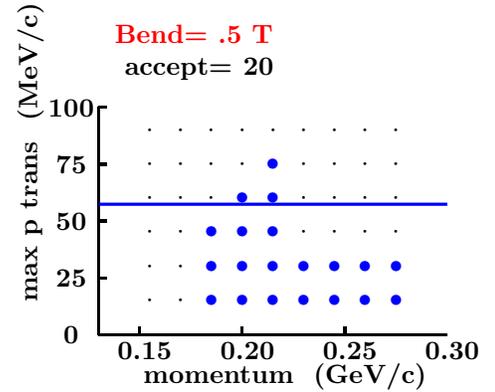
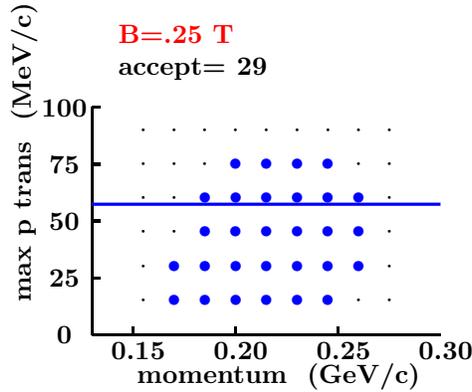
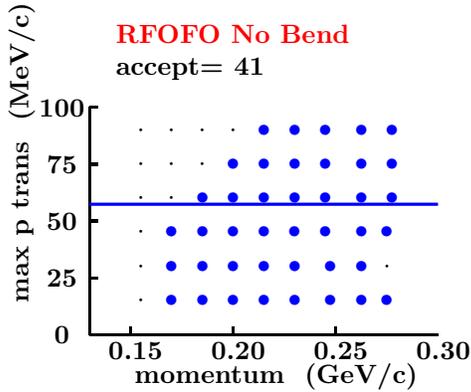


- RFOFO Mom acceptance worse
- But all cells the same

- Fewer resonances

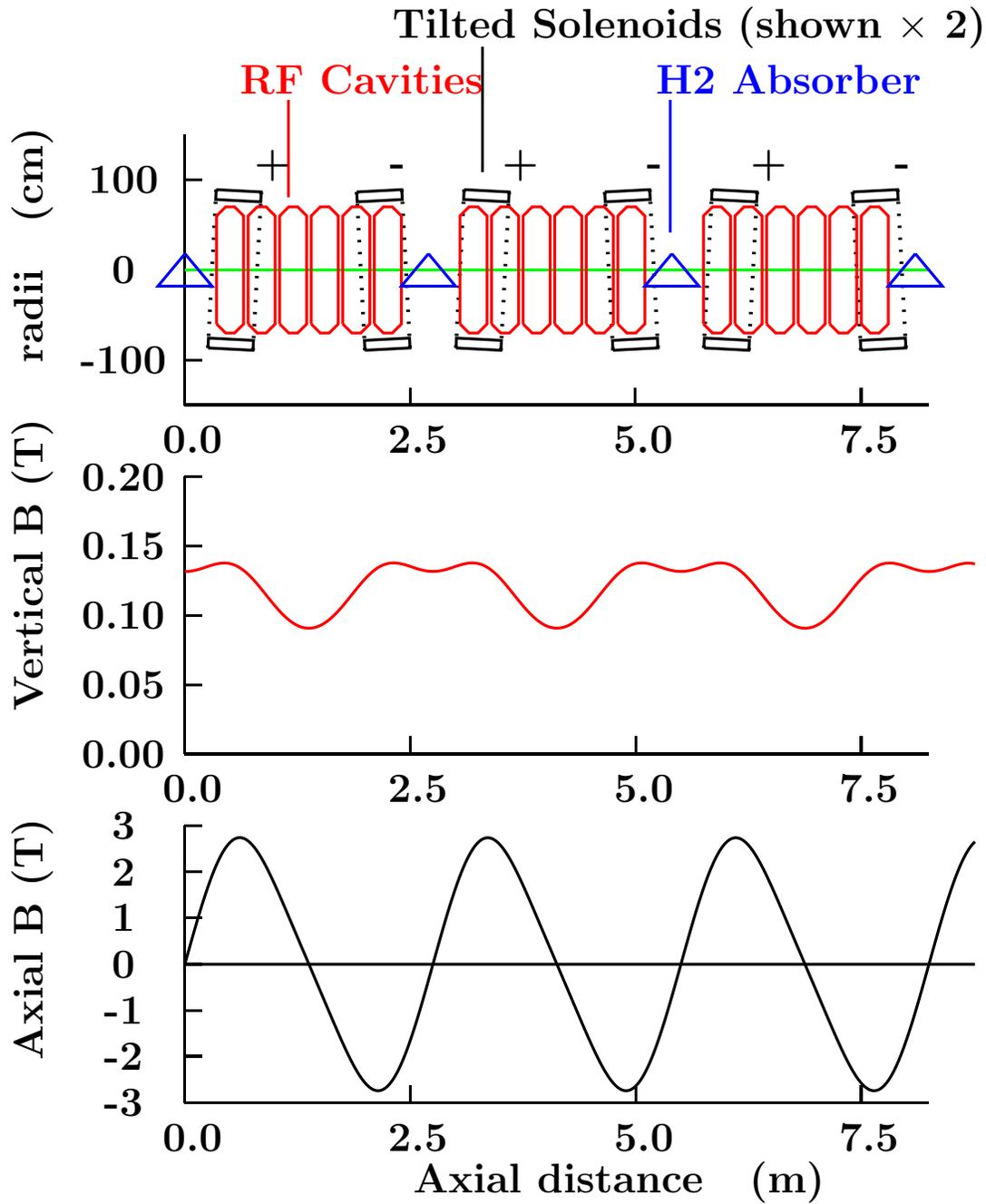
Try adding B everywhere

Acceptance vs. Bend Field

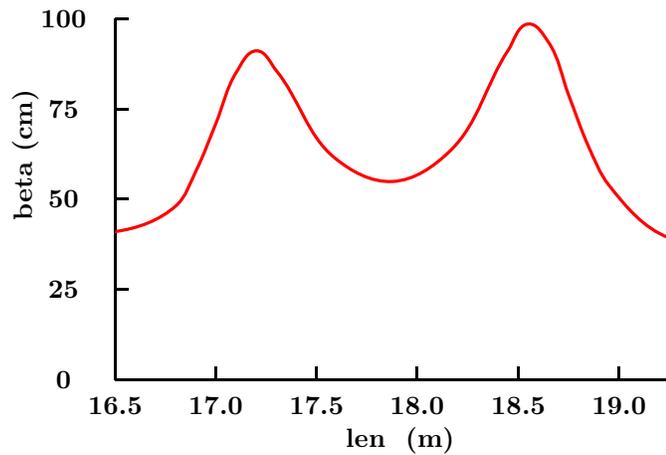


- Use least possible bend:
0.125 T gives 12 cell, 33 m Circ.
- Ang acceptance $75/200=0.37$ rad.
≫ any Quad Channel

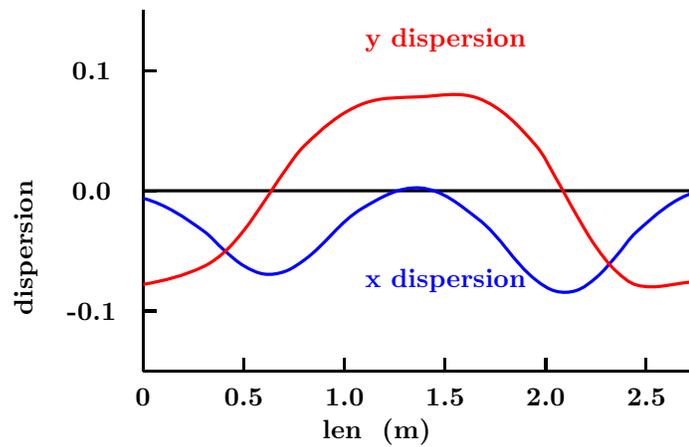
How to generate By



Beta and Dispersion



beta is \approx straight case



Dispersion is rotating
back and forth

Params for 1st Simulation

Coils

len1	dl	rad	dr	tilt	I/A
m	m	m	m	deg	A/mm ²
0.300	0.500	0.770	0.110	1.5	95.27
1.950	0.500	0.770	0.110	-1.5	-95.27

amp turns 10.48 (MA)

amp turns length 54.3 (MA m)

cell length 2.75 (m)

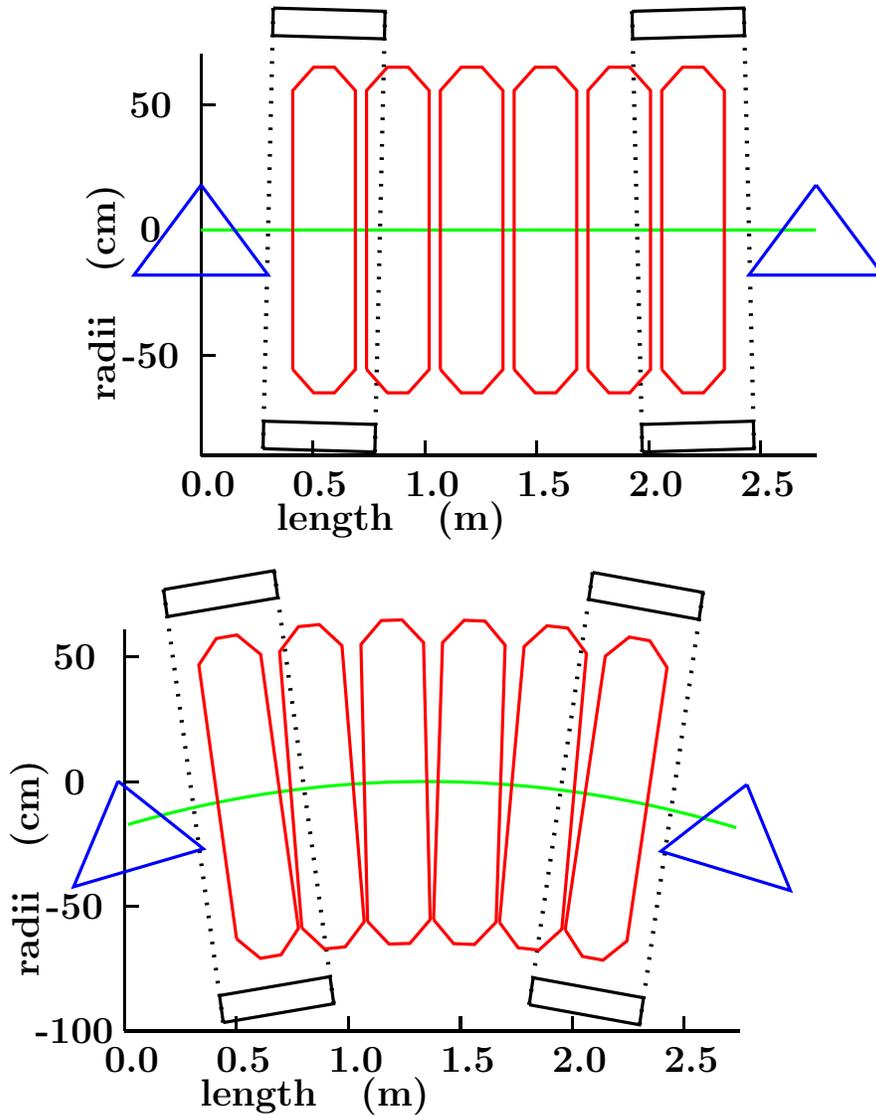
Wedge

Material		H2
Windows		none
Radius	cm	18
central thickness	cm	28.6
min thickness	cm	0
wedge angle	deg	76.93
wedge azimuth from vertical	deg	30

RF

Cavities		6
Lengths	cm	28
Central gaps	cm	5
Radial aperture	cm	25
Frequency	MHz	201.25
Gradient	MV/m	12
Phase rel to fixed ref	deg	25
Windows		none

RF & Absorber Layout

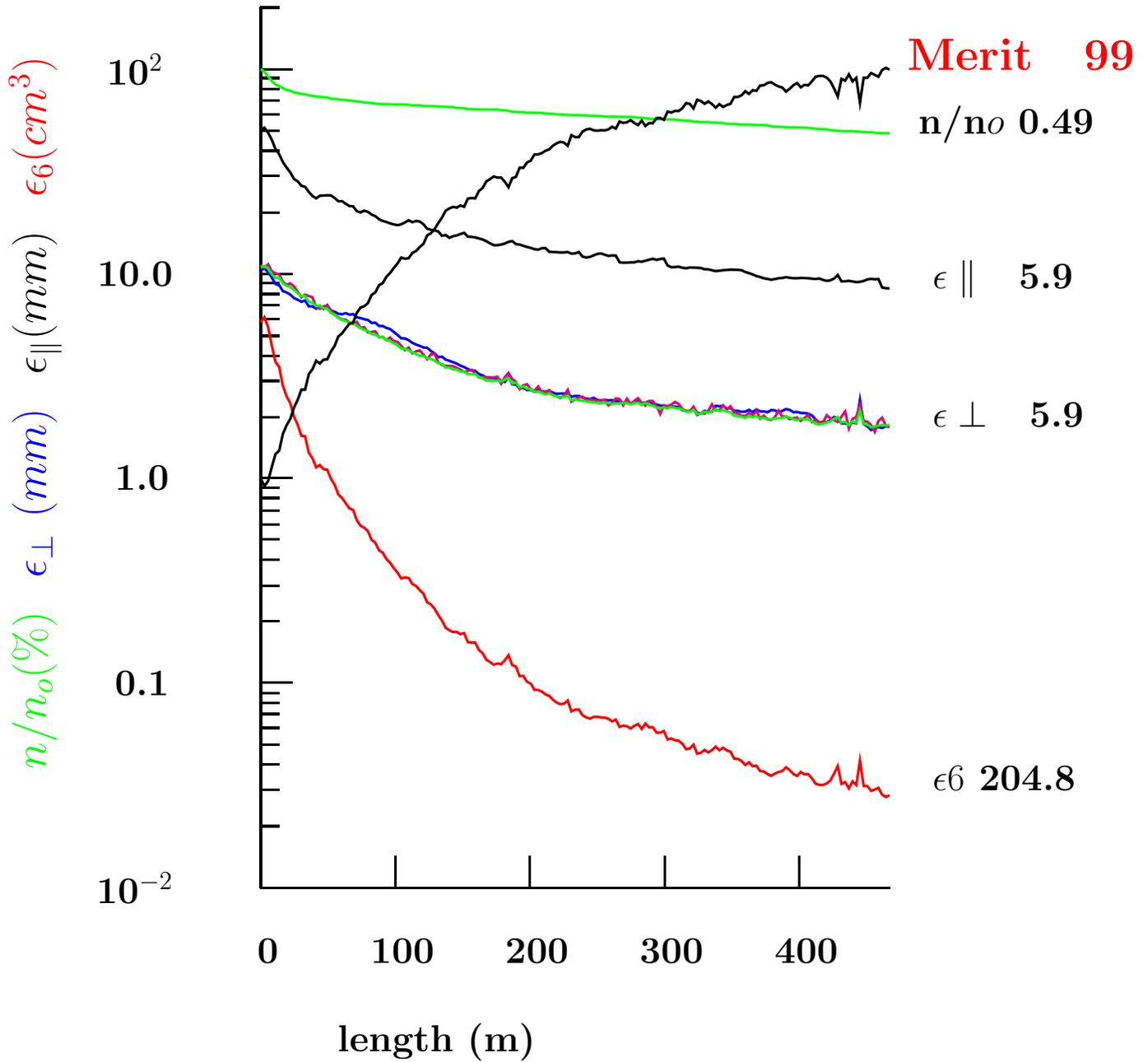


- New ICOOL (2.38) for wedge rf
- Wedges shown 0 and 90 deg.
true angle 30 deg

ICool Simulation

Input From Study 2

$n/n_0 = 485 / 1000$



Cooling Efficiency

”Merit” is maximized by cooling for as long as possible in a given ring, even if the gains are slow. This will not give the best final performance for multiple rings. We define a local criterion:

”Cooling Efficiency” (Q).

Define

$$Q(x) = \frac{d\epsilon_6/\epsilon_6}{dN/N}$$

Note, if $Q(x)=\text{constant}$, then

$$\int_o^n \frac{d\epsilon_6}{\epsilon_6} = Q \int_o^n \frac{dN}{N}$$

$$\text{Ln} \left(\frac{\epsilon_6(n)}{\epsilon_6(o)} \right) = Q \text{Ln} \left(\frac{N(n)}{N(o)} \right)$$

$$\left(\frac{\epsilon_6(n)}{\epsilon_6(o)} \right) = \left(\frac{N(n)}{N(o)} \right)^Q$$

or

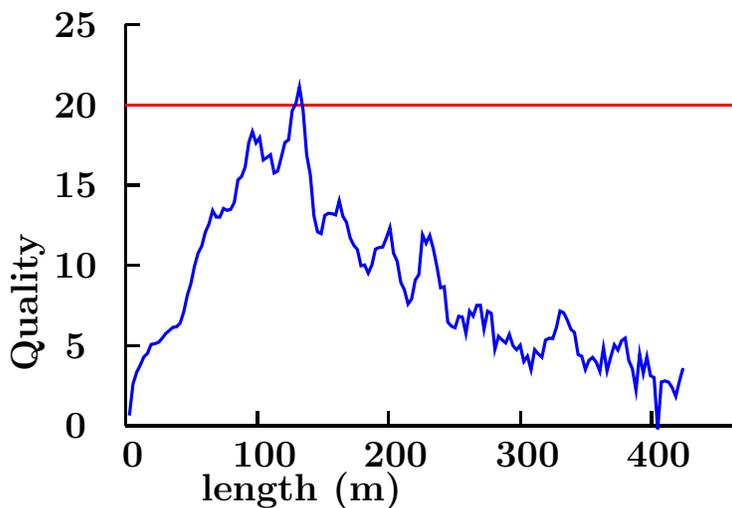
$$\frac{N(n)}{N(o)} = \left(\frac{\epsilon_6(n)}{\epsilon_6(o)} \right)^{1/Q}$$

e.g. for a collider

$$\frac{\epsilon_6(n)}{\epsilon_6(o)} = 10^{-6}, \quad \frac{N(n)}{N(o)} = \quad = 0.5$$

$$\text{Required } Q = \ln\left(\frac{10^{-6}}{0.5}\right) = 20$$

**For Hydrogen without windows
or Injection/extraction**

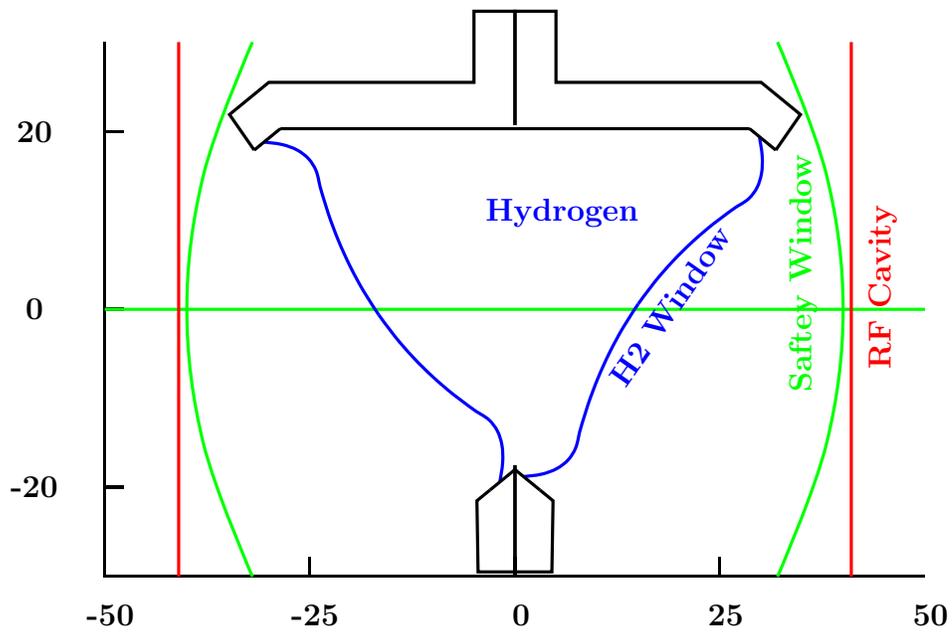


Almost ok even for collider.

But

for only short length
no windows,
no injection/extraction

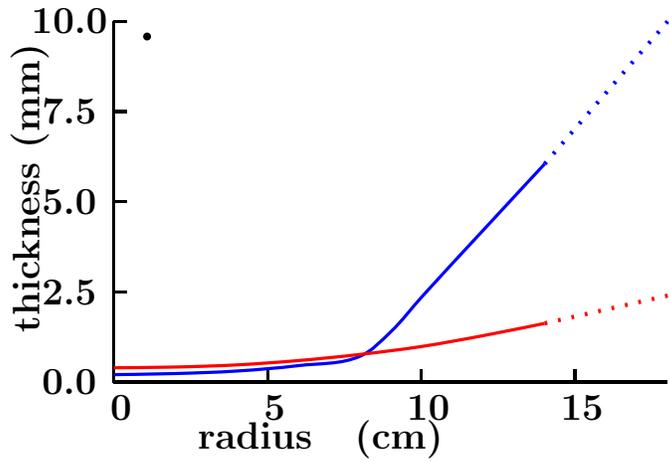
Hydrogen Absorber



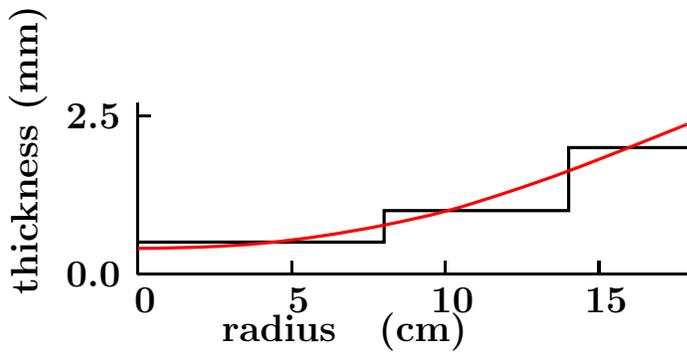
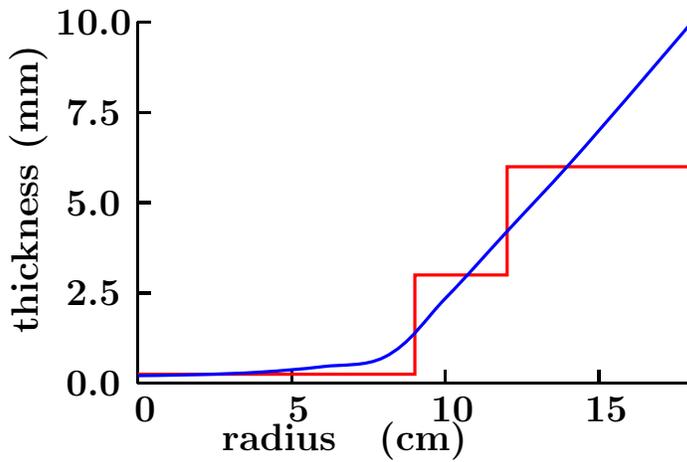
- "Bellows" type Windows
- One Convex, One Concave ?

Hydrogen Windows

Compare Conventional & Bellows types



Approximate by steps for ICOOL



ICOOL Results

No RF or Safety Windows

Absorber	window	center thickness mm	Merit	Maximum Q
Hydrogen	none		92	20
”	Conventional	0.5	31	7
”	Bellows	0.25	41	10
”	Bellows	0.125	61	18
LiH	none		19	7

- Rings are more sensitive to windows than linear cooling
- Maximum Efficiency is less damaged than Merit
- Implies use of more rings: Expensive
- Even 125 micron Al degrades Merit 92 → 61
- Must Consider AlBemet, Li, LiH as window materials

RF Windows

- Current Be Foils too thick
although not yet simulated
- Propose Nitrogen temp RF
 - expansion coeff = 1/10
→ Thinner windows
 - RF Power = 1/2.5
 - Cryo Cost < RF Savings ?
 - radiation heating to H2 down
 - Same vacuum for RF and Coils

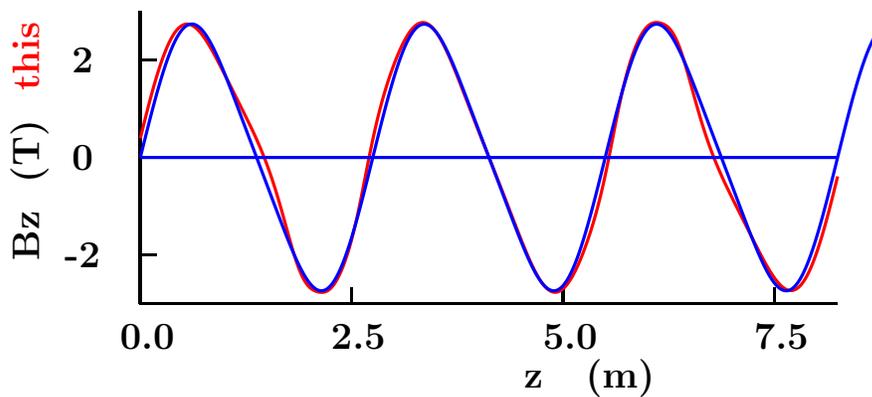
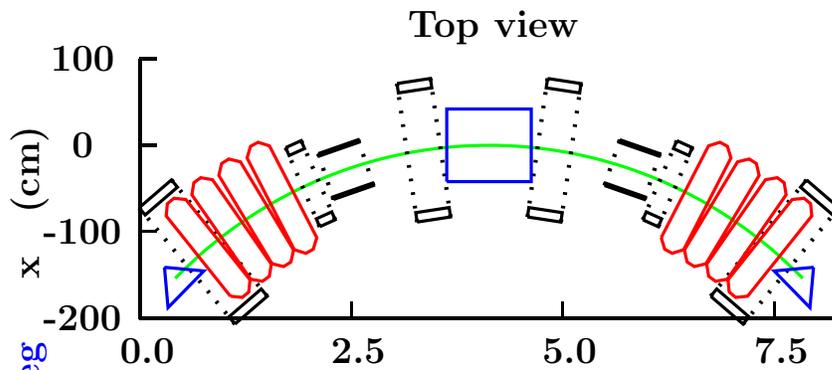
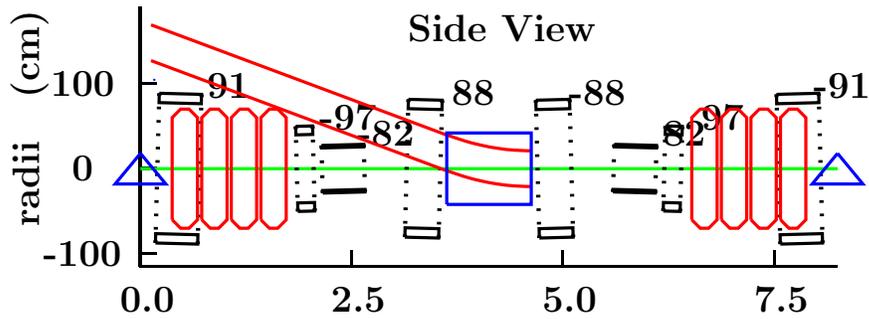
Wall Power if 77 deg RF

If η_{RF} (wall to RF) = 25 %
and η_{Cryo} = 50% of Carnot = 15 %
and rf power = P_{RF}
then

$$\frac{P_{\text{wall}}(\text{cold})}{P_{\text{wall}}(\text{warm})} = \frac{[P_{RF}/\eta_{RF} + P_{RF}/\eta_{Cryo}] / 2.5}{P_{RF}/\eta_{RF}} \approx 1.0$$

Not obviously a greater

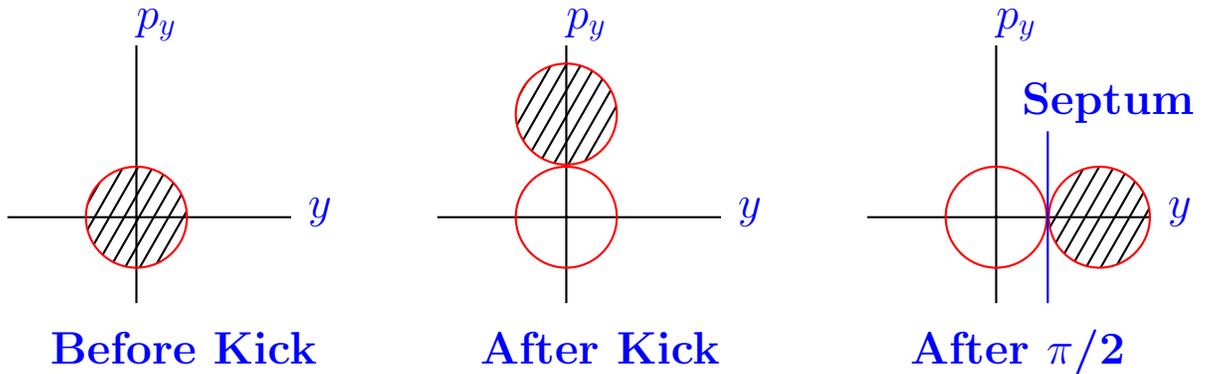
Injection/Extraction



- First Simulation gave Merit = 10
Synchrotron tune = 2.0: Integer
- Change Circ. to 41 m: Merit = 55
- Improvements probable by matching

Kicker

Minimum Required kick



$$I = \left(\frac{f_\mu \ 4 \ f_\sigma^2 \ m_\mu}{\mu_o \ c} \right) \frac{\epsilon_n}{L}$$

$$V = \left(\frac{f_\Phi \ 4 \ f_\sigma^2 \ m_\mu \ R}{c} \right) \frac{\epsilon_n}{\tau}$$

$$U = \left(f_\mu \ f_\Phi \ \frac{m_\mu^2 \ 8 \ f_\sigma^4 \ R}{\mu_o \ c^2} \right) \frac{\epsilon_n^2}{L}$$

- muon $\epsilon_n \gg$ other ϵ_n 's
- So muon kicker Joules \gg other kickers
- Nearest are \bar{p} kickers

Compare with others

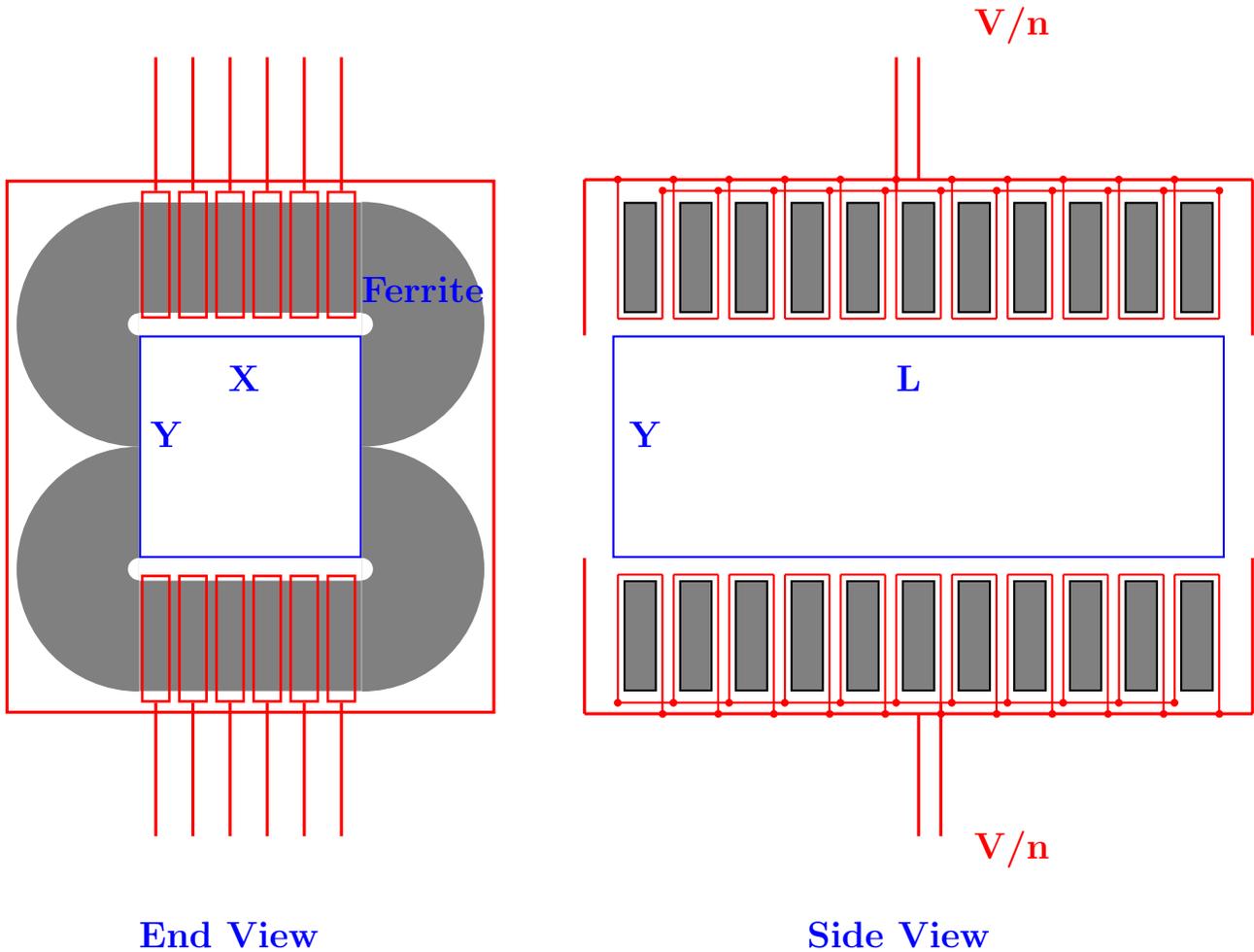
		μ Cooling	CERN \bar{p}	Ind Linac
$\int Bdl$	Tm	.30	.088	
L	m	1.0	≈ 5	5.0
t_{rise}	ns	50	90	40
B	T	.30	≈ 0.018	0.6
X	m	.42	.08	
Y	m	.63	.25	
$V_{1\text{turn}}$	kV	3,970	800	5,000
U_{magnetic}	J	10,450	≈ 13	8000

Note

- J is 3 orders above \bar{p}
- Same order as Induction
- And t same order
- But V is too High

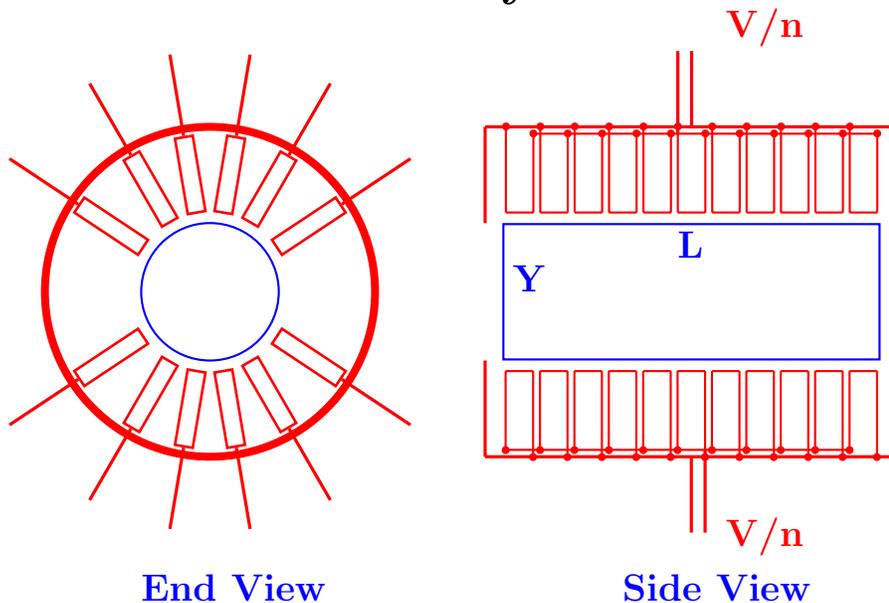
New Idea

- Drive Flux Return
- Subdivide Flux Return
- Conducting Box Removes Stray Field Return



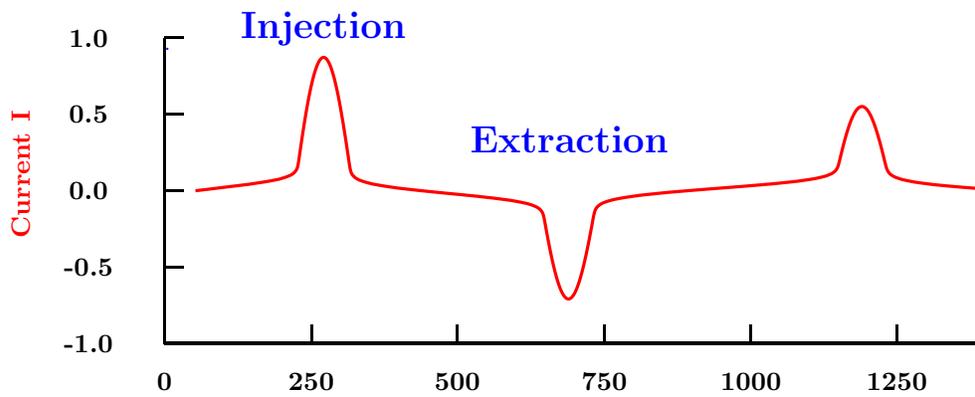
Works with no Ferrite

- $V = \text{the same}$
- $U \approx 2\times$
- $I \approx 2\times$
- No rise time limit
- Not effected by solenoid fields

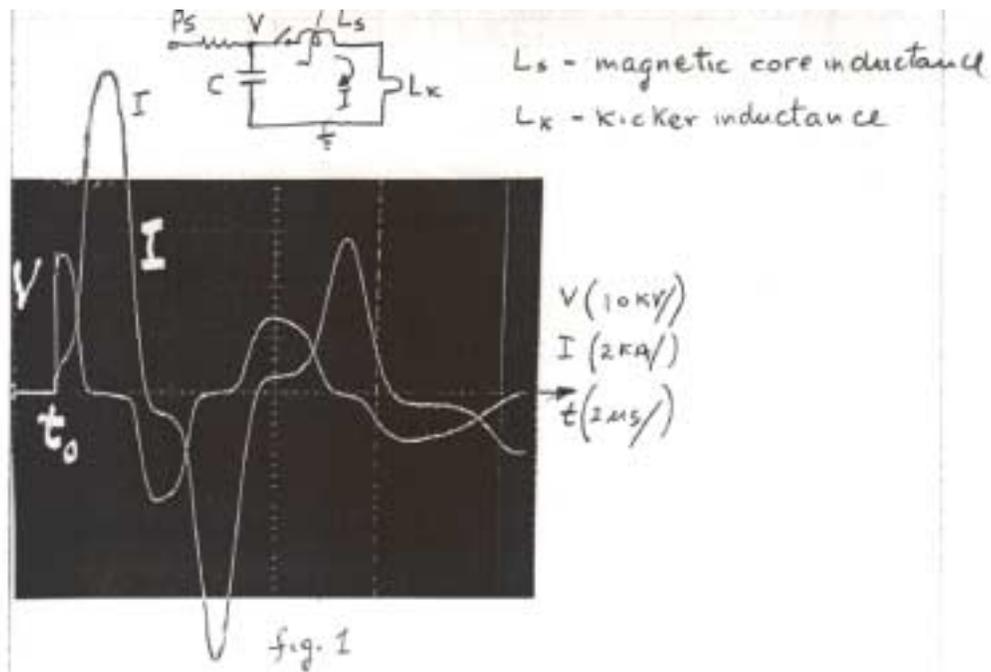


- If non Resonant: 2 Drivers
for inj. & extract.
Need 24×2 Magamps (≈ 20 M\$)
- If Resonant: 1 Driver, $2\times$ efficient
Need 12 Magamps (≈ 5 M\$)

Resonant Circuit



Circuit Model



- May be hard for many turns
- Not simulated with initial stages

Conclusion

- Much better than Quad Rings
- Similar to Balbakov's
- But Maxwellian & Realistic Fields

Need to Study

- Integration in a system
Front end, E, freq etc
- Wedge absorber design
- Thin H₂ windows,
e.g. AlBemet
- Thin Be Windows,
e.g. Nitrogen Temp RF
- Injection Extraction Tracking
- Kicker
- Cost Reduction (Don's idea)
- SFOFO More Sin:
Pi Resonance in Acceptance.
Valeri gets away with it.