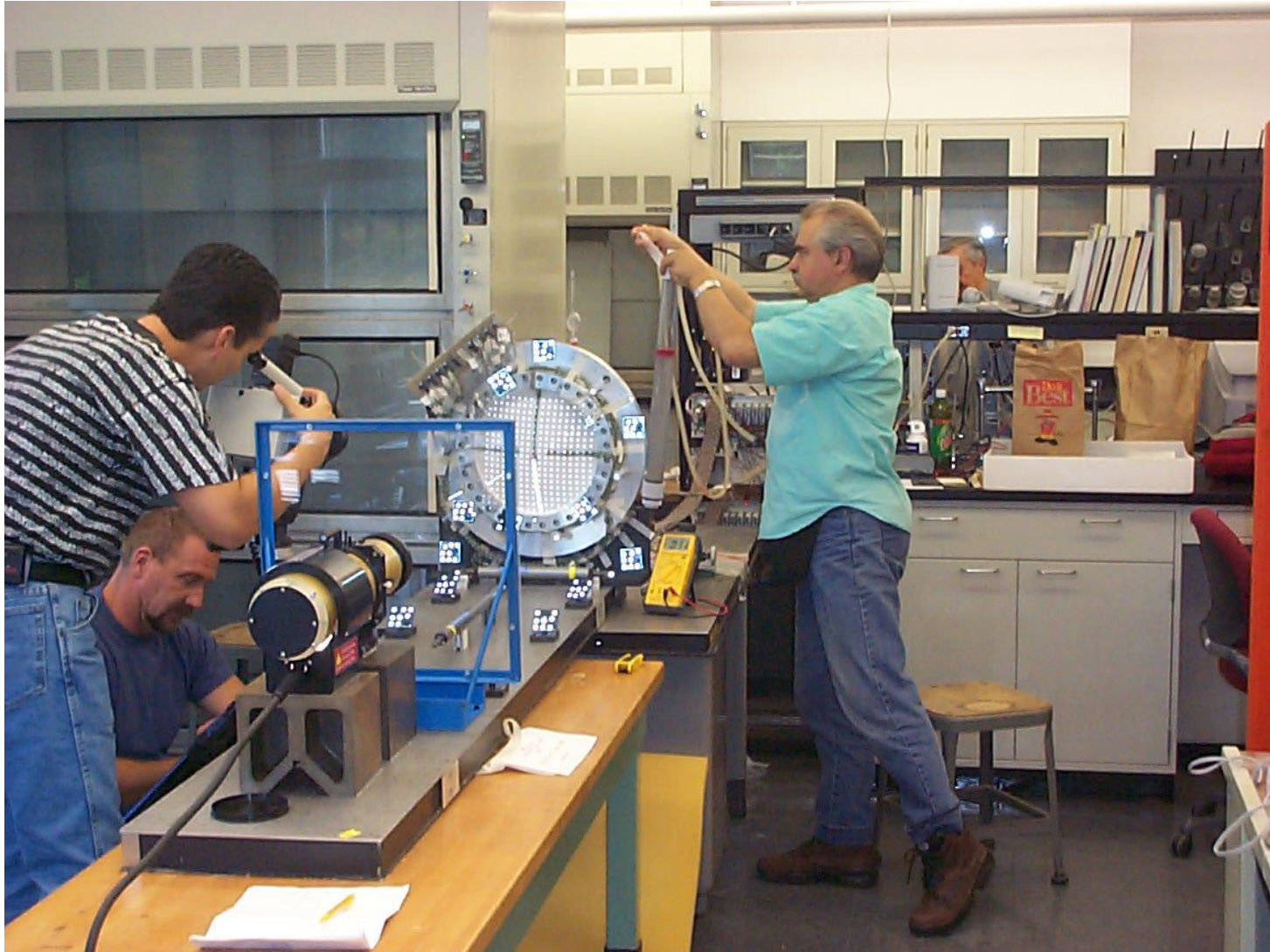


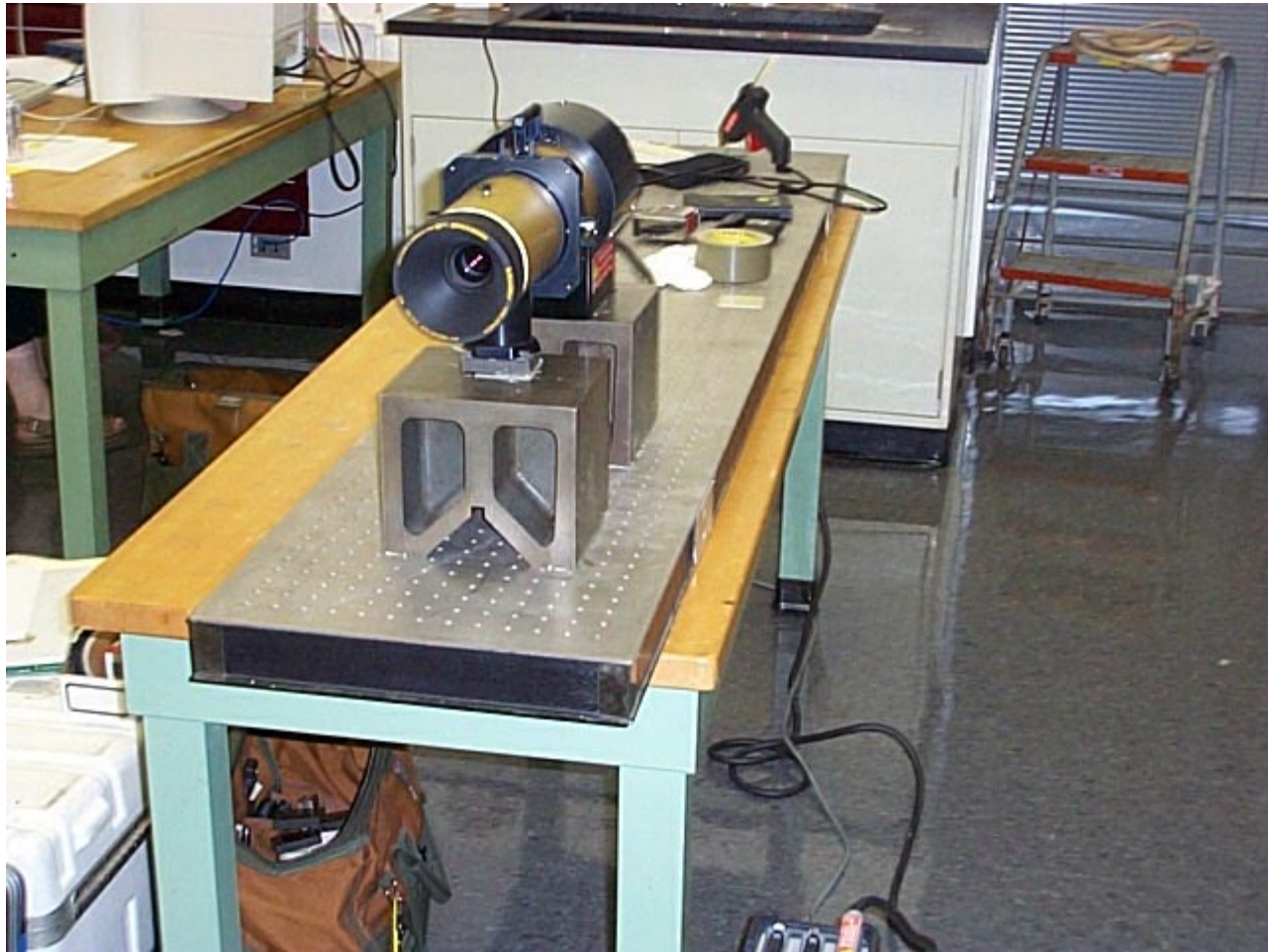
# *Mucool history of photogrammetry*

- Compare the window's *performance* to FEA
- Observe *characteristics* of the window's performance
- Compare the window's *shape and thickness* to design specifications

# Photogrammetry setup



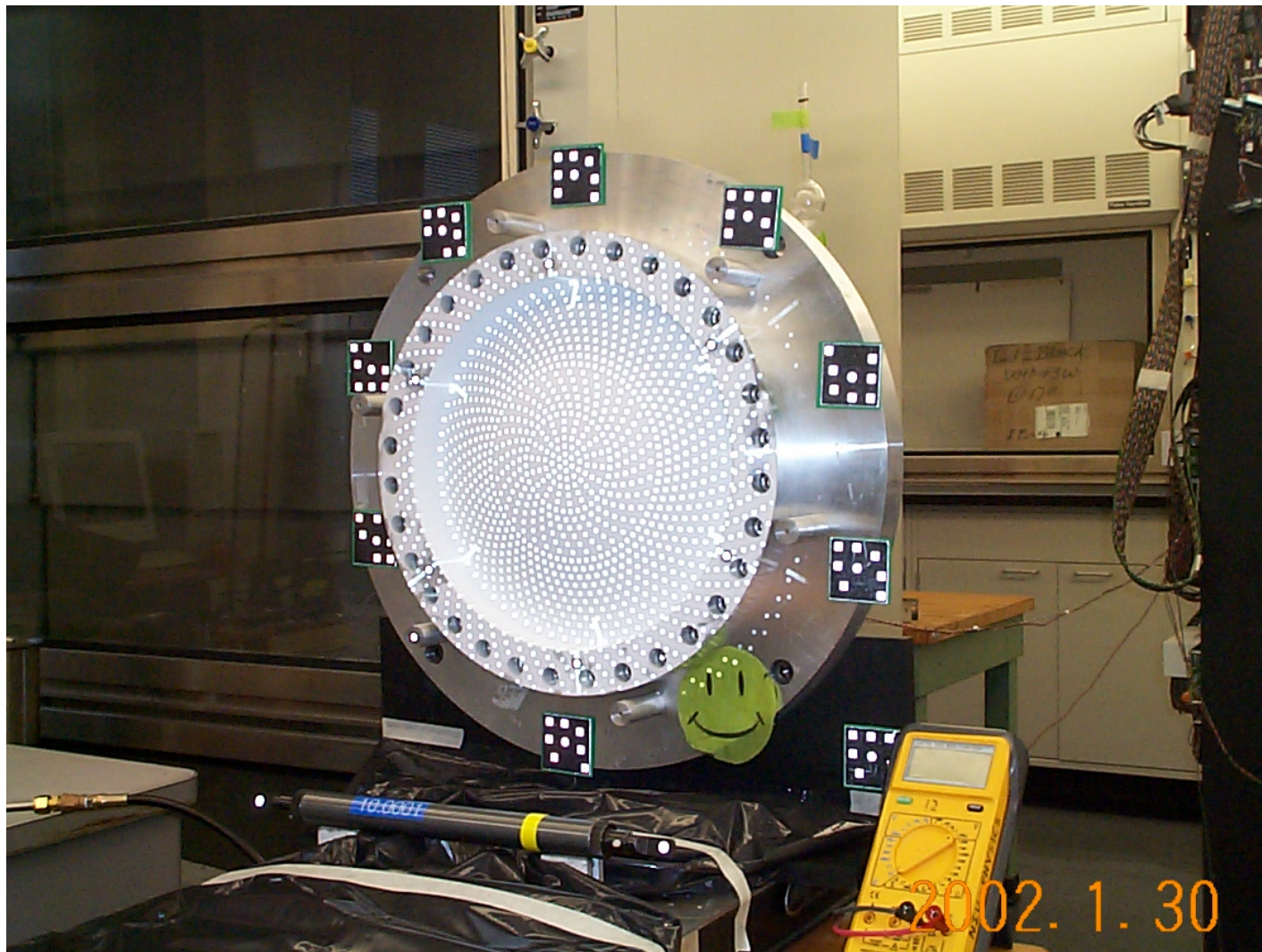
# Pro-Spot projector



# Projecting targets



# Targets

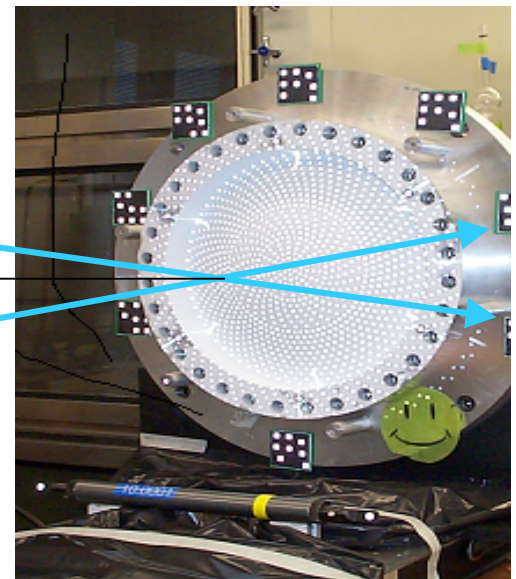
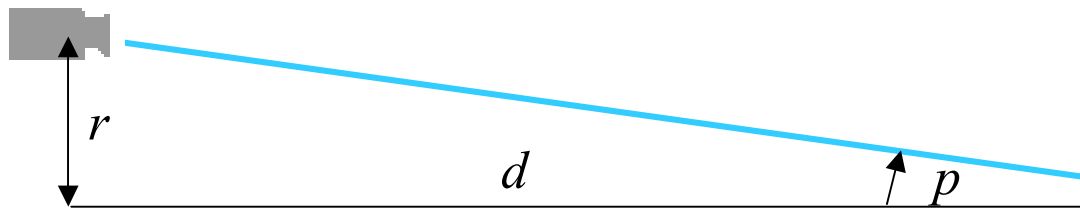
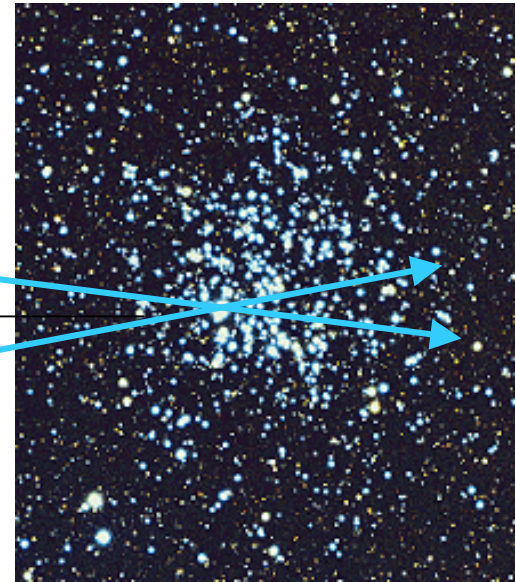
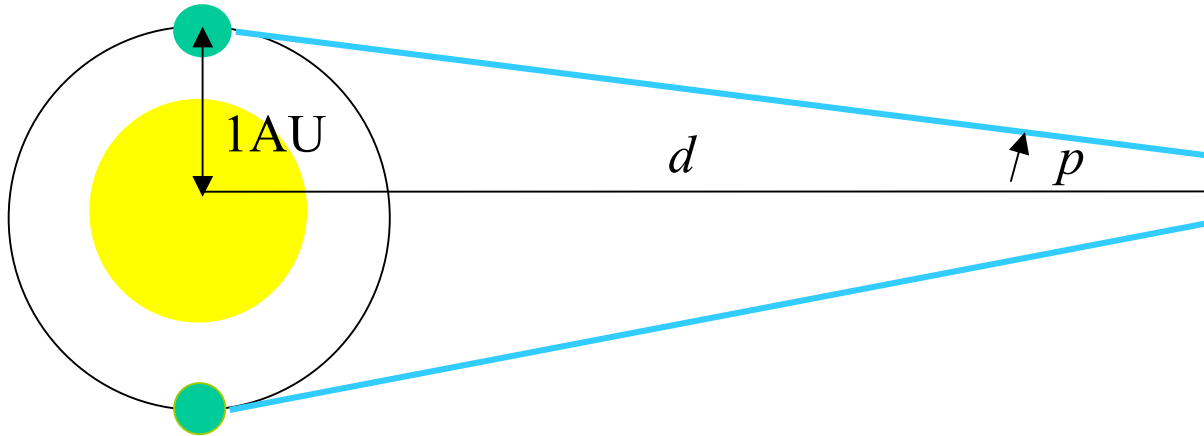


How does photogrammetry work?  
How does photogrammetry work?

# Parallax

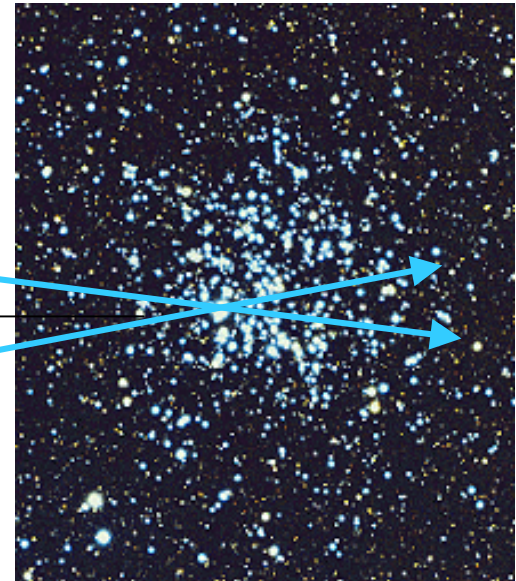
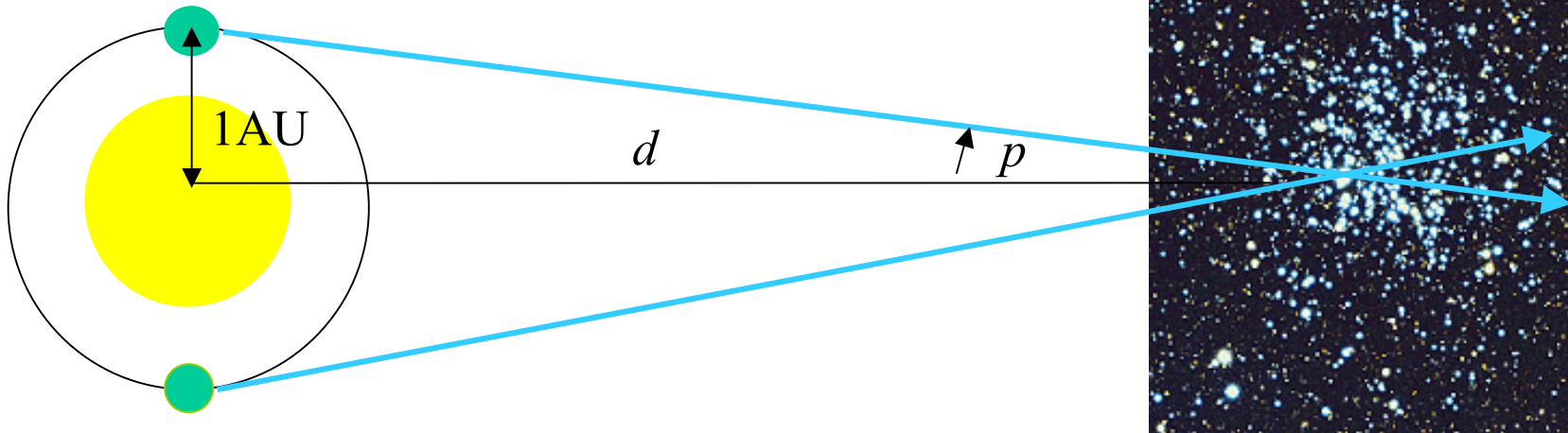
## Parallax

Stellar parallax  
Stellar parallax

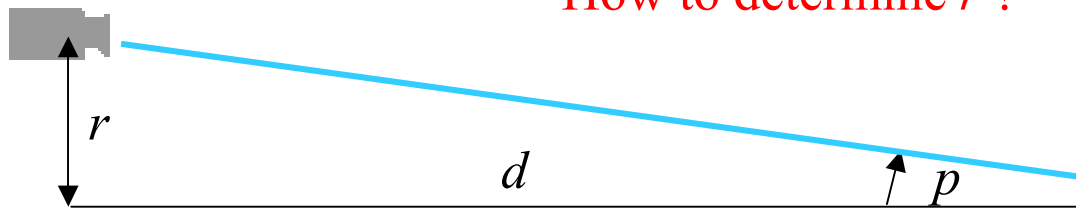


Photogrammetry  
Photogrammetry

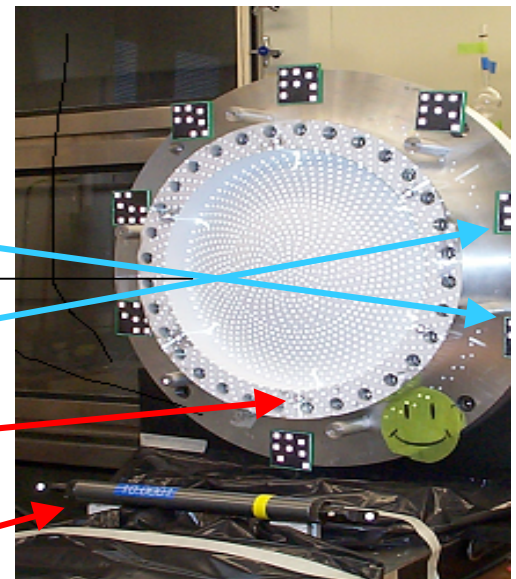




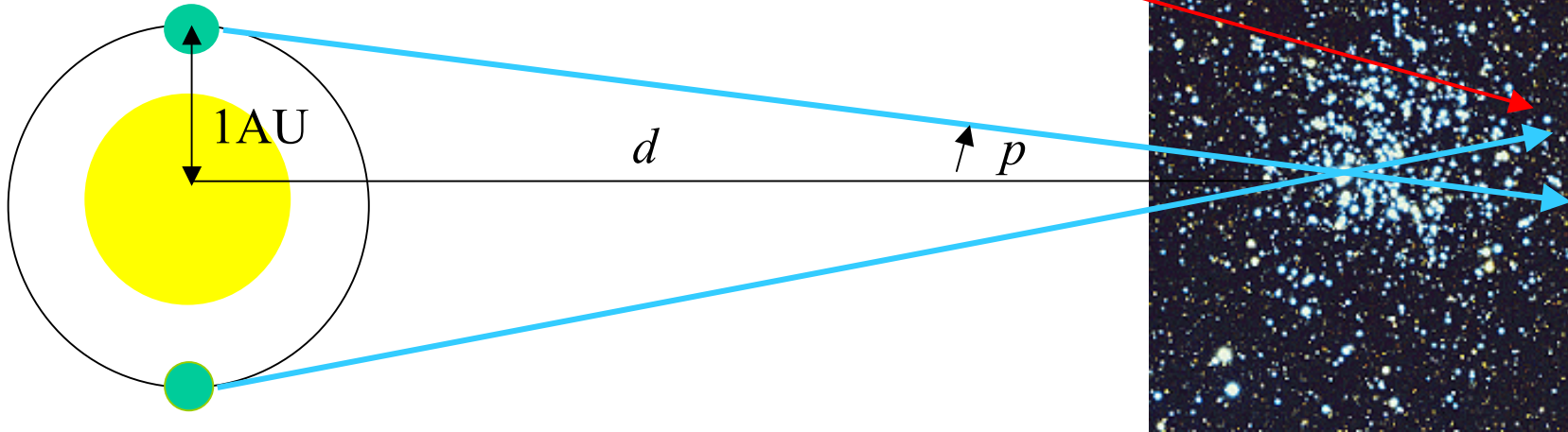
How to determine  $r$  ?



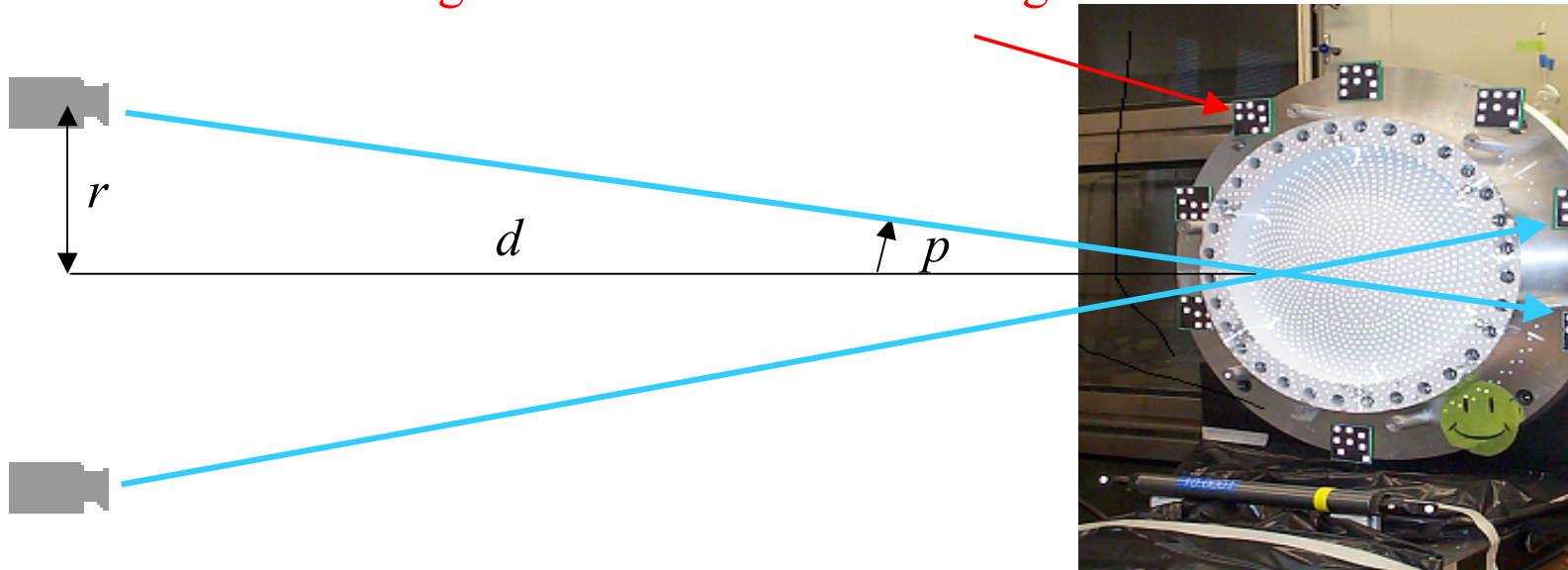
Fixed targets  
and  
scale bar



Identifiable “field stars”



Coded targets = Identifiable “field targets”

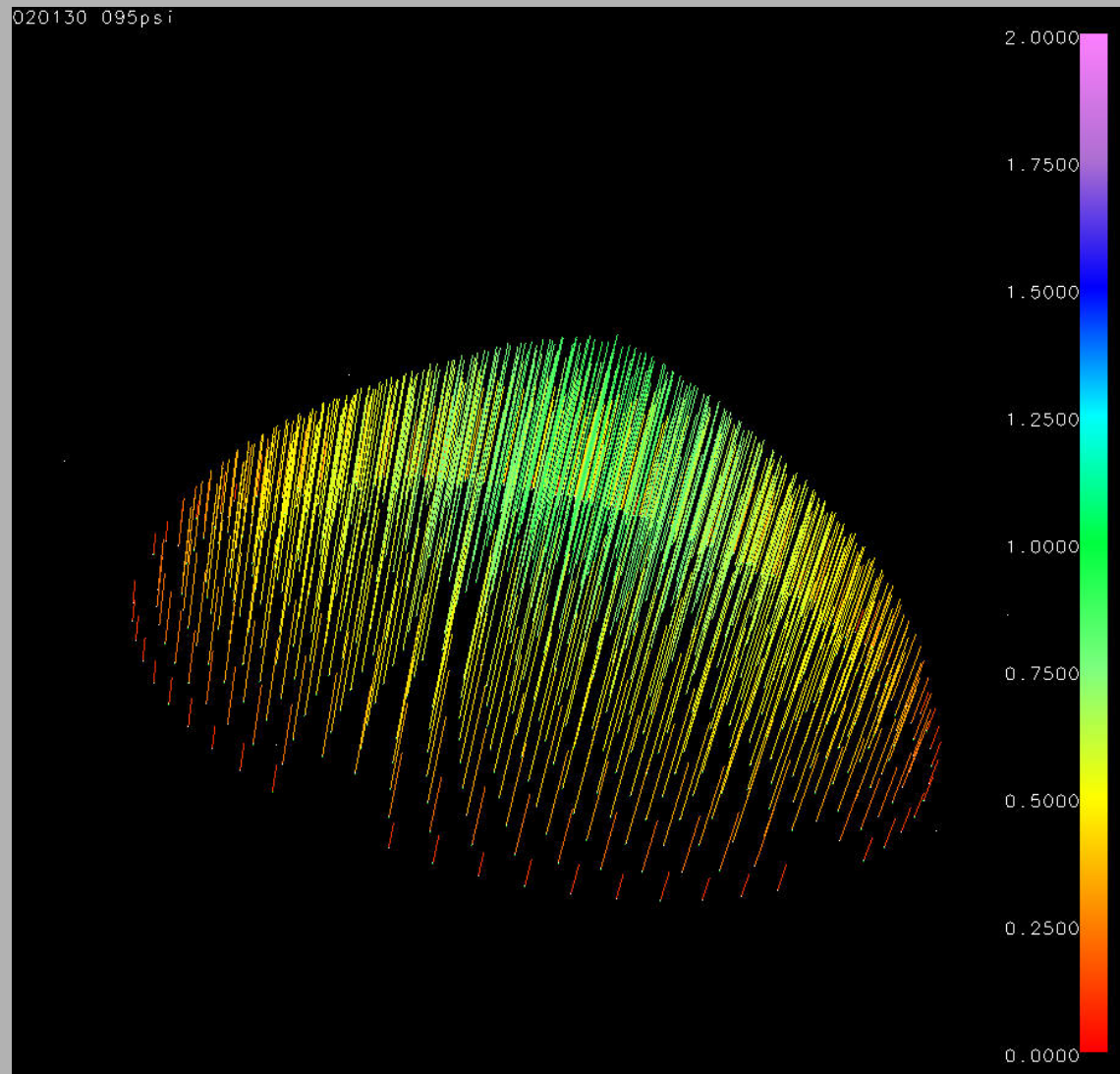


# *Mucool history of photogrammetry*

- Compare the window's *performance* to FEA
- Observe *characteristics* of the window's performance
- Compare the window's *shape and thickness* to design specifications

# Create an “animation” of the deformation of the window using whisker plots

Display the *change* in the surface from the initial, unstressed shape

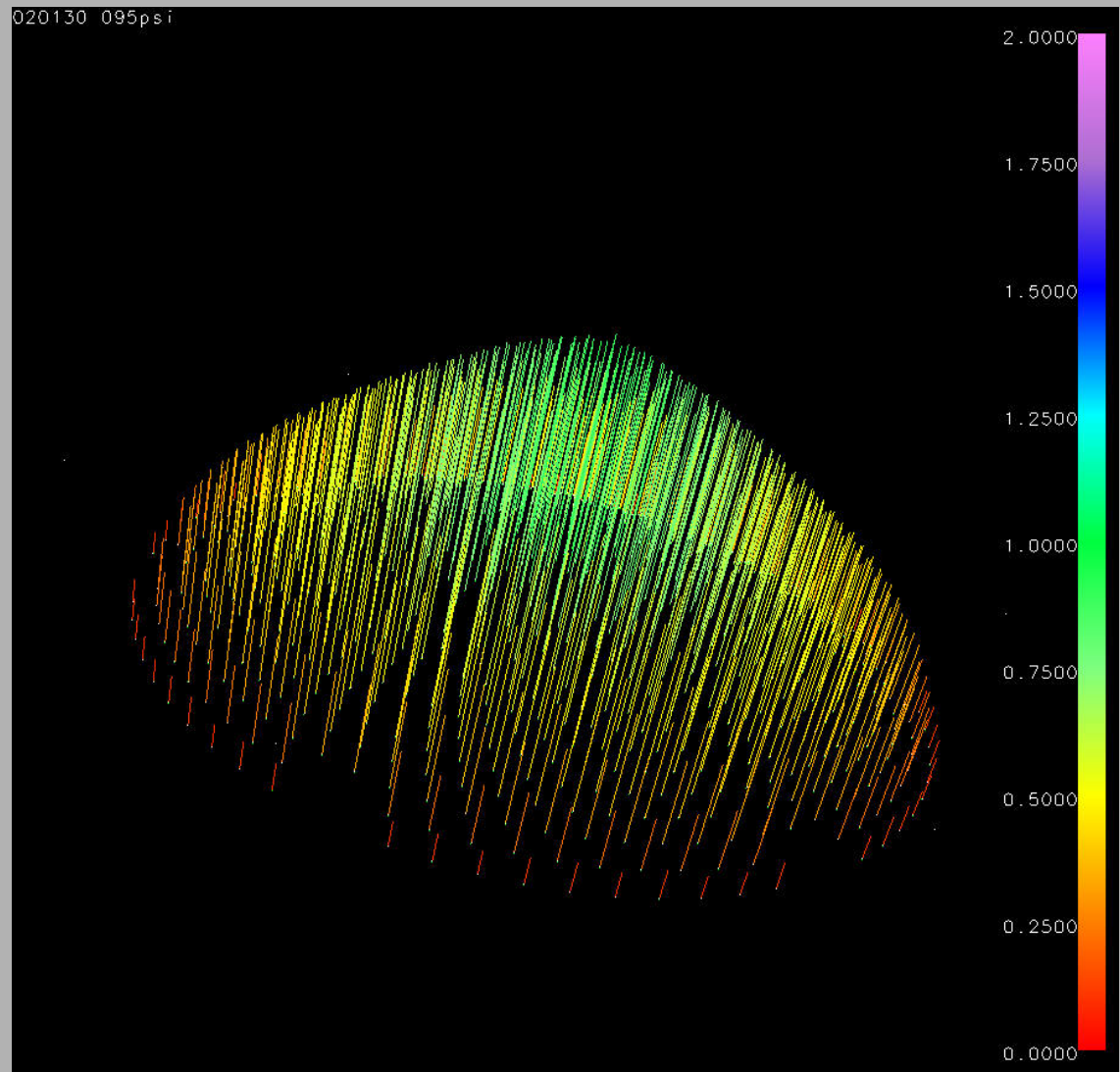


Window 3

Pressure



Delta z (mm)

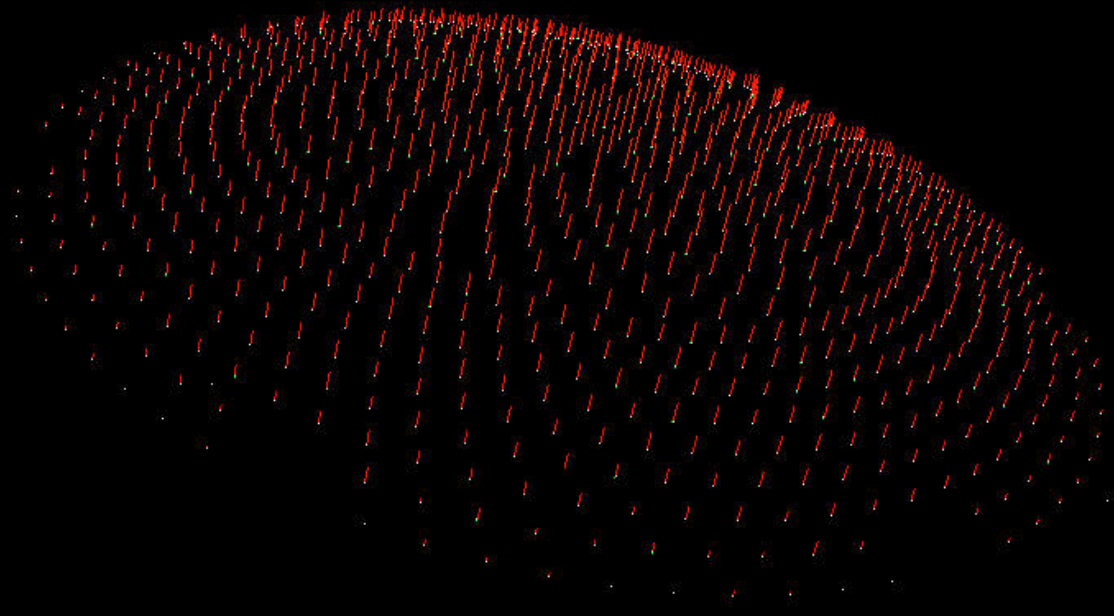


Whisker length =  
 $z(95\text{psi}) - z(0\text{psi})$

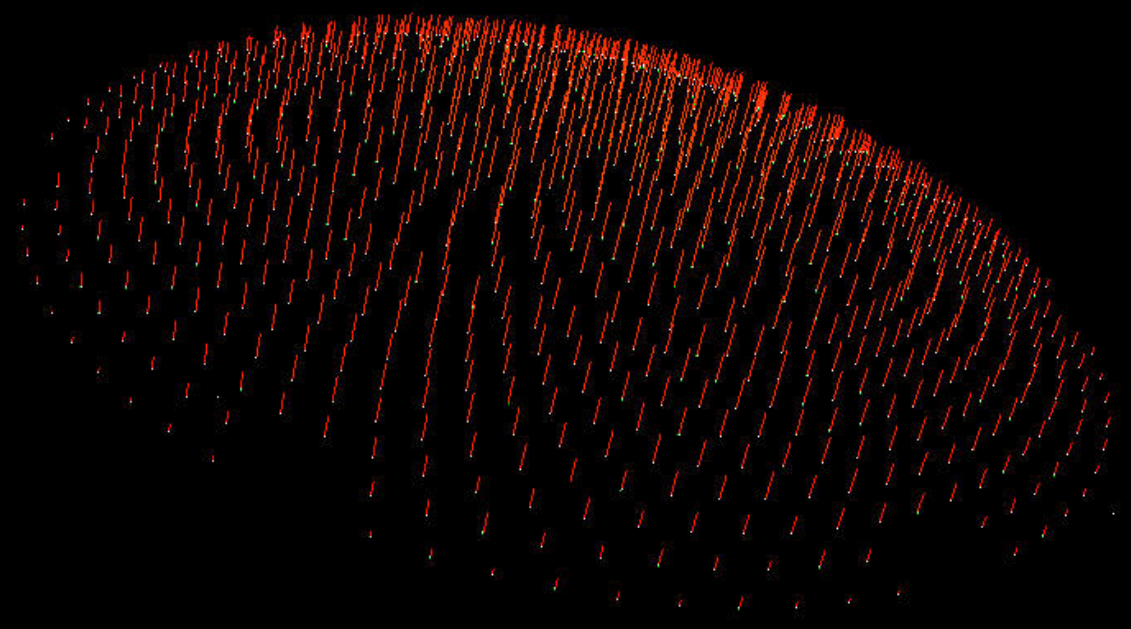
Window 3

Observe the linear rate of deformation evolve into a nonlinear rate after the Al yields...

020130 010psi

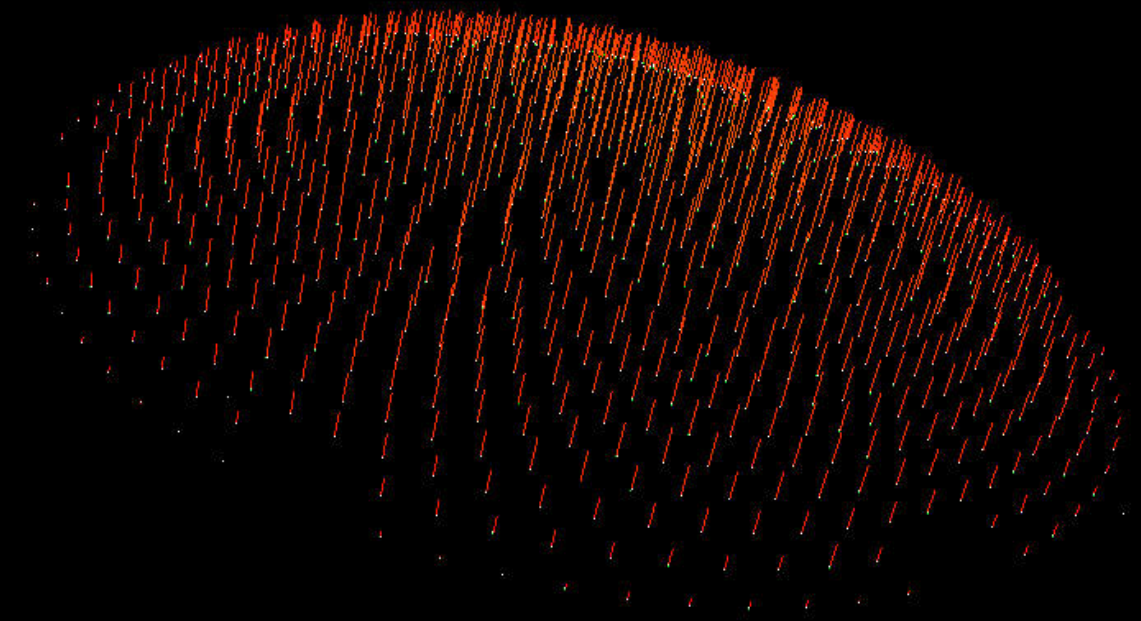


020130 015psi

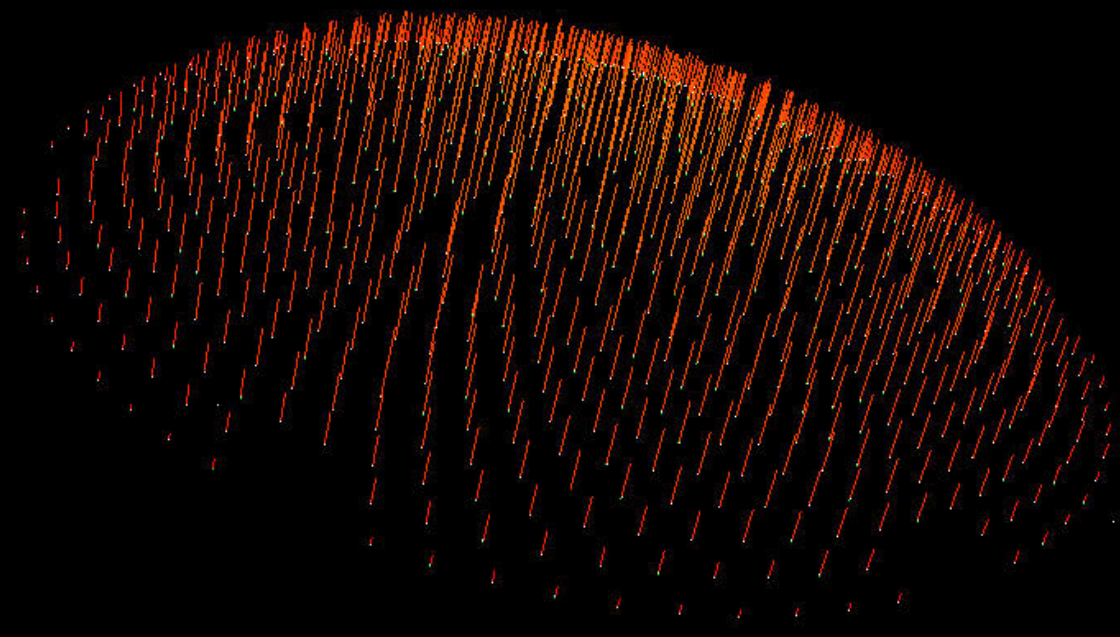




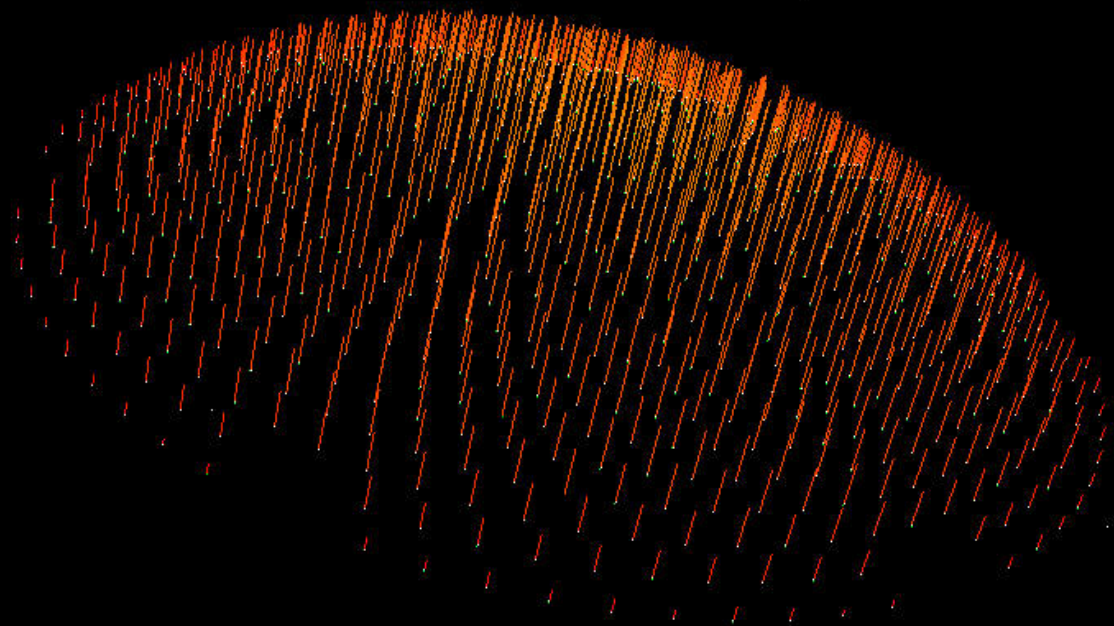
020130 020psi



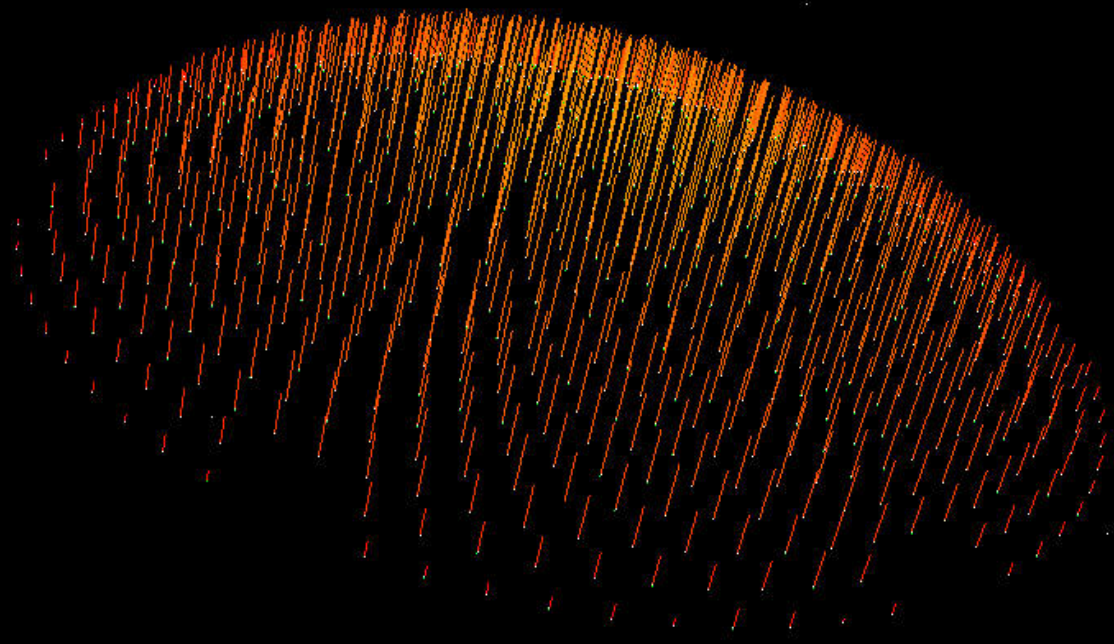
020130 025psi



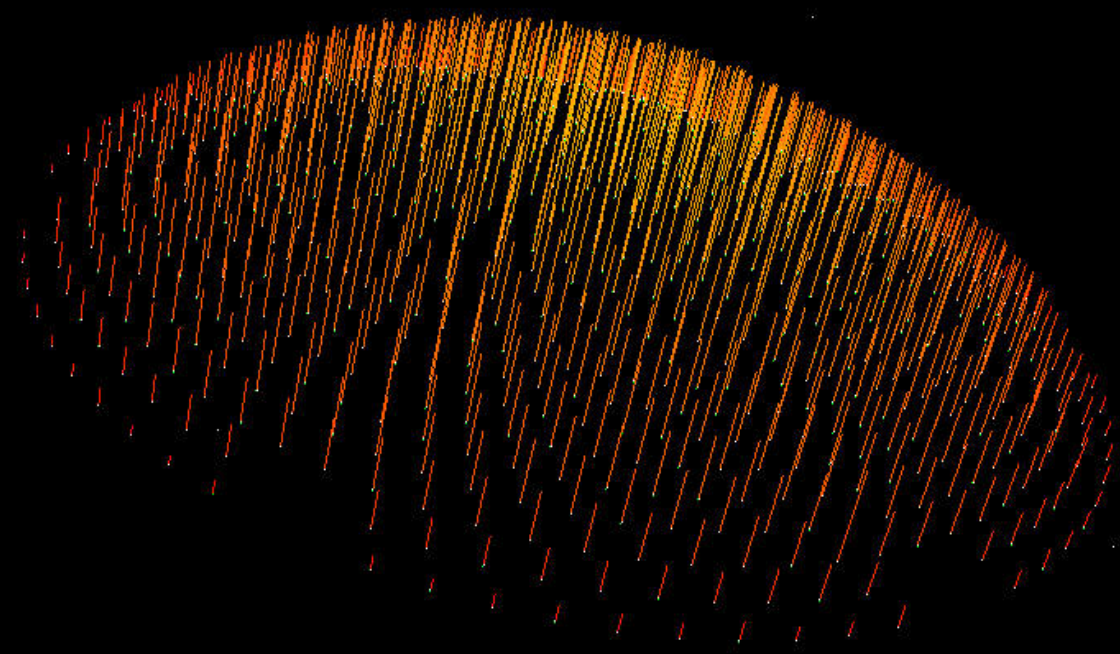
020130 030psi



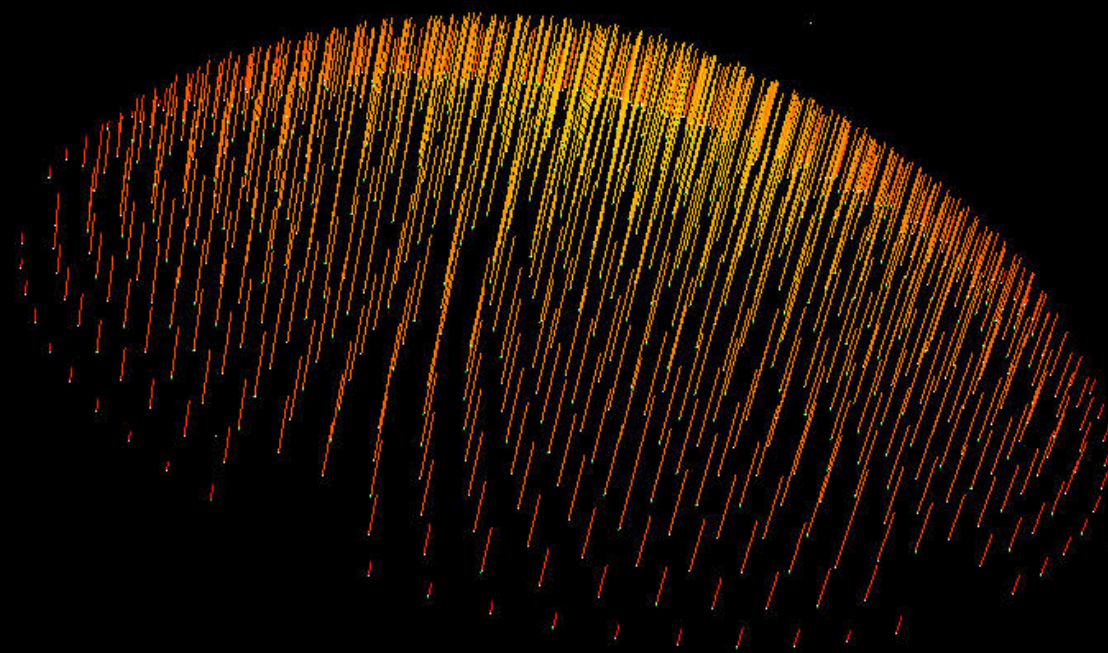
020130 035psi



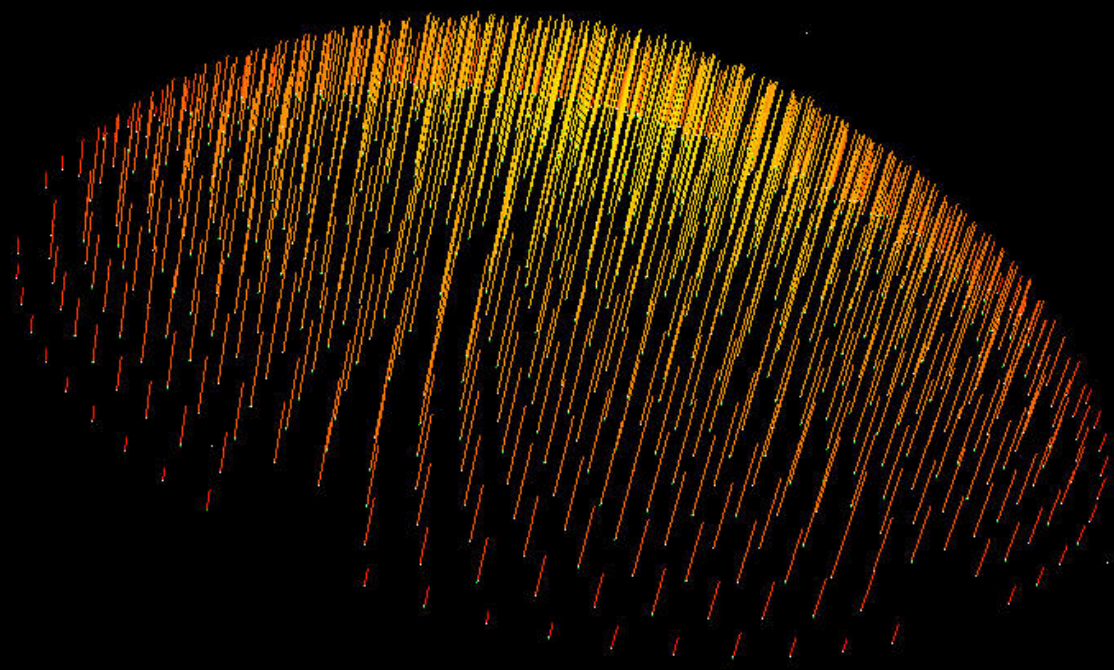
020130 040psi



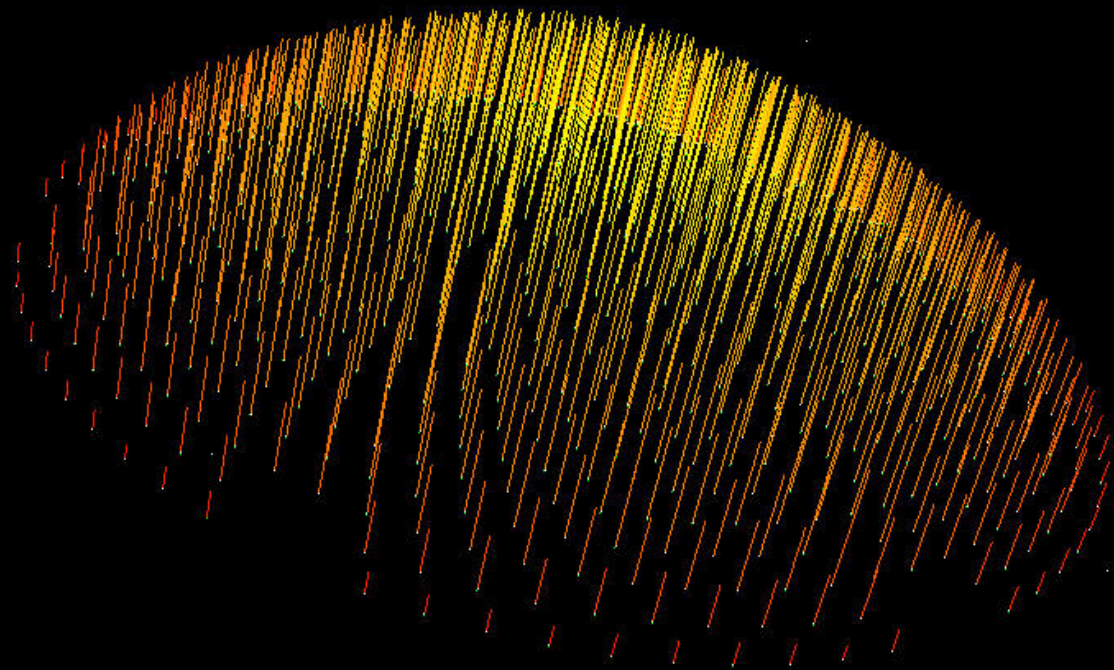
020130 045psi



020130 050psi

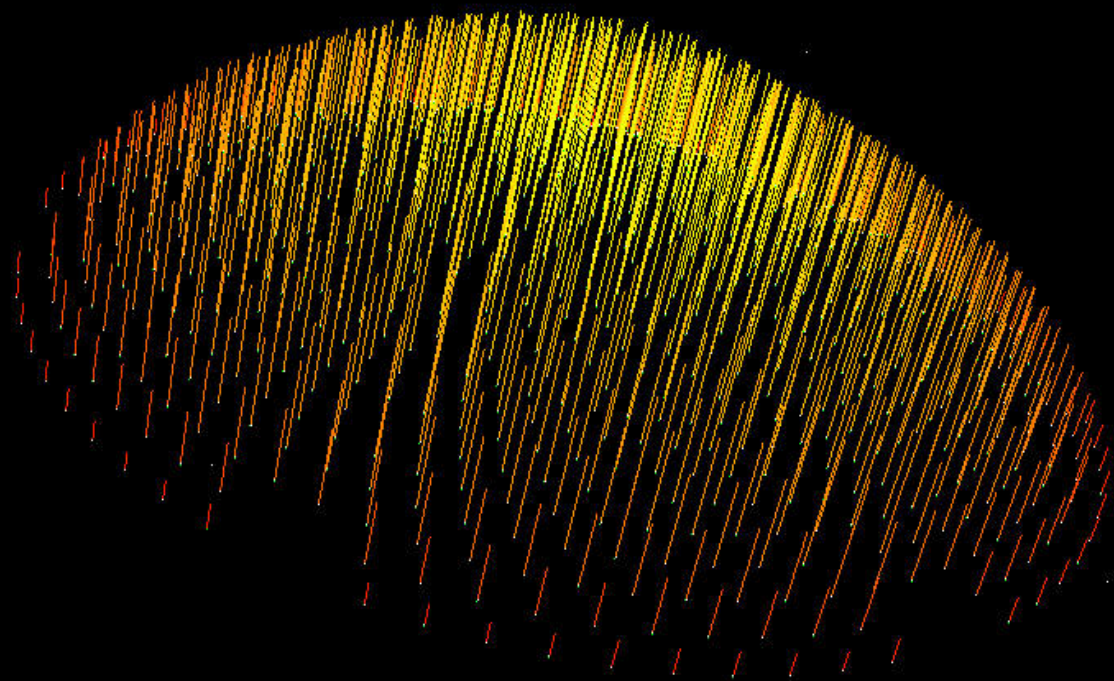


020130 055psi

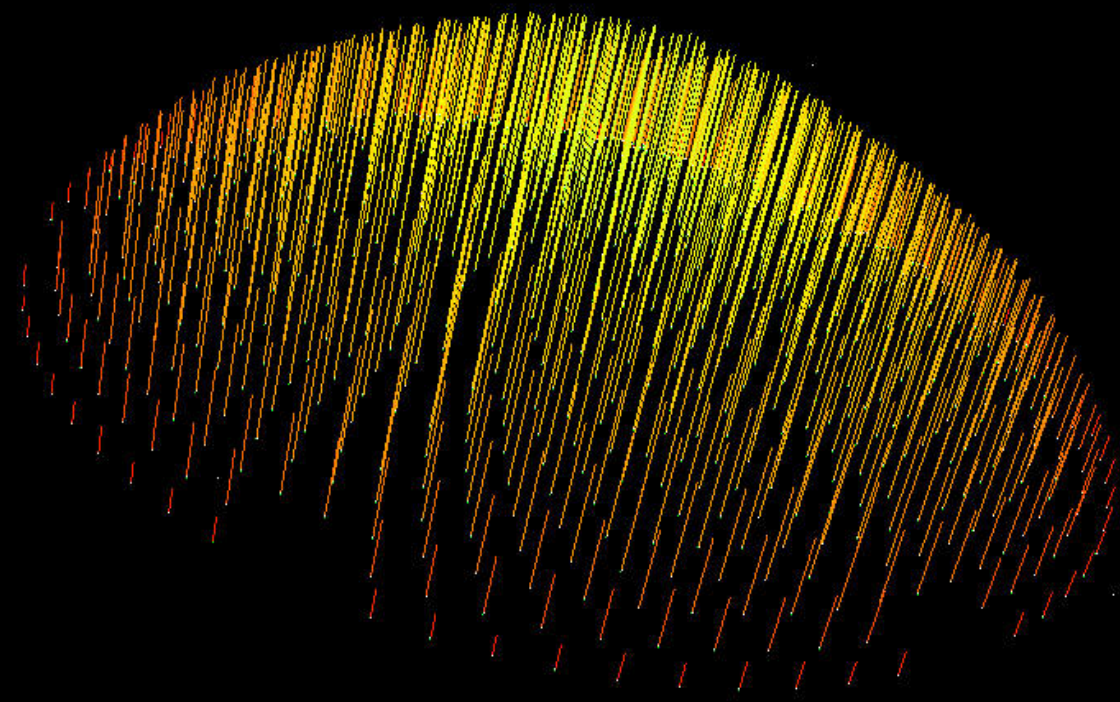




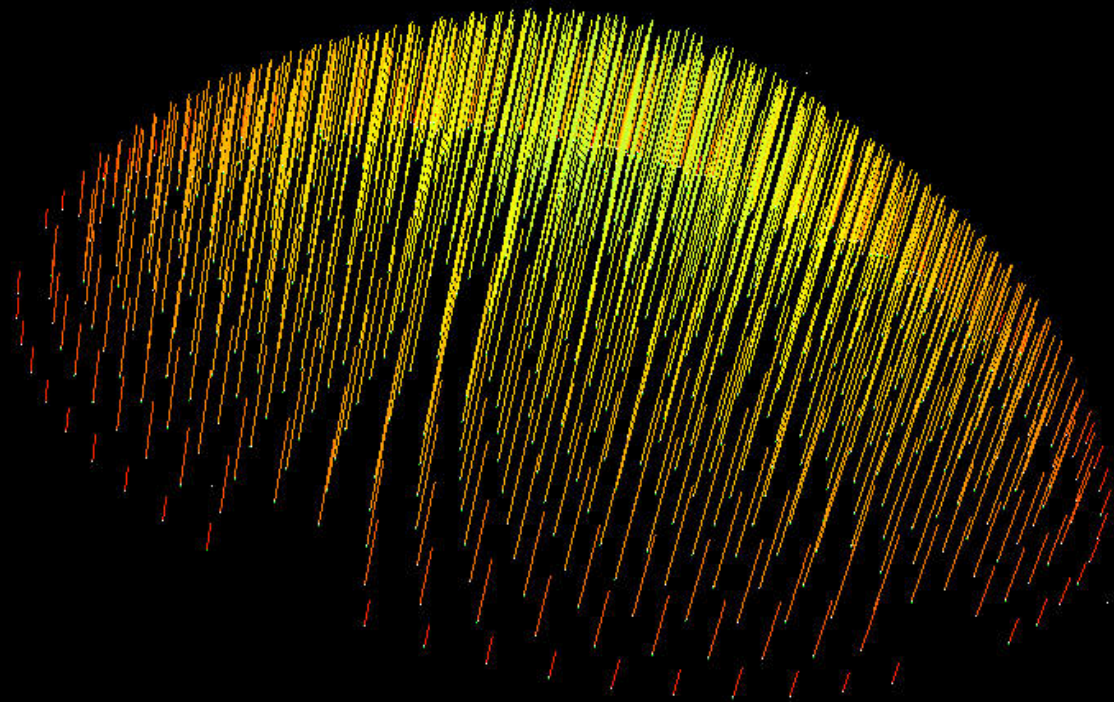
020130 060psi



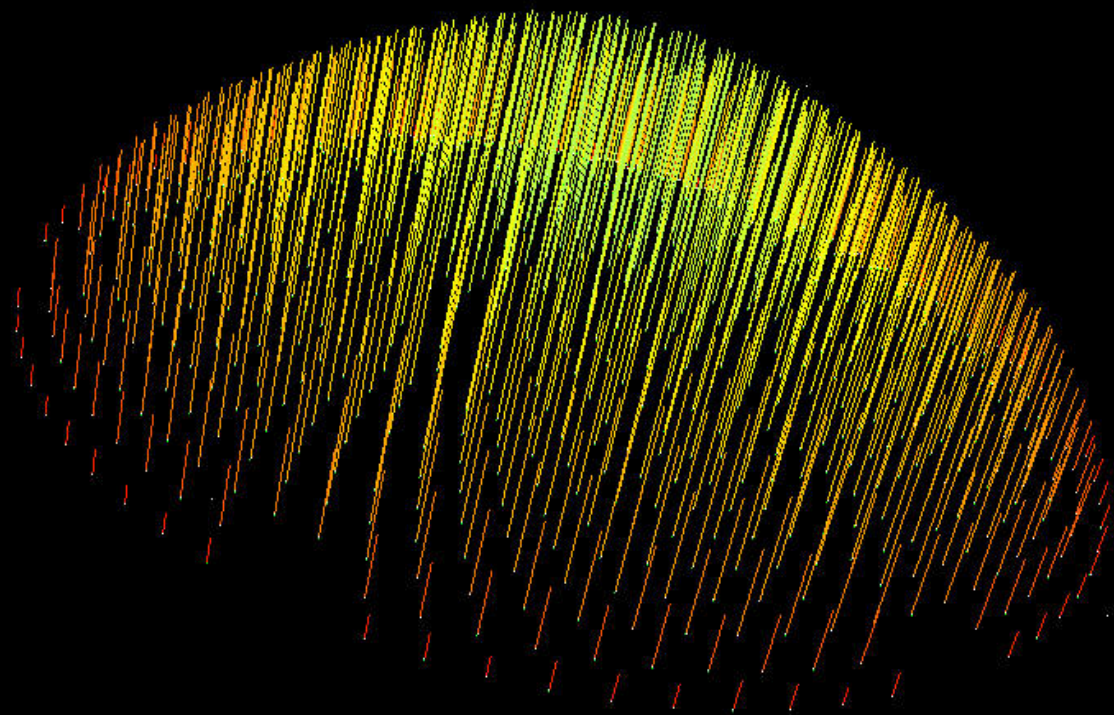
020130 065psi



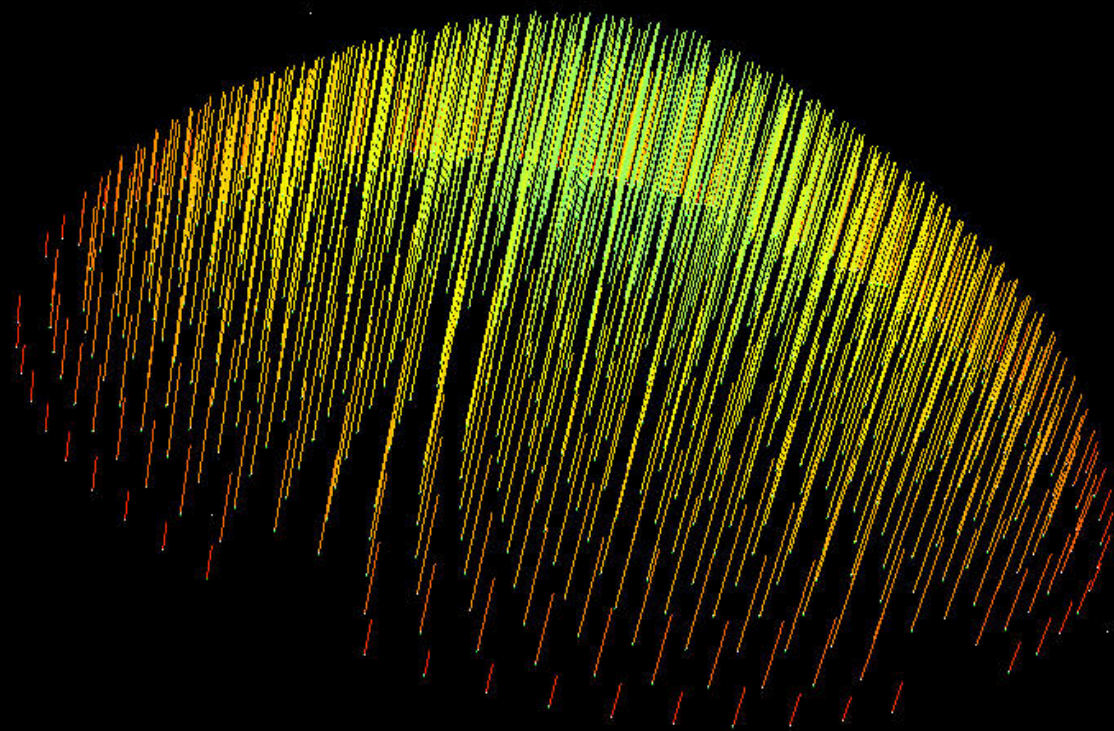
020130 070psi



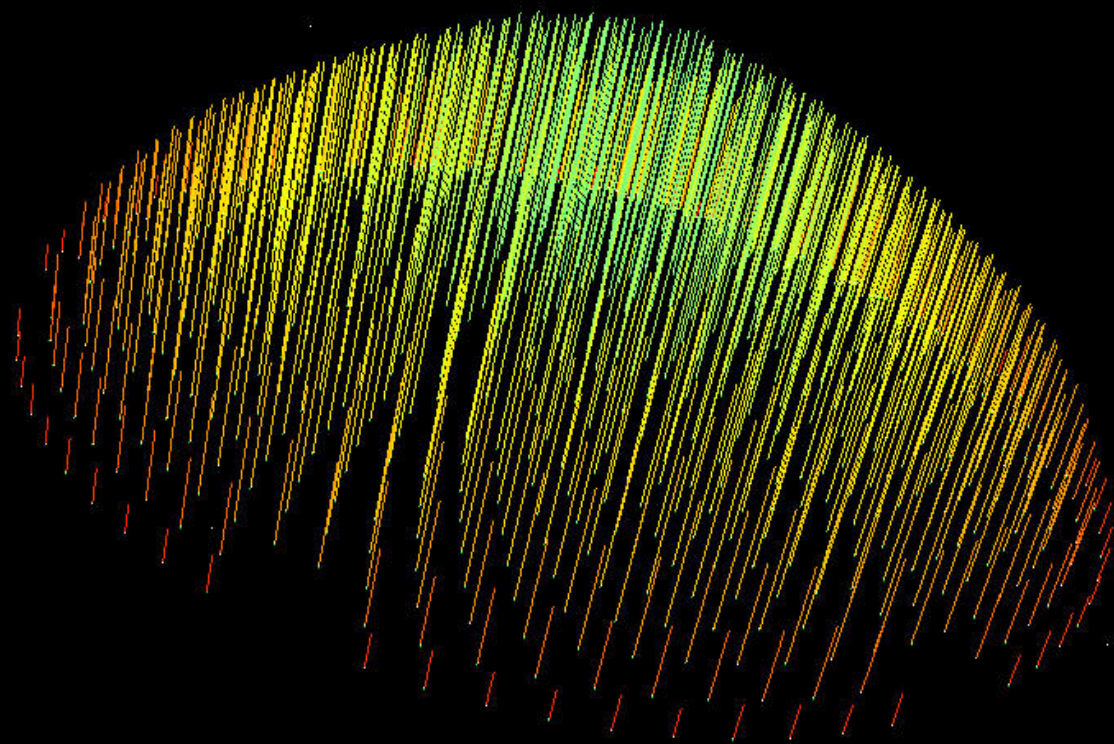
020130 075psi



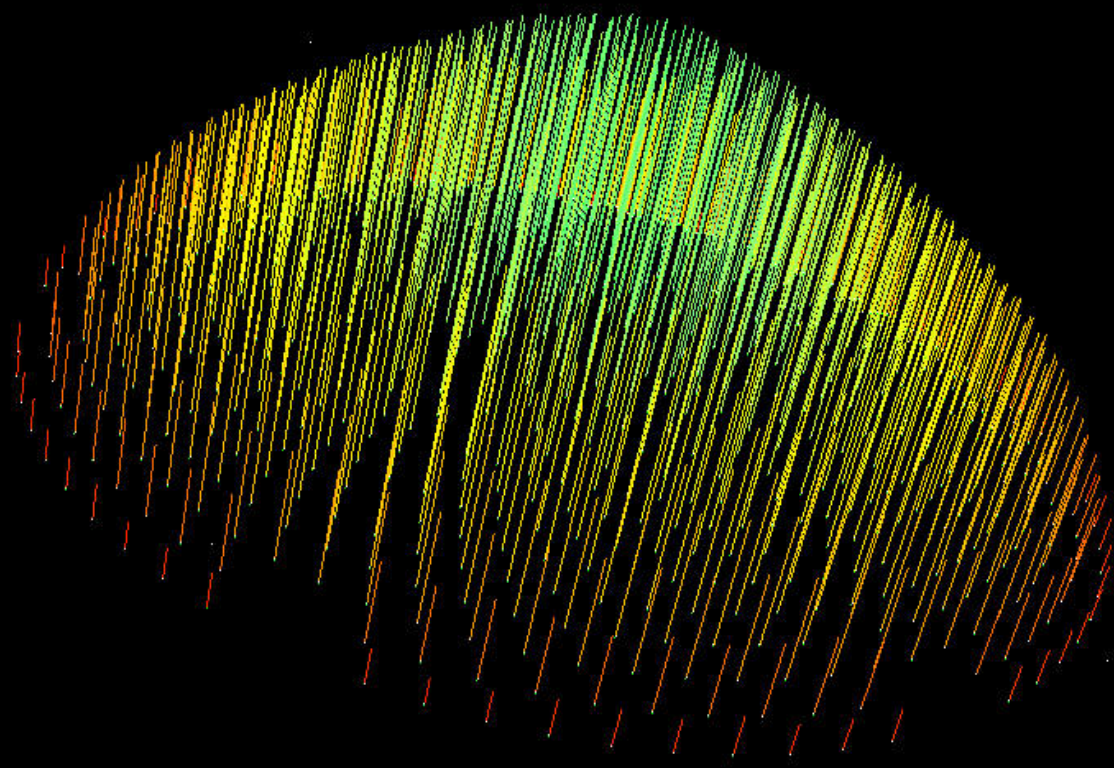
020130 080psi



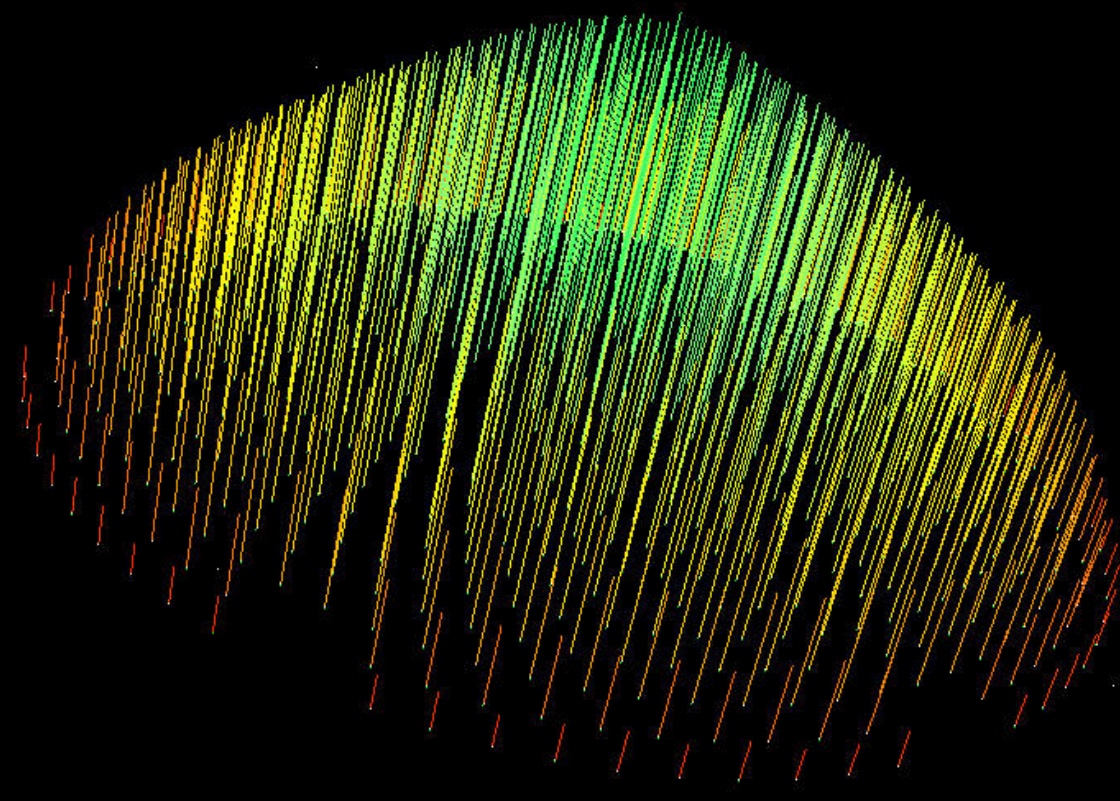
020130 085psi



020130\_090psi

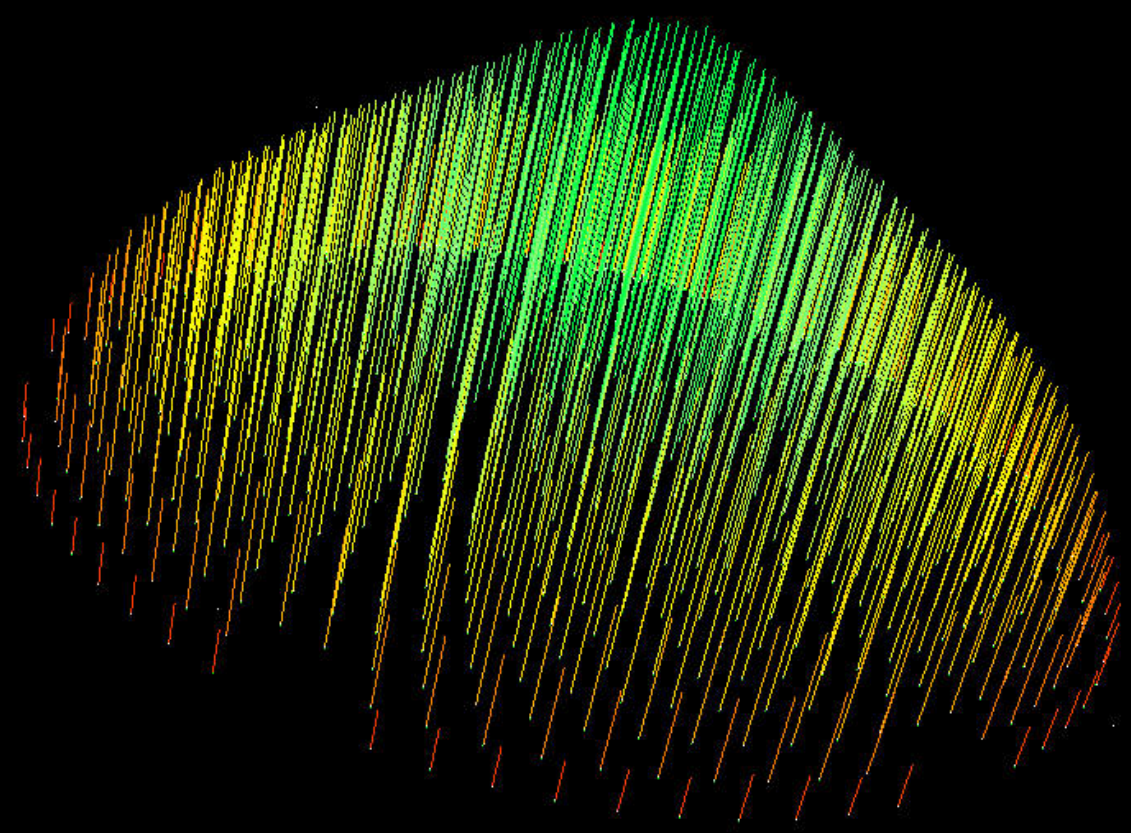


020130 095psi

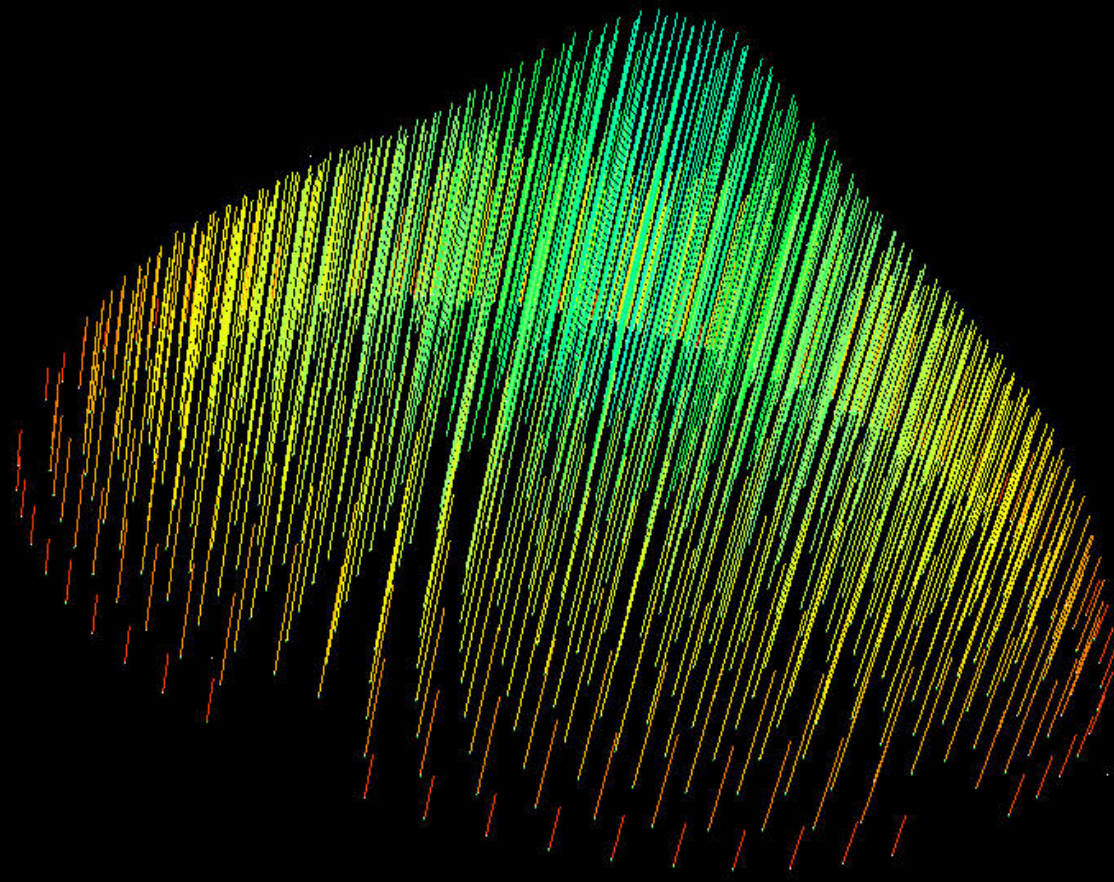




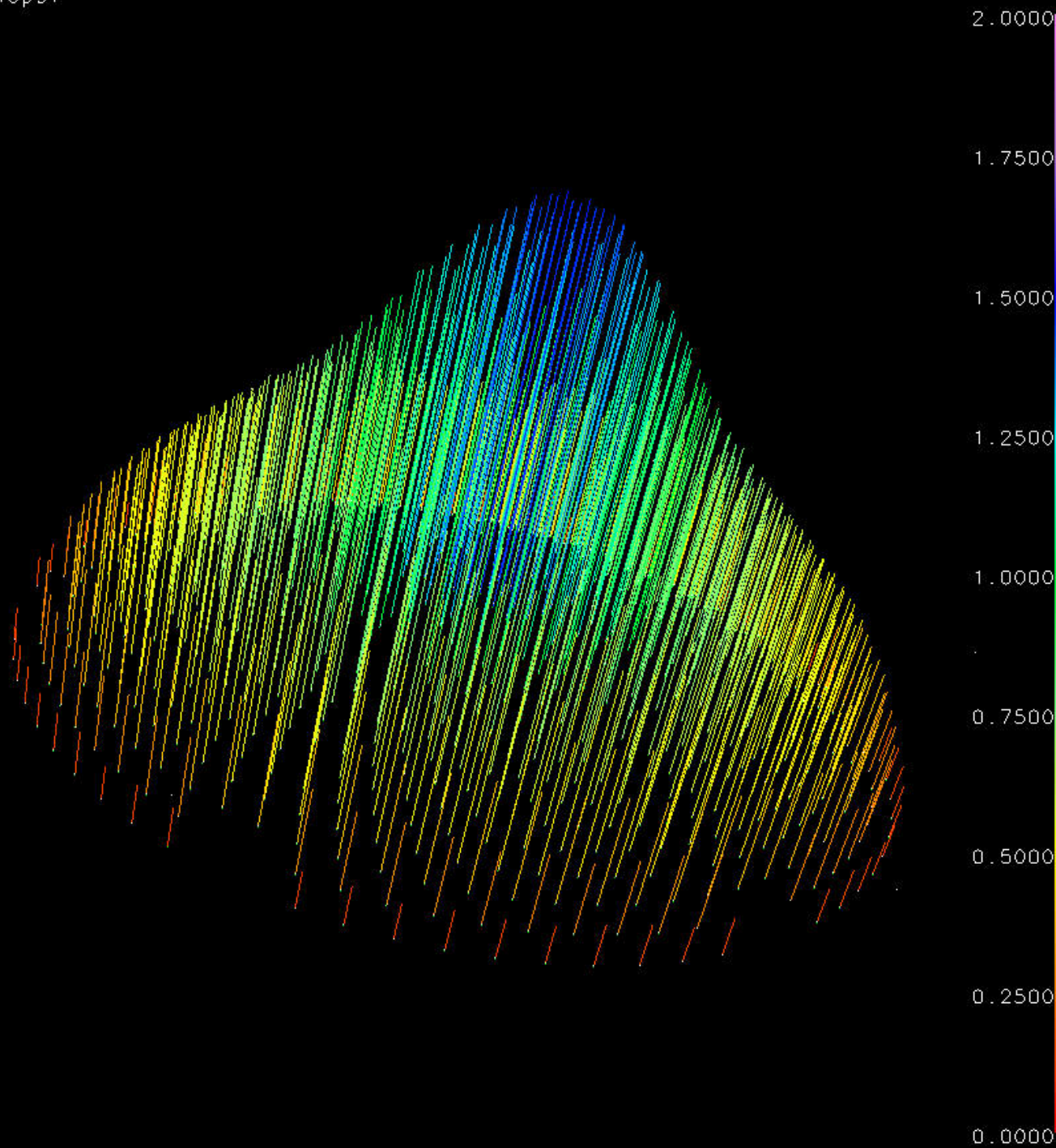
020130 100psi



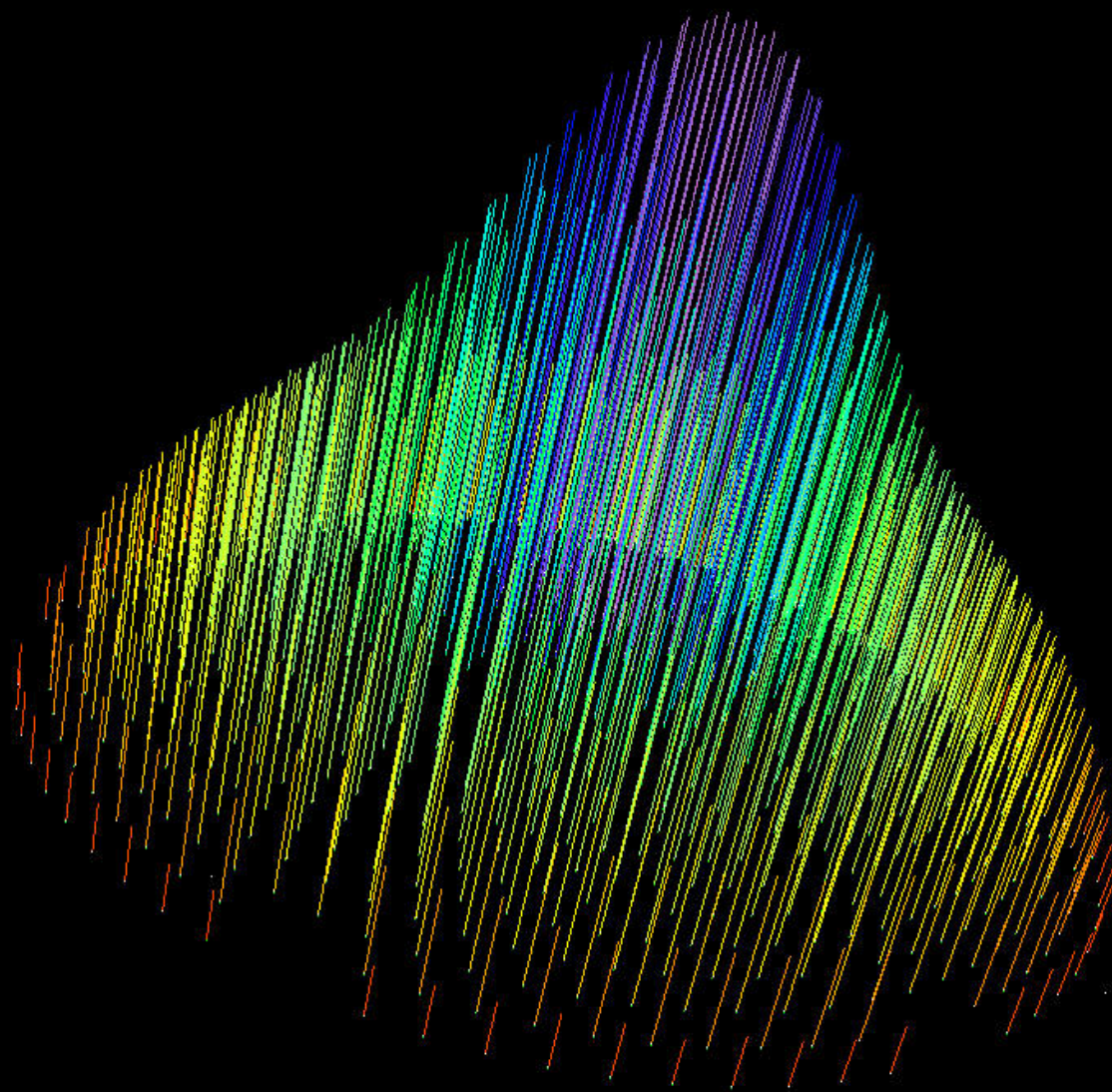
020130 105psi



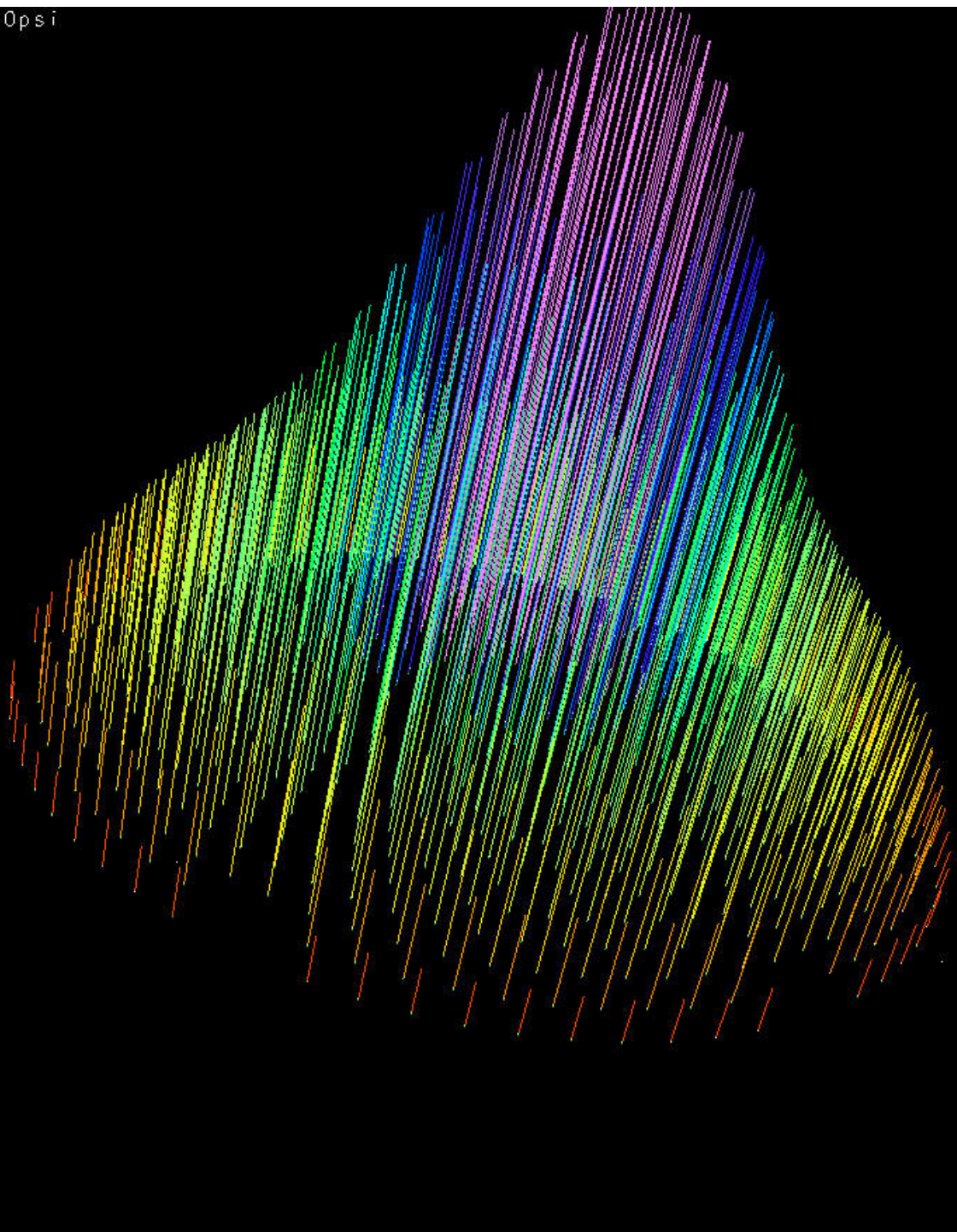
020130 110psi

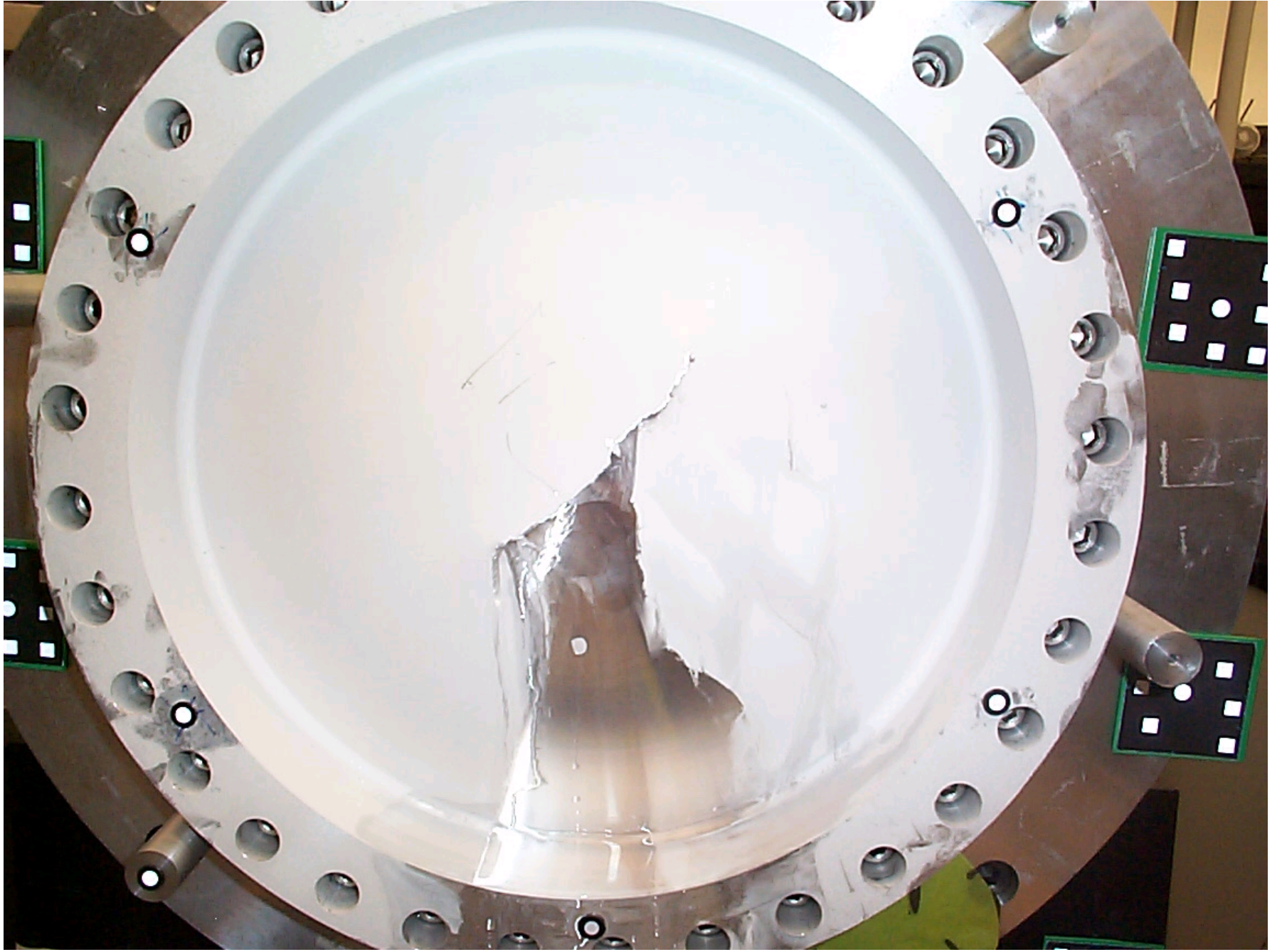


020130 115psi



020130 120psi

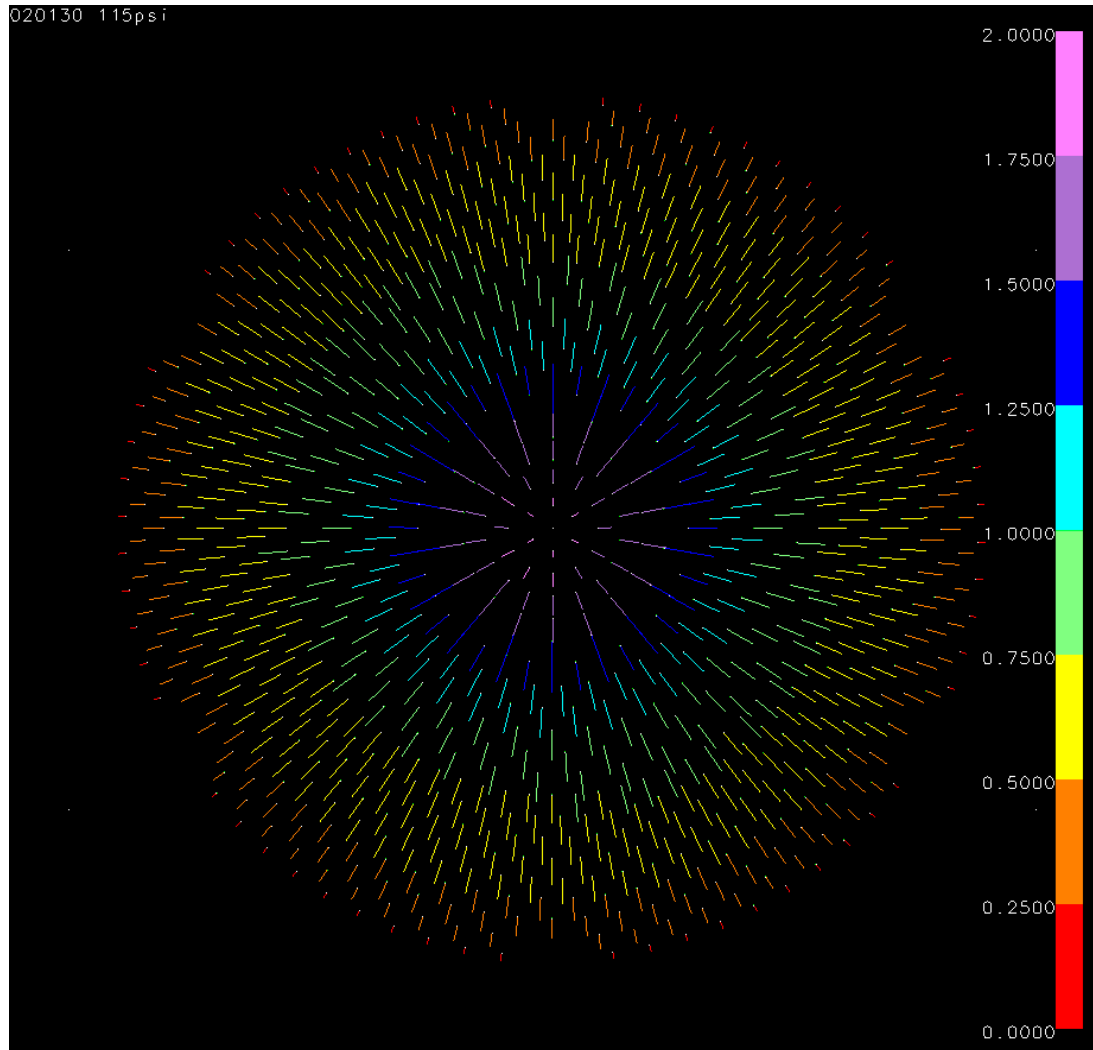




# Symmetry

By plotting the *change* from initial shape, any asymmetry due to pattern or window eccentricity is removed.

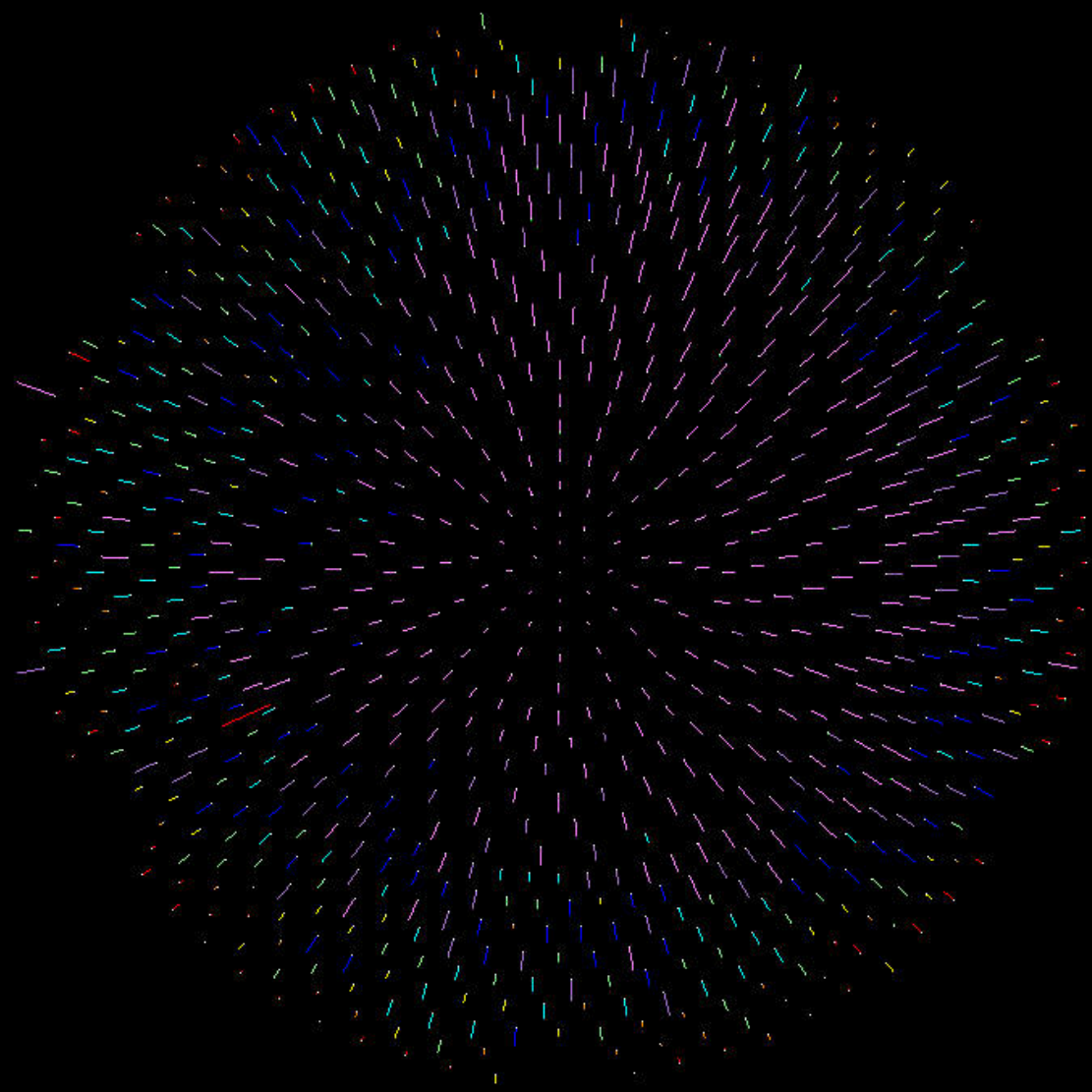
What's left is  $f(\text{pressure})$ .



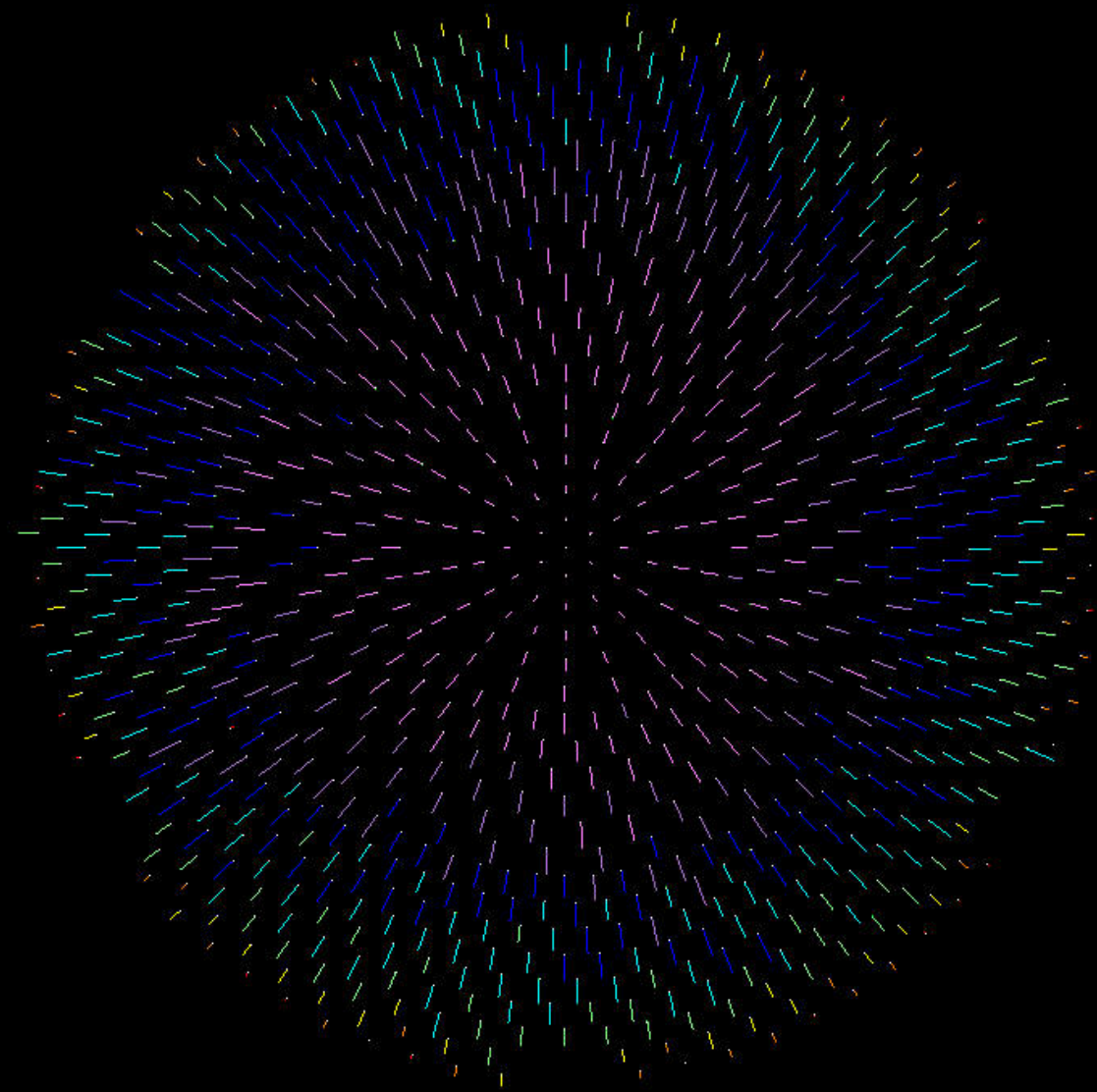
Observe the whisker plots to check for any asymmetry in the deformation of the window as the pressure is increased...



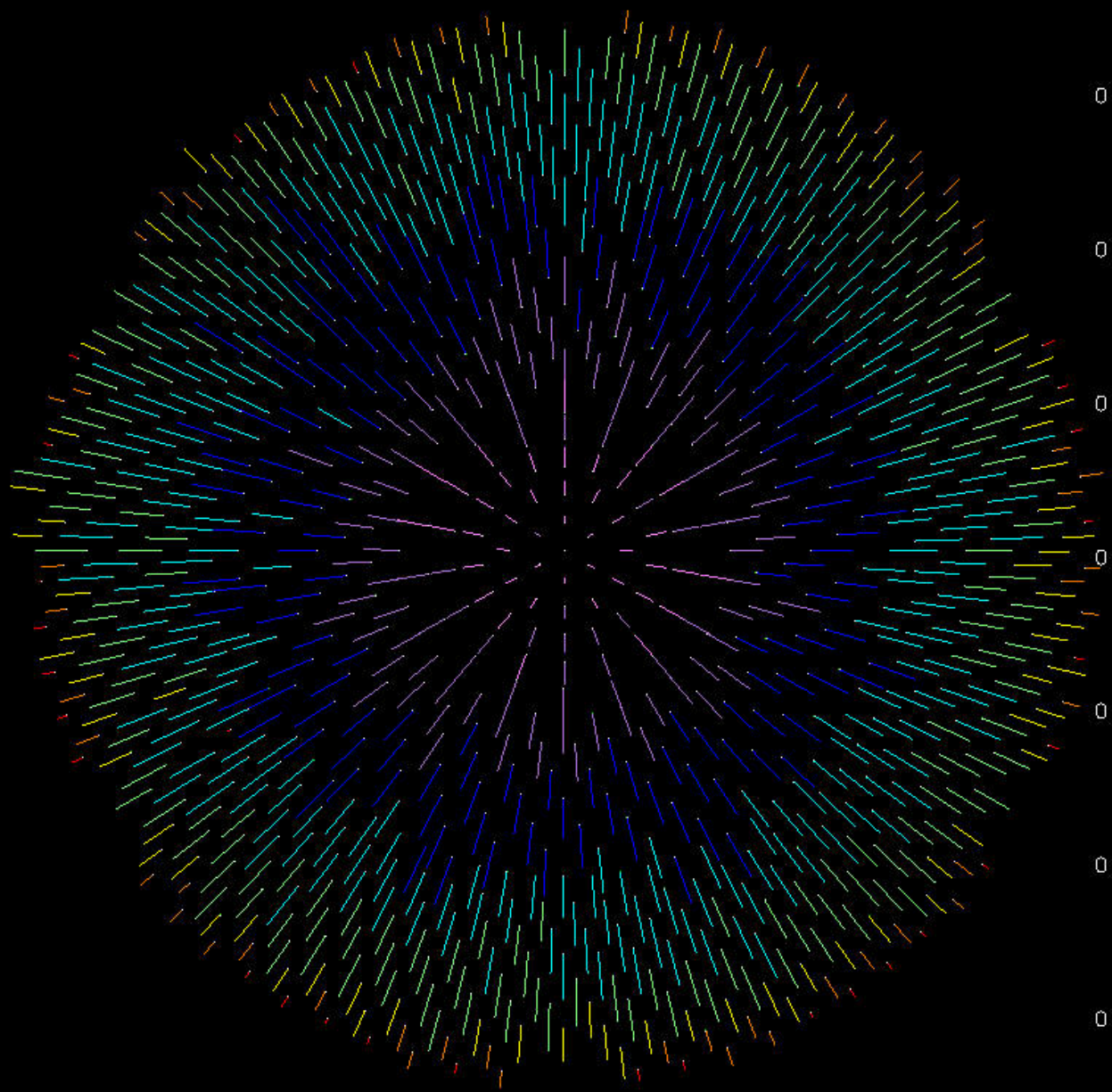
020130 005psi



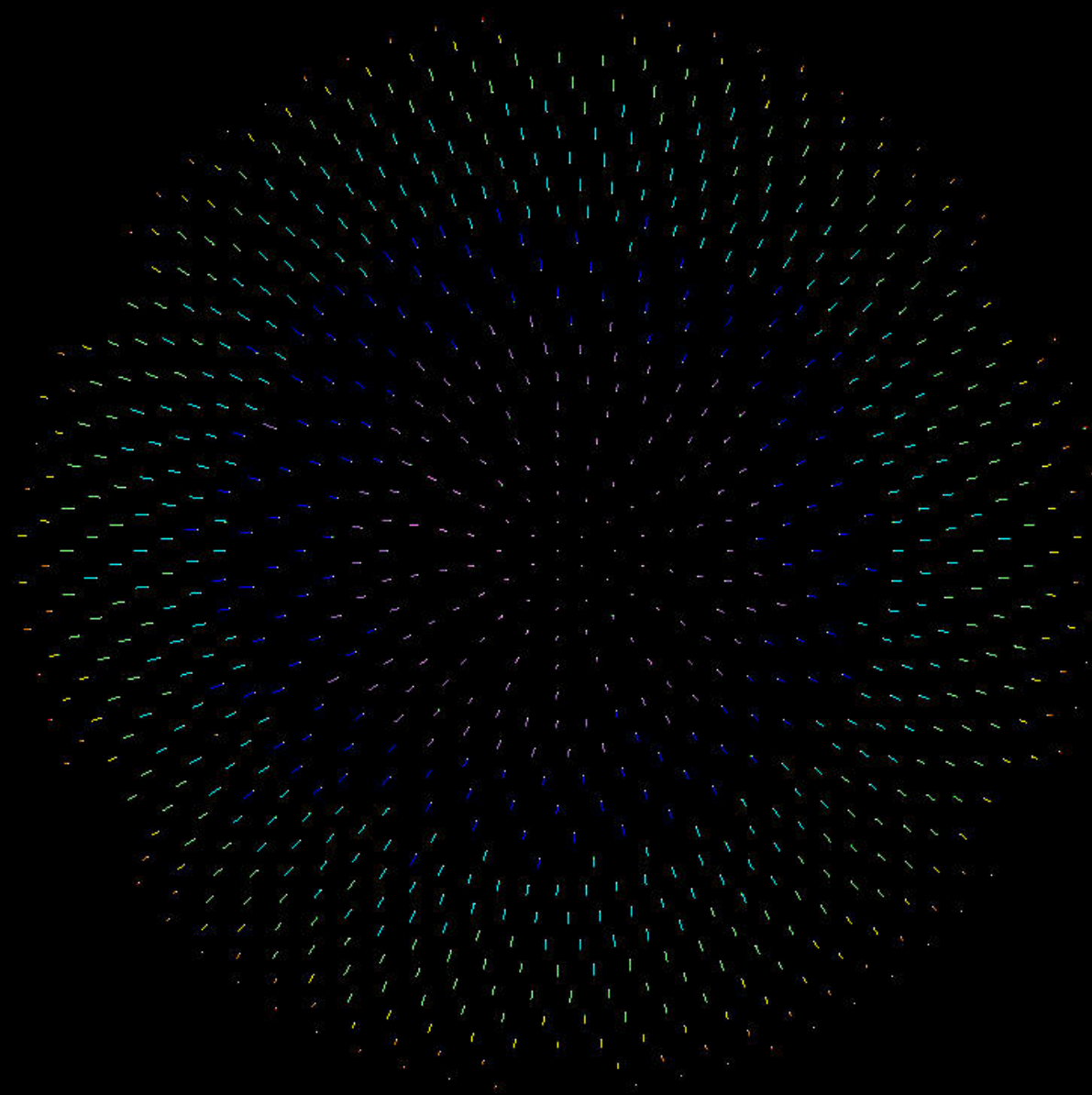
020130 010psi



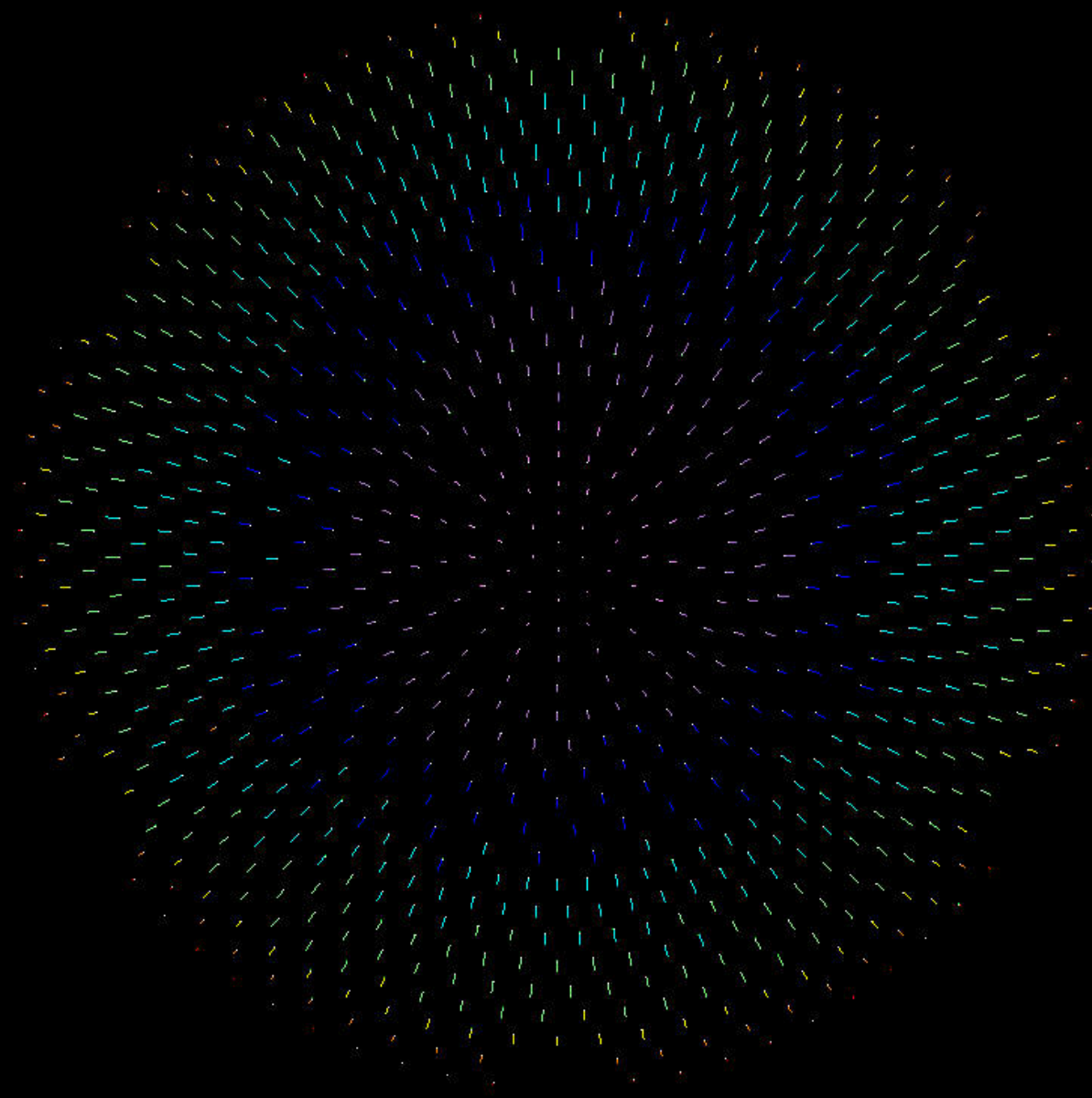
020130 015psi



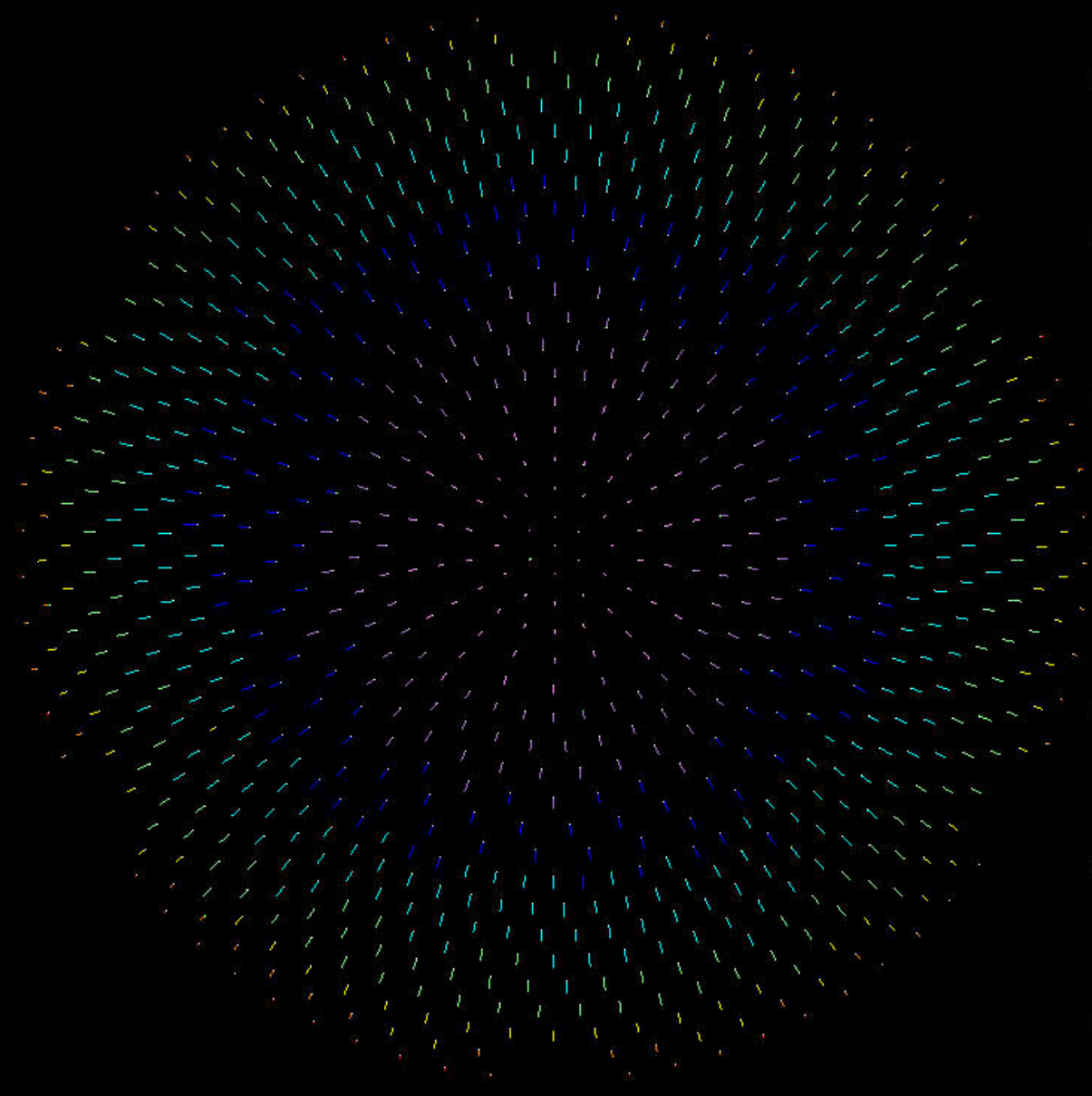
020130 020psi



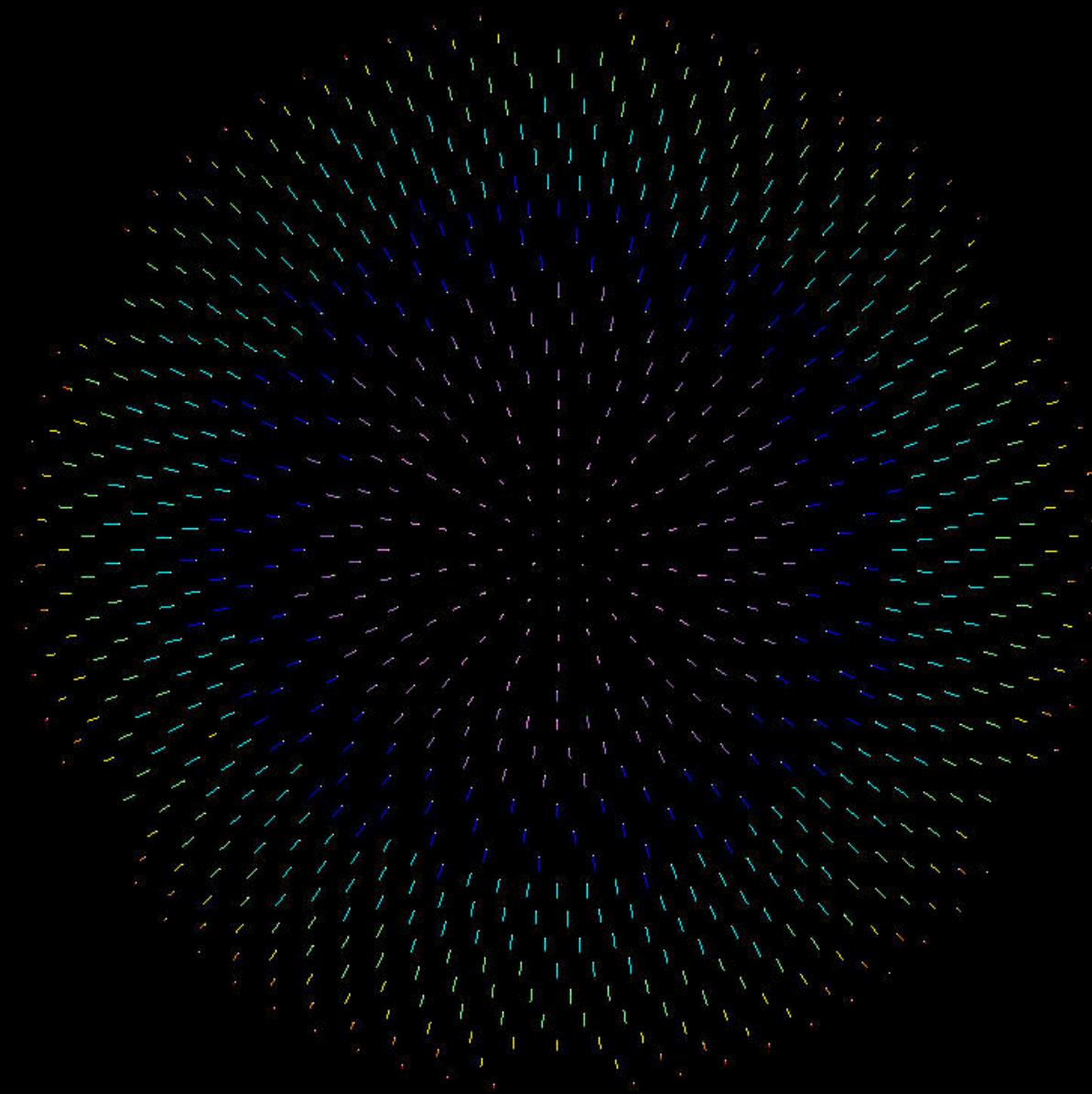
020130 025psi



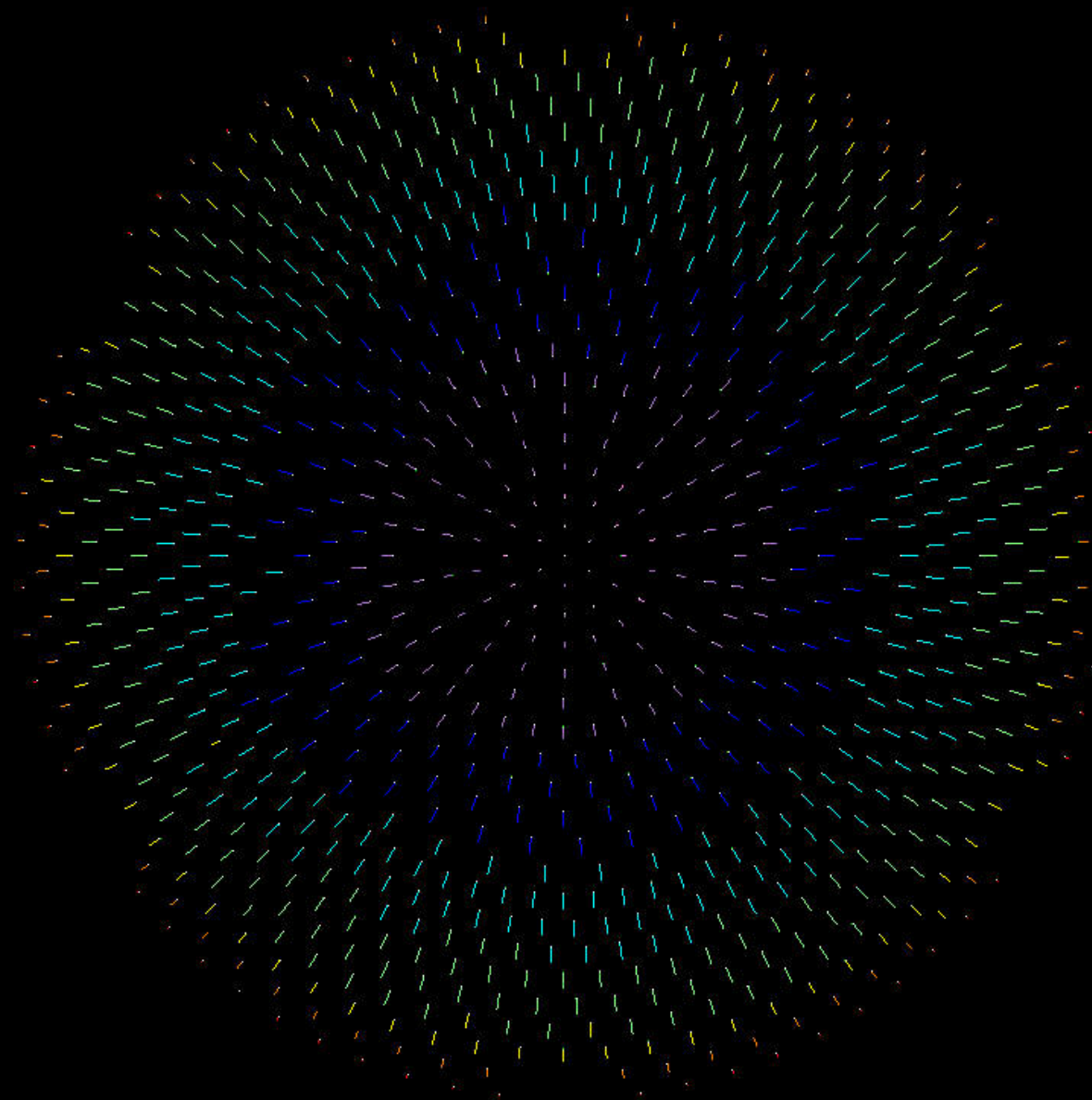
020130 030psi



020130 035psi

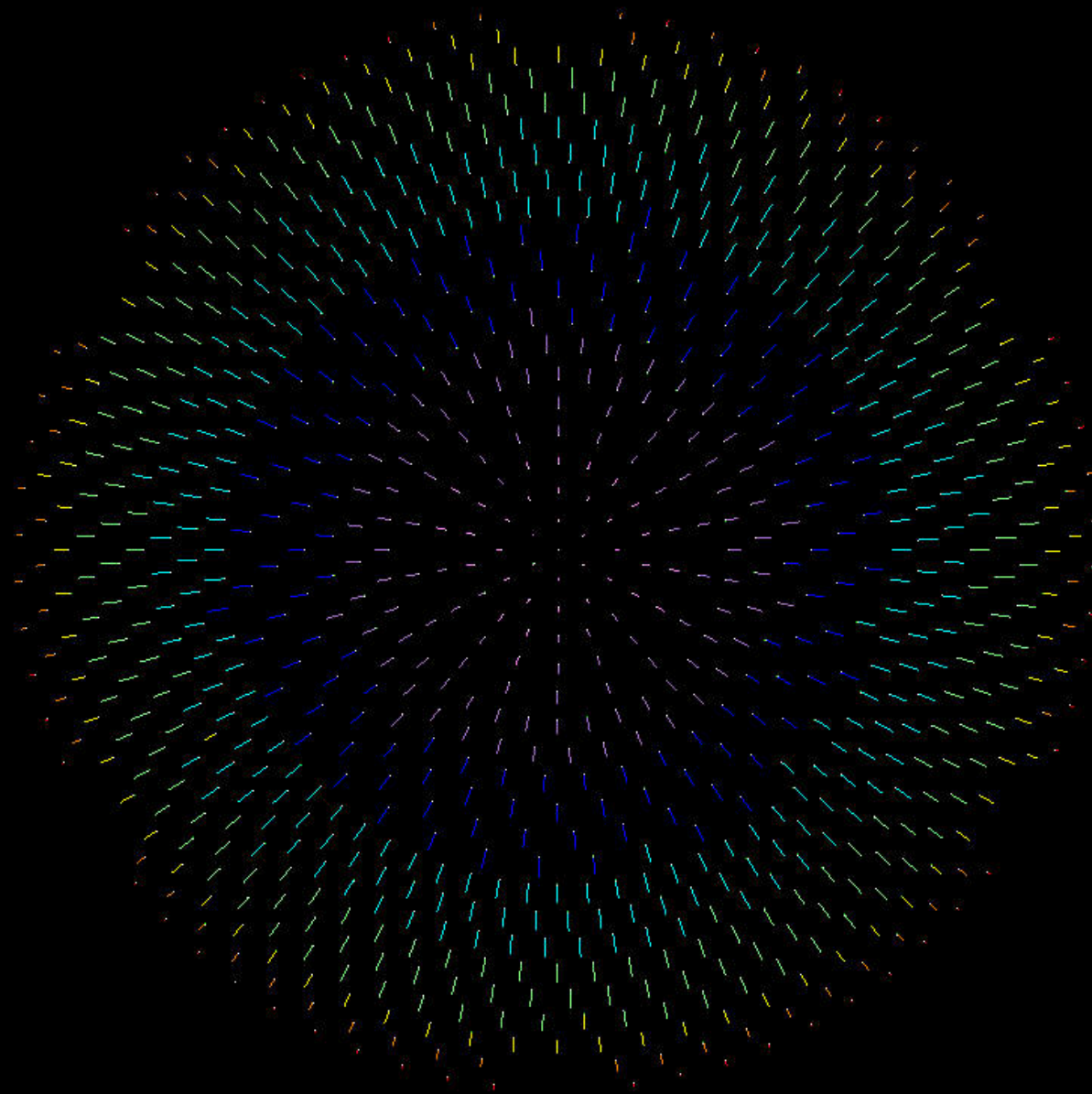


020130 040psi

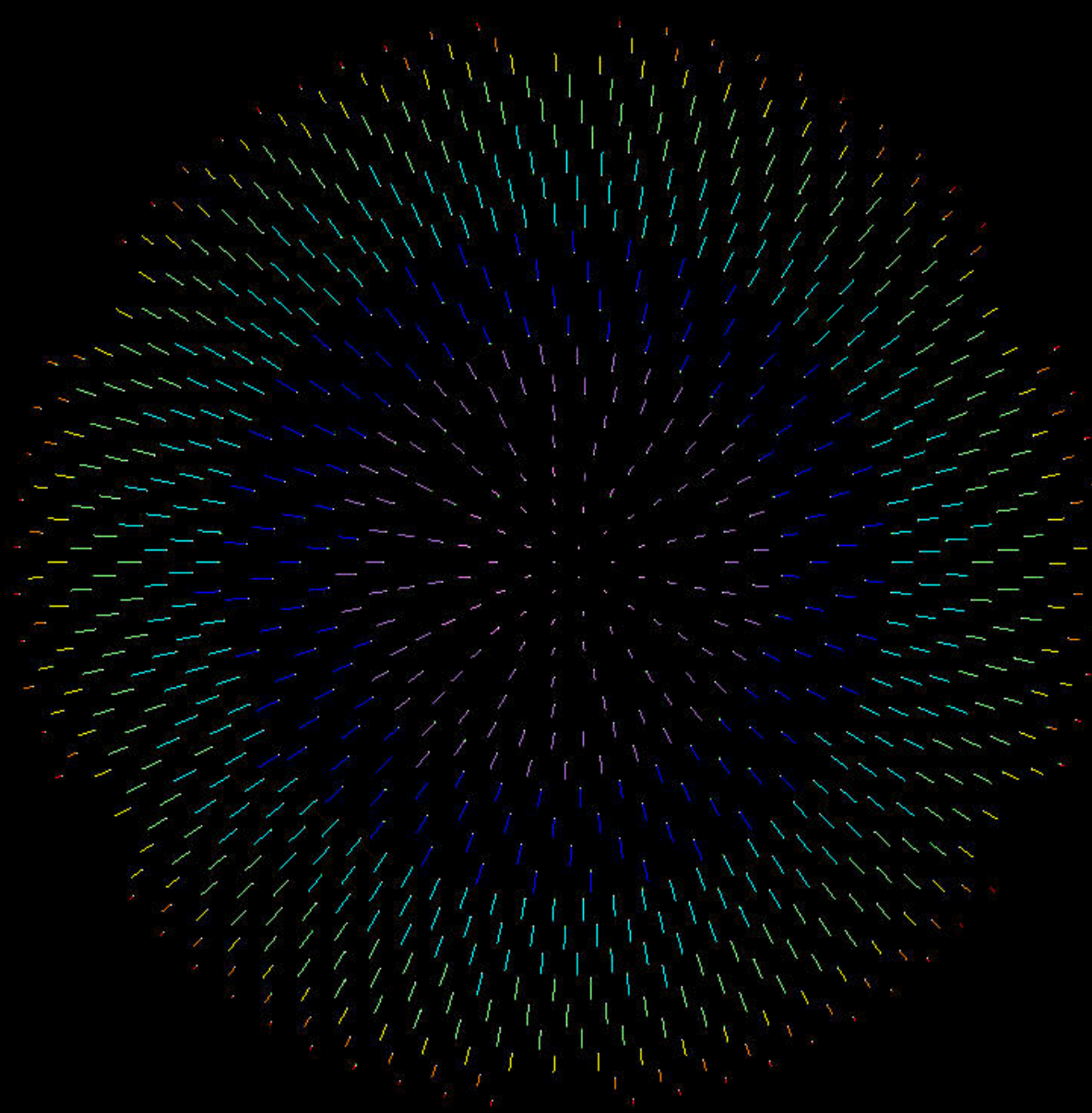




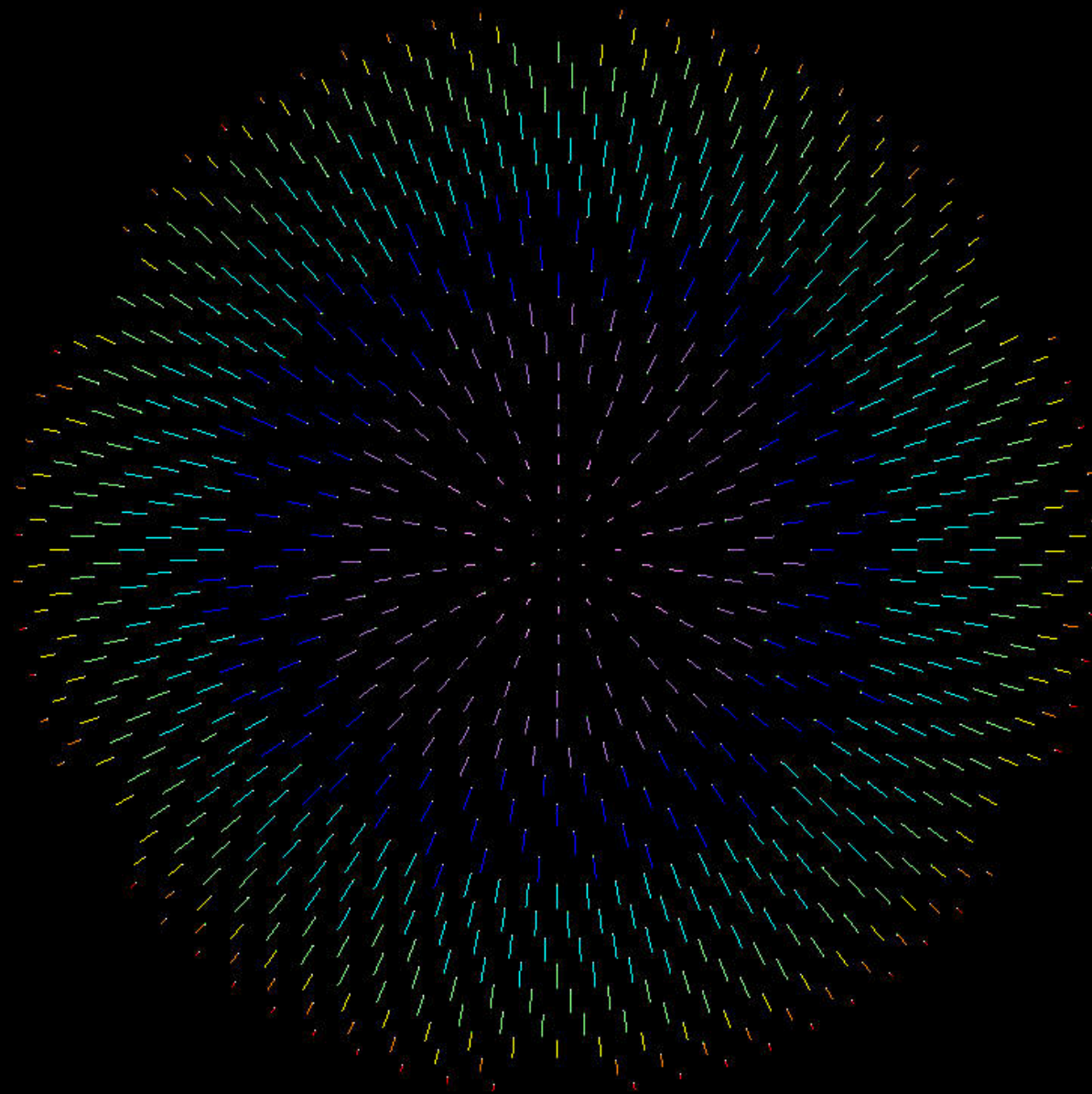
020130 045psi



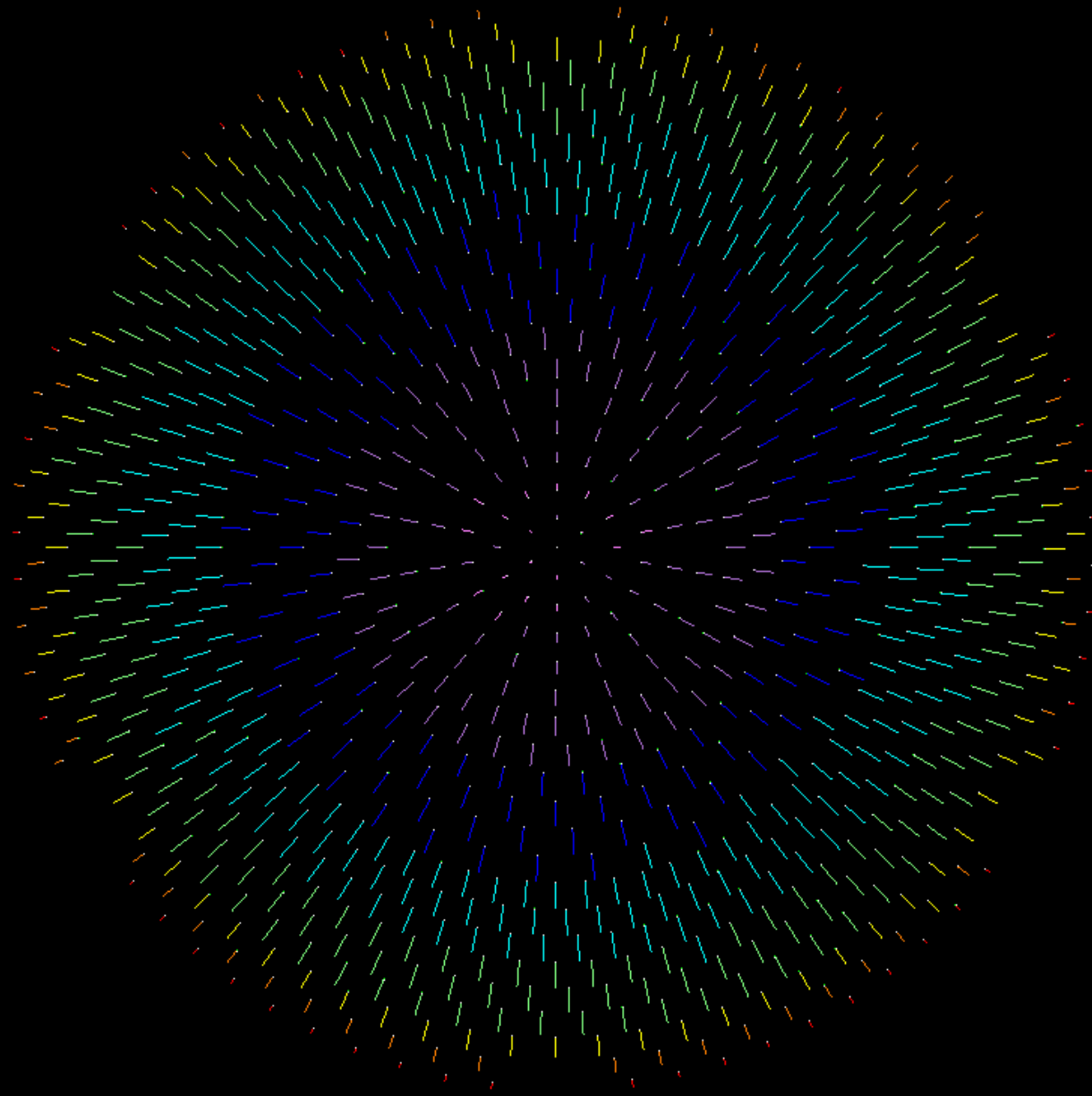
020130 050psi



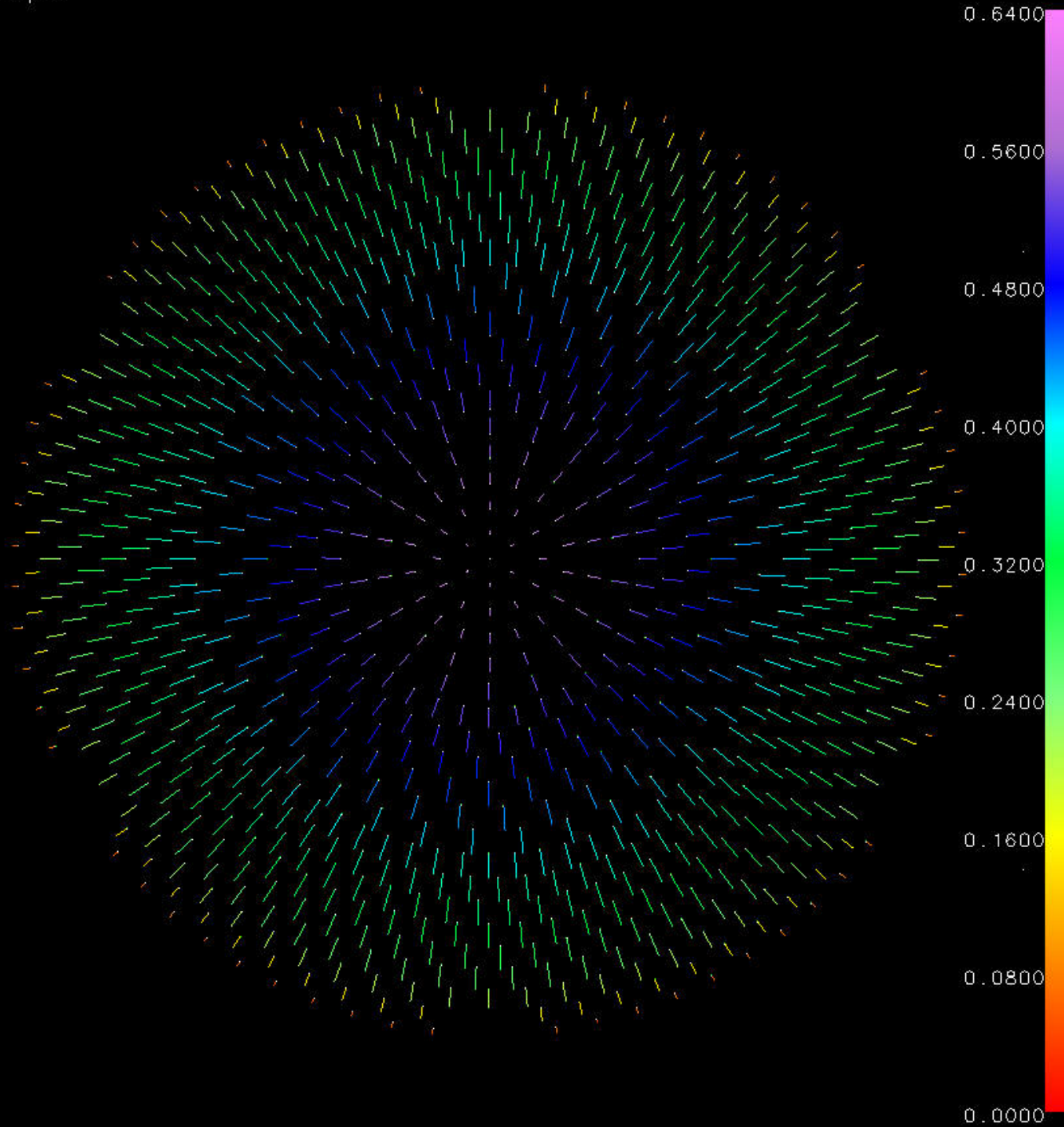
020130 055psi



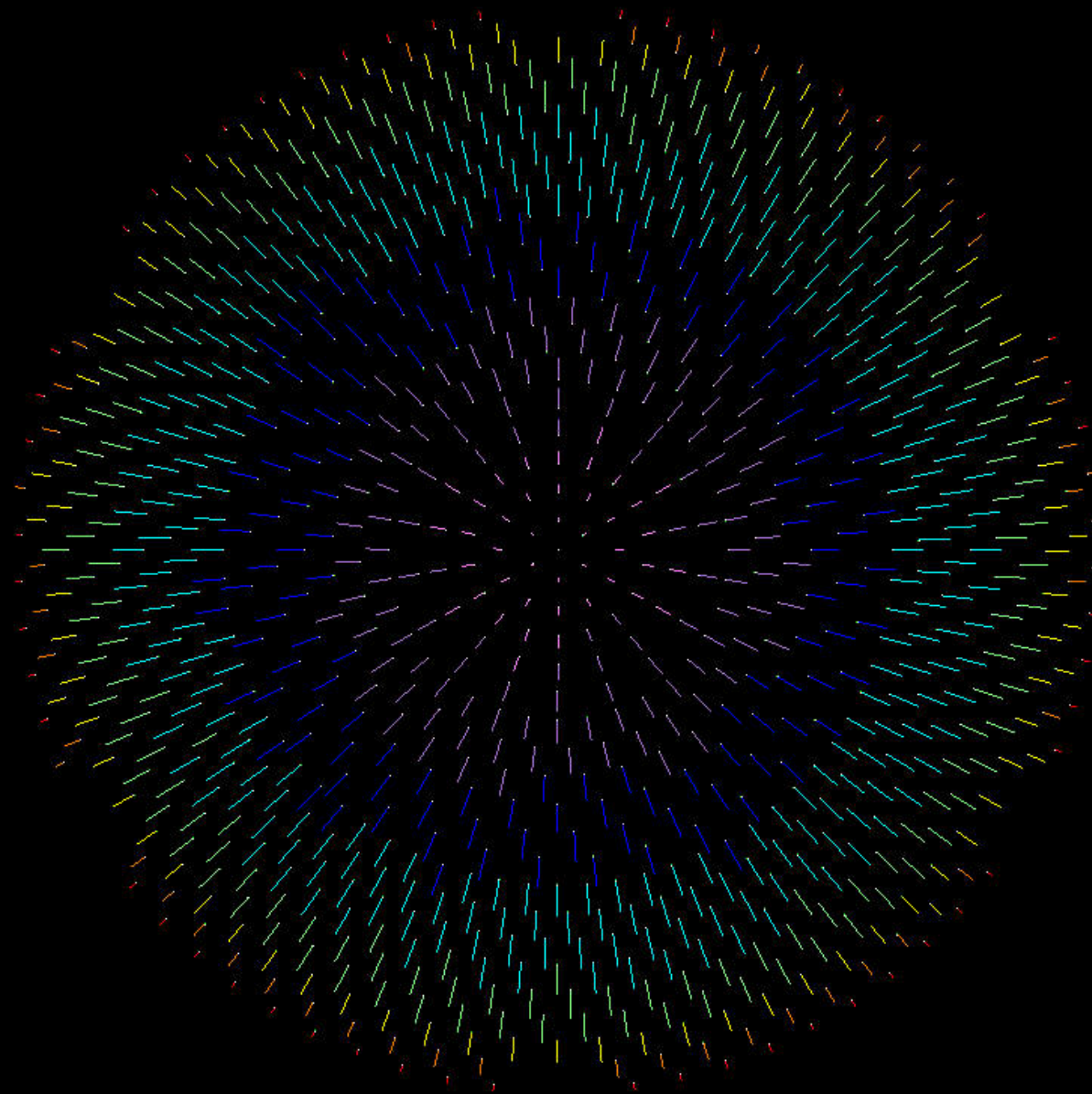
020130 060psi



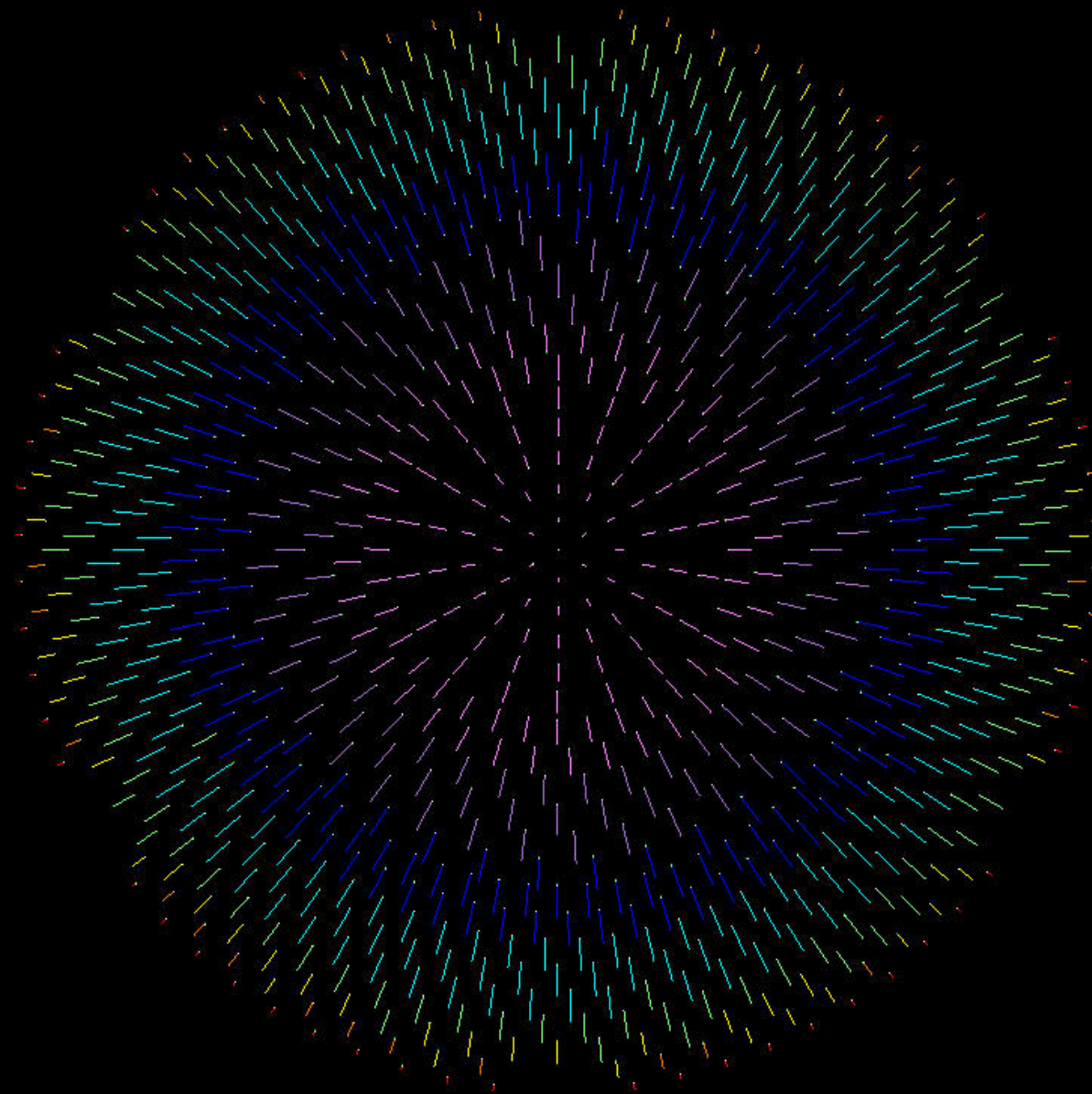
020130 065psi



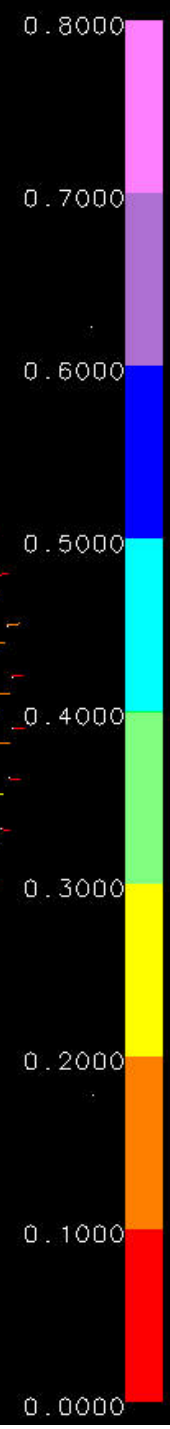
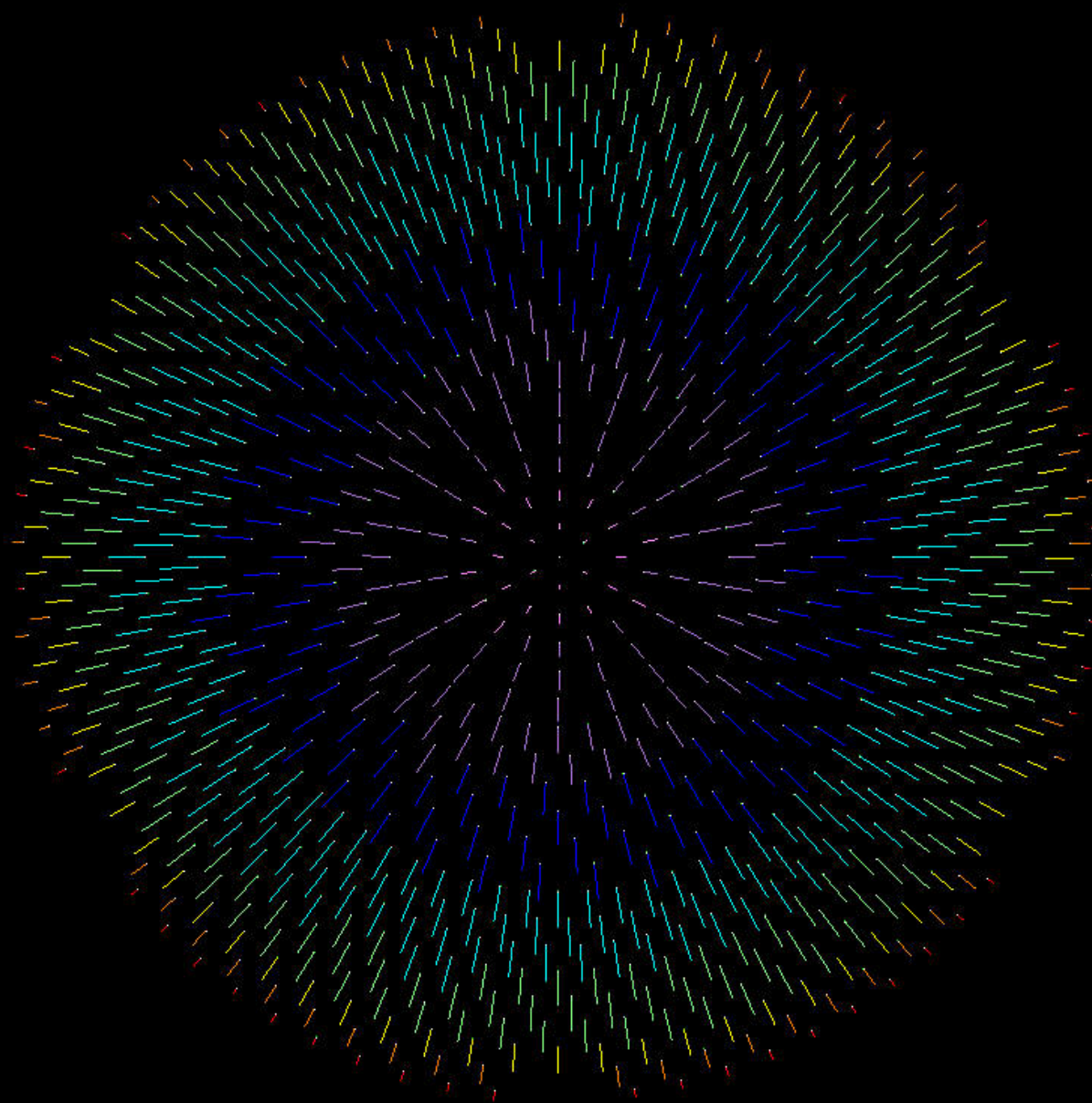
020130 070psi



020130 075psi

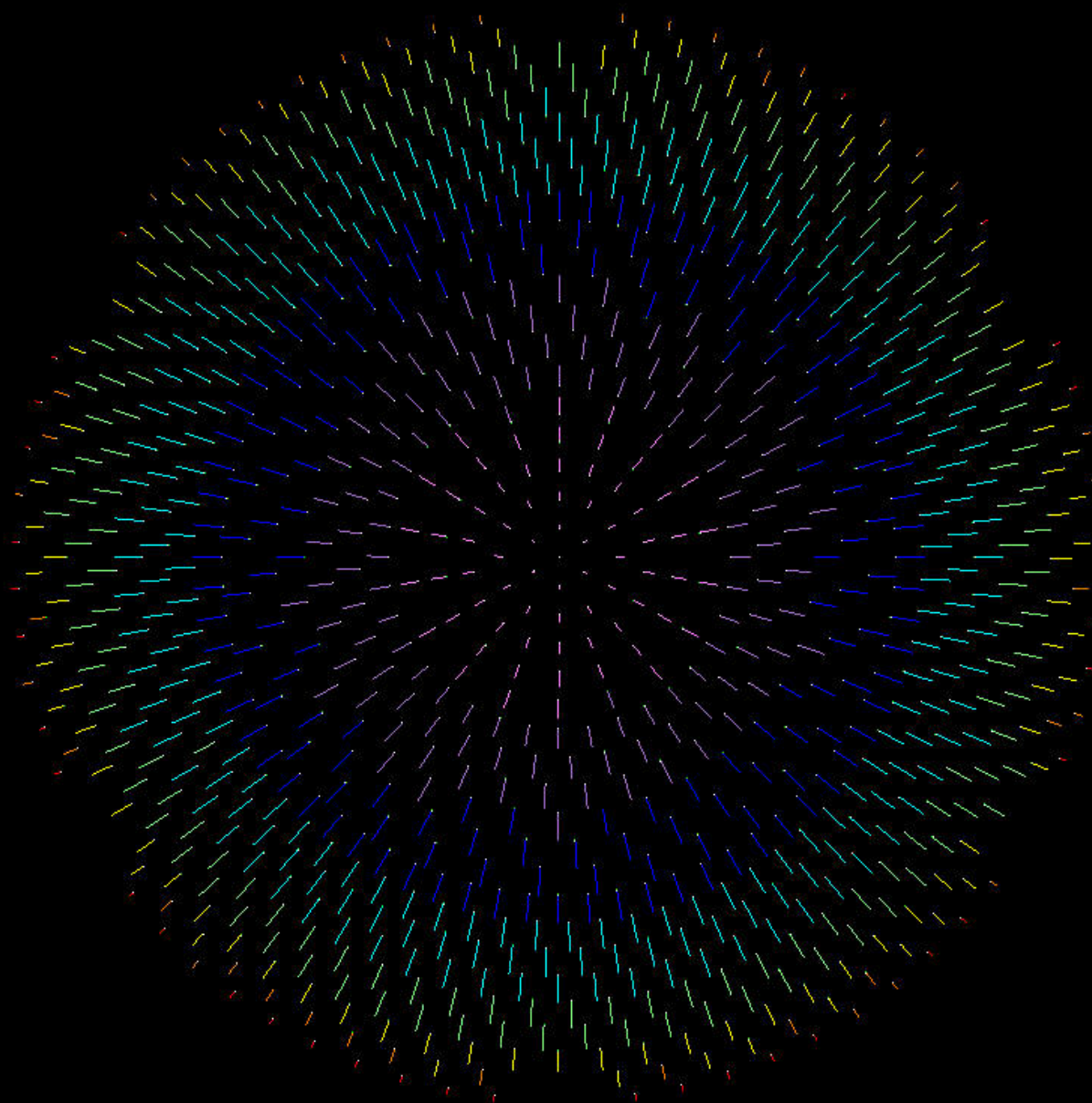


020130 080psi

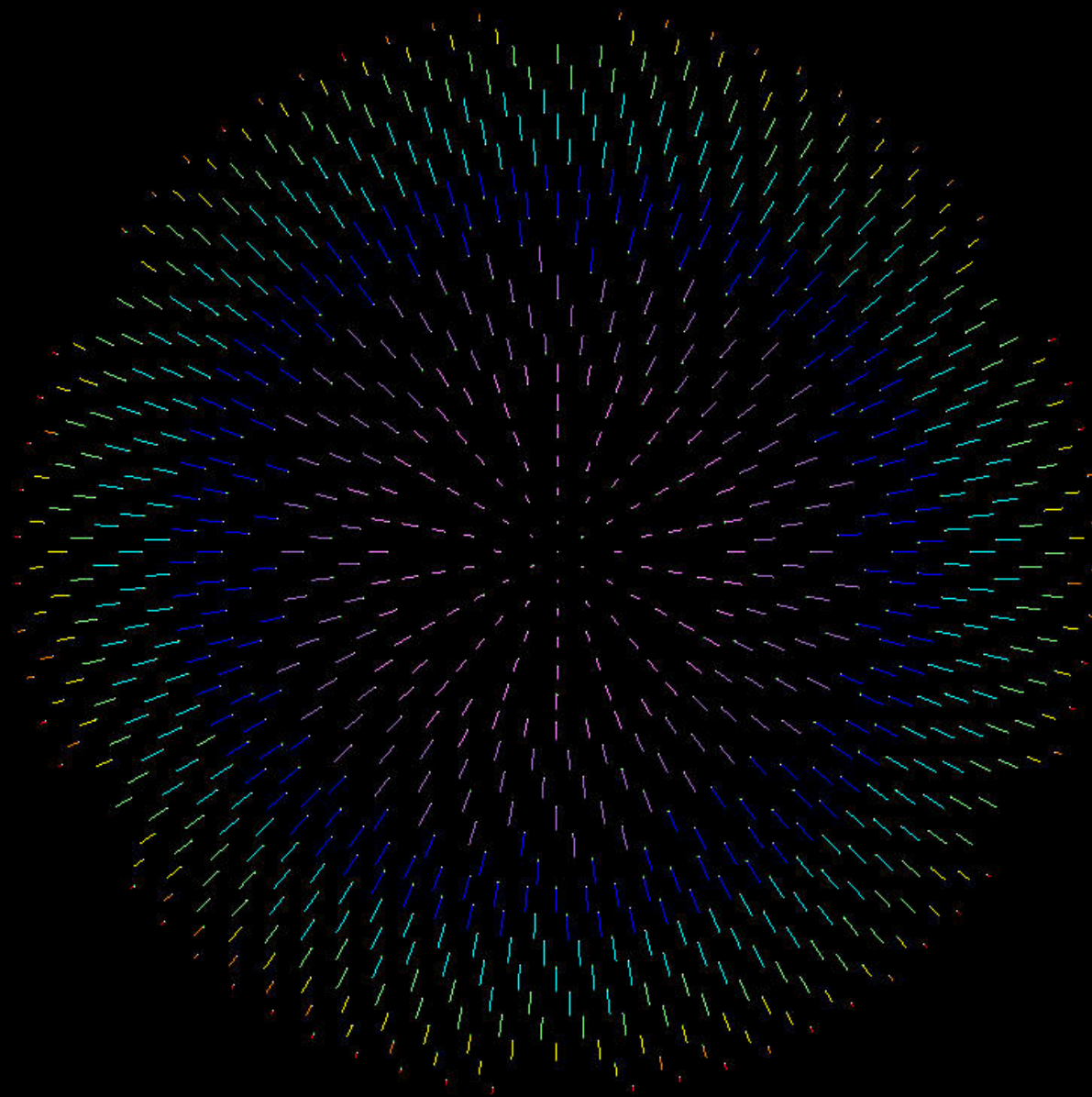




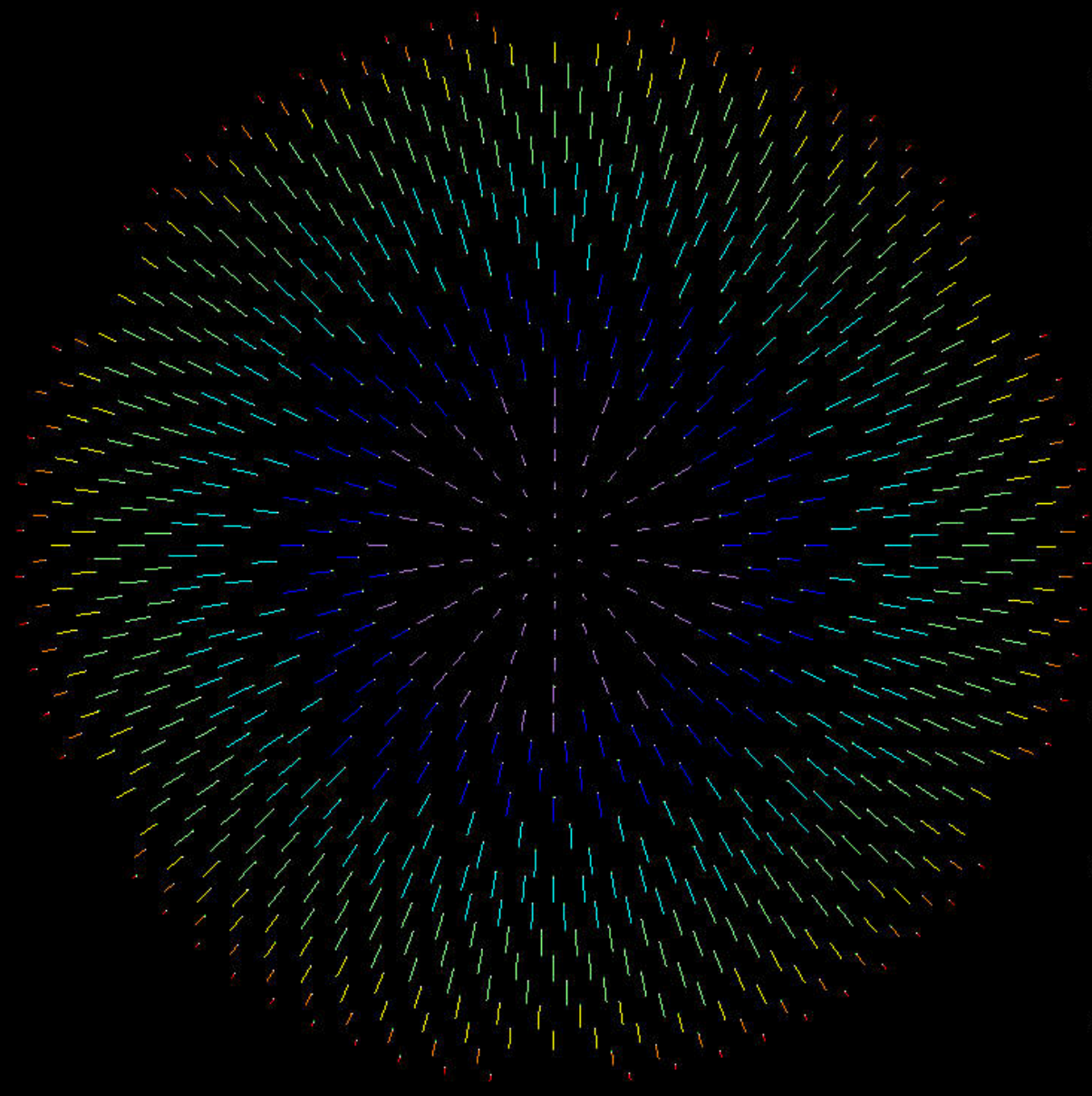
020130 085psi



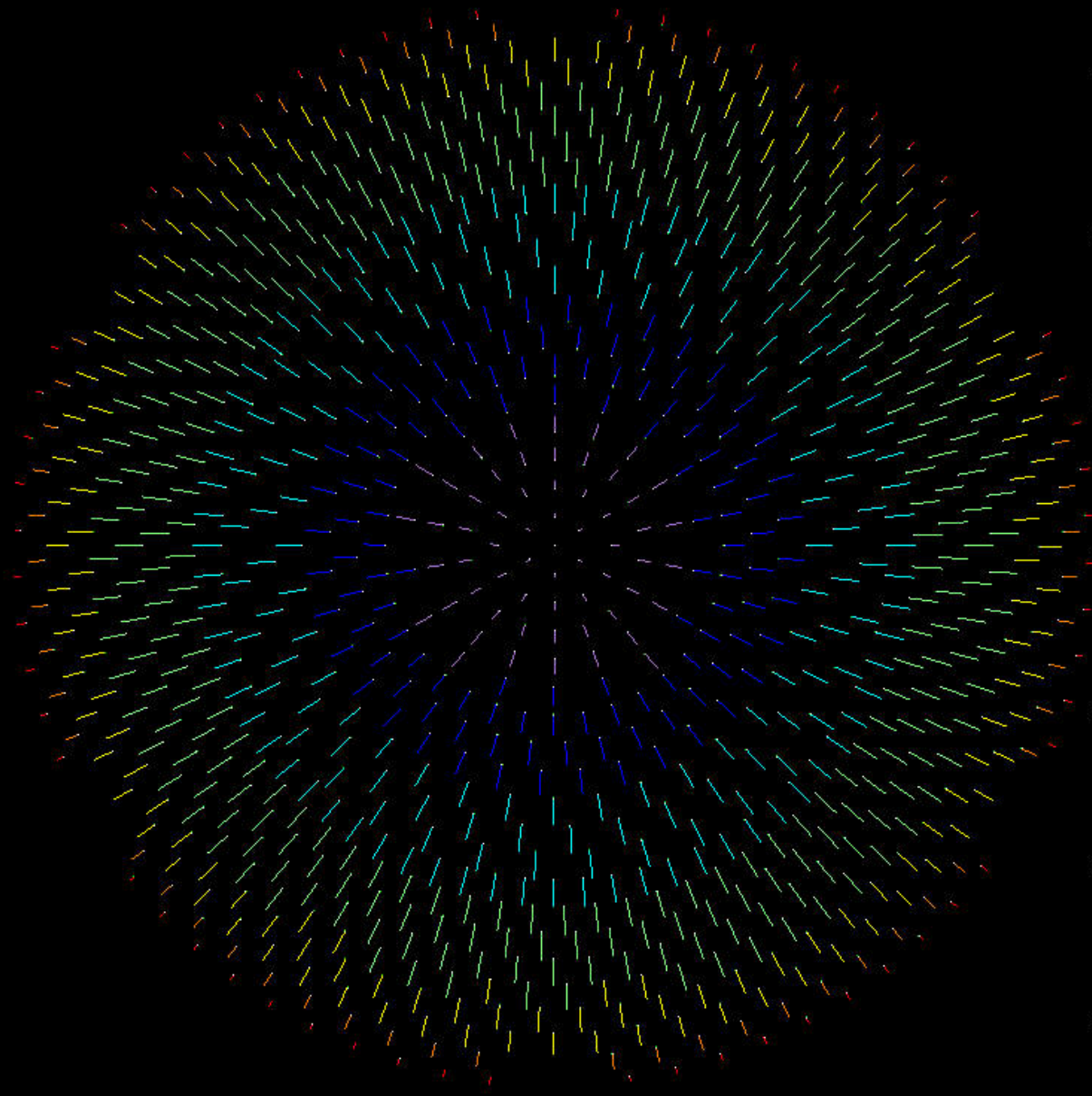
020130 090psi



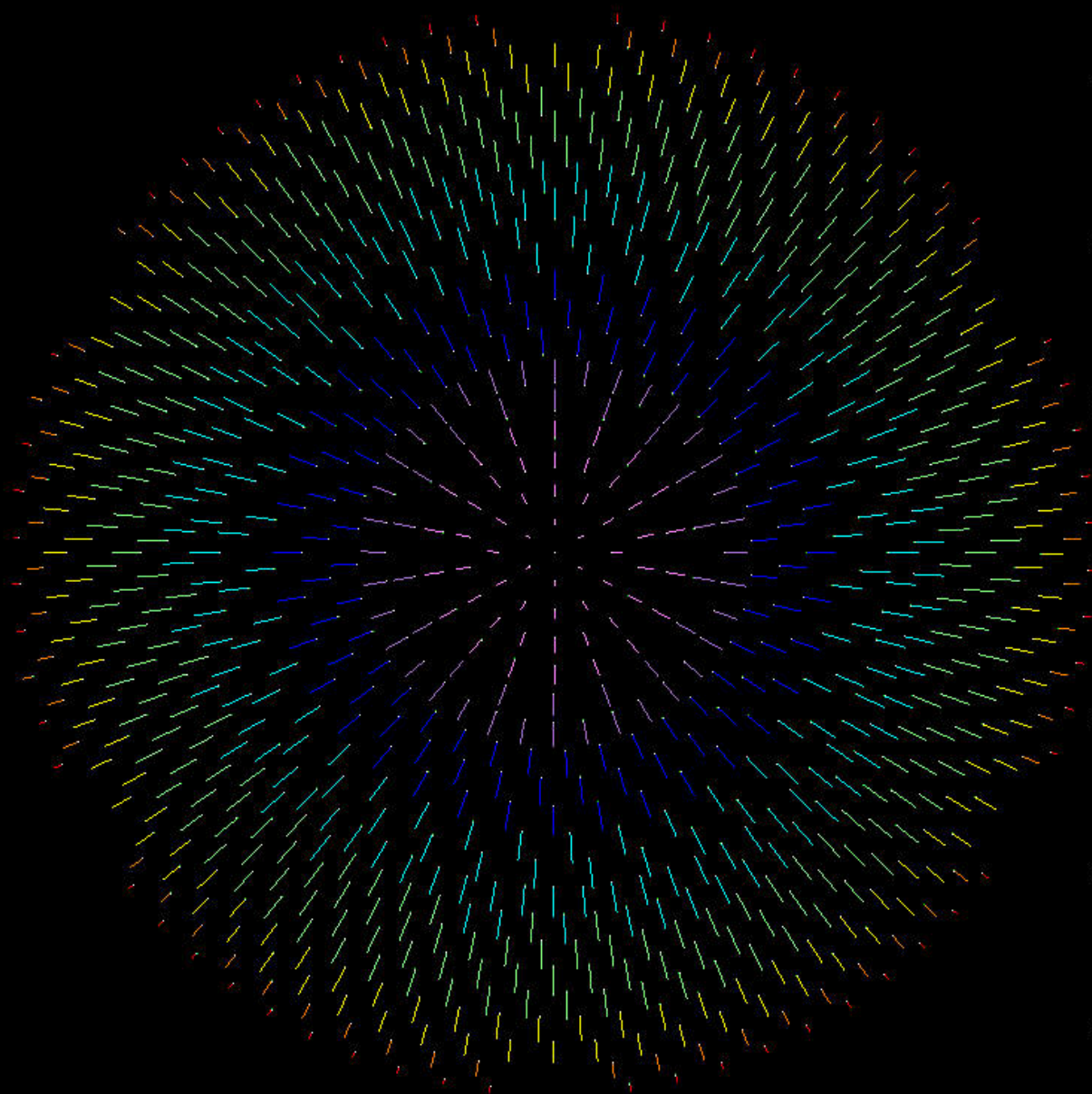
020130 095psi



020130 100psi

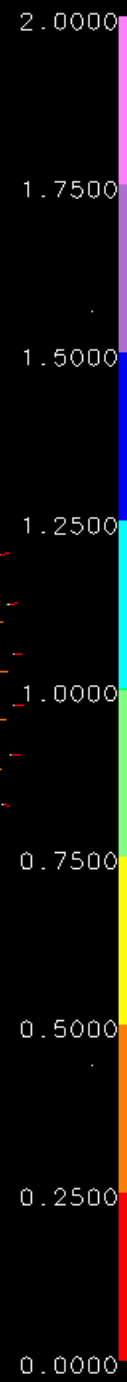
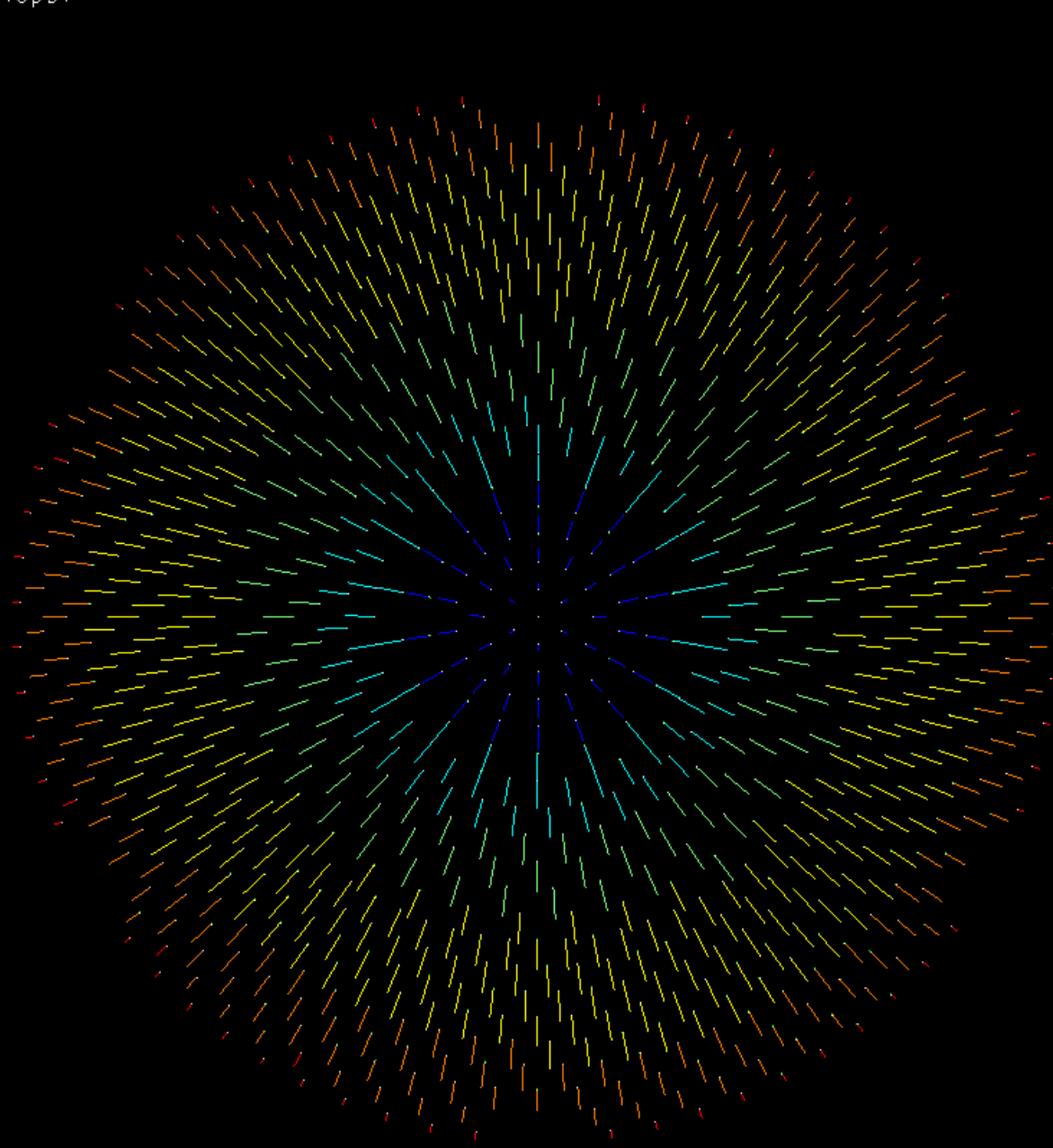


020130 105psi

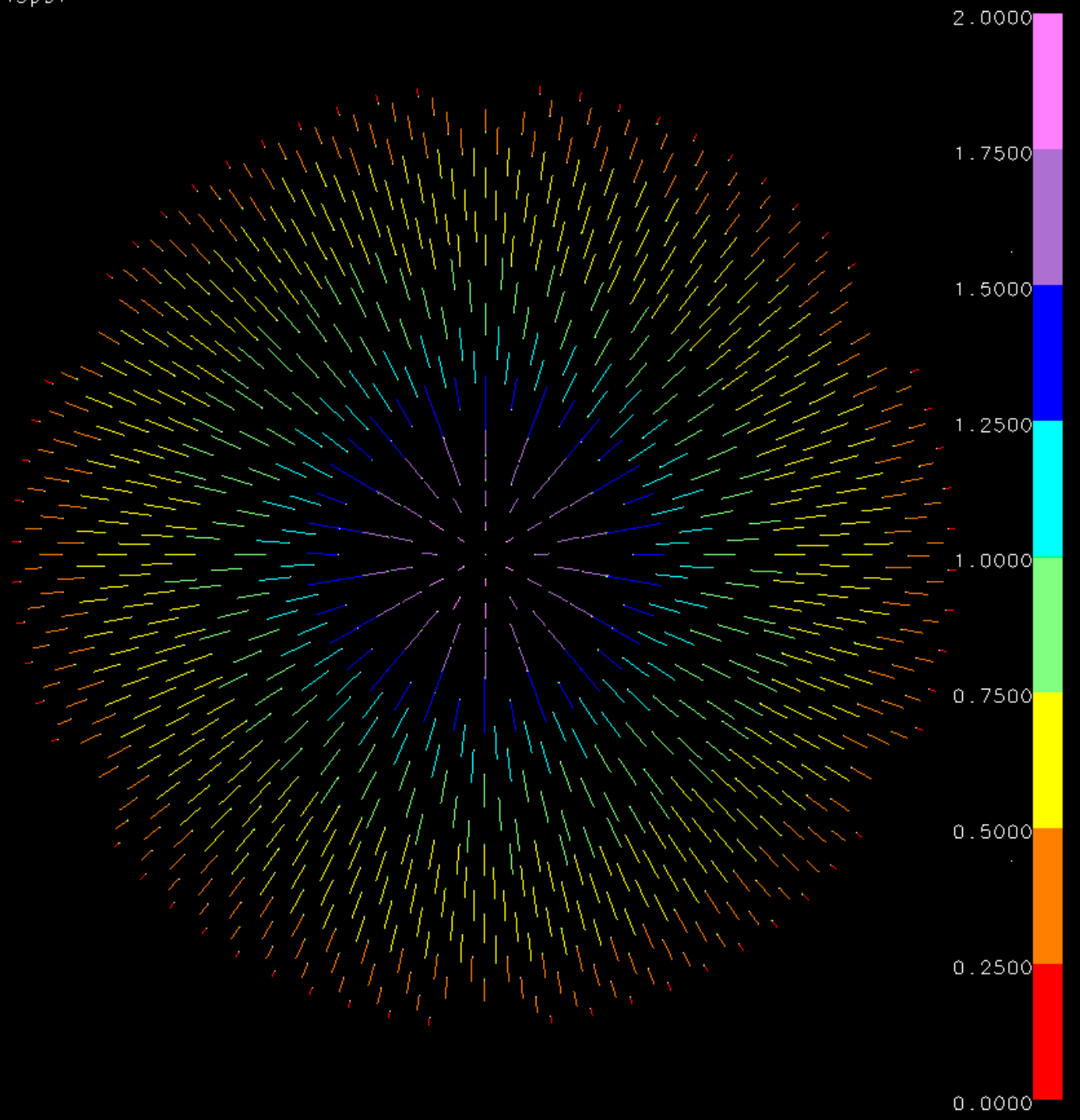


1.2000  
1.0500  
0.9000  
0.7500  
0.6000  
0.4500  
0.3000  
0.1500  
0.0000

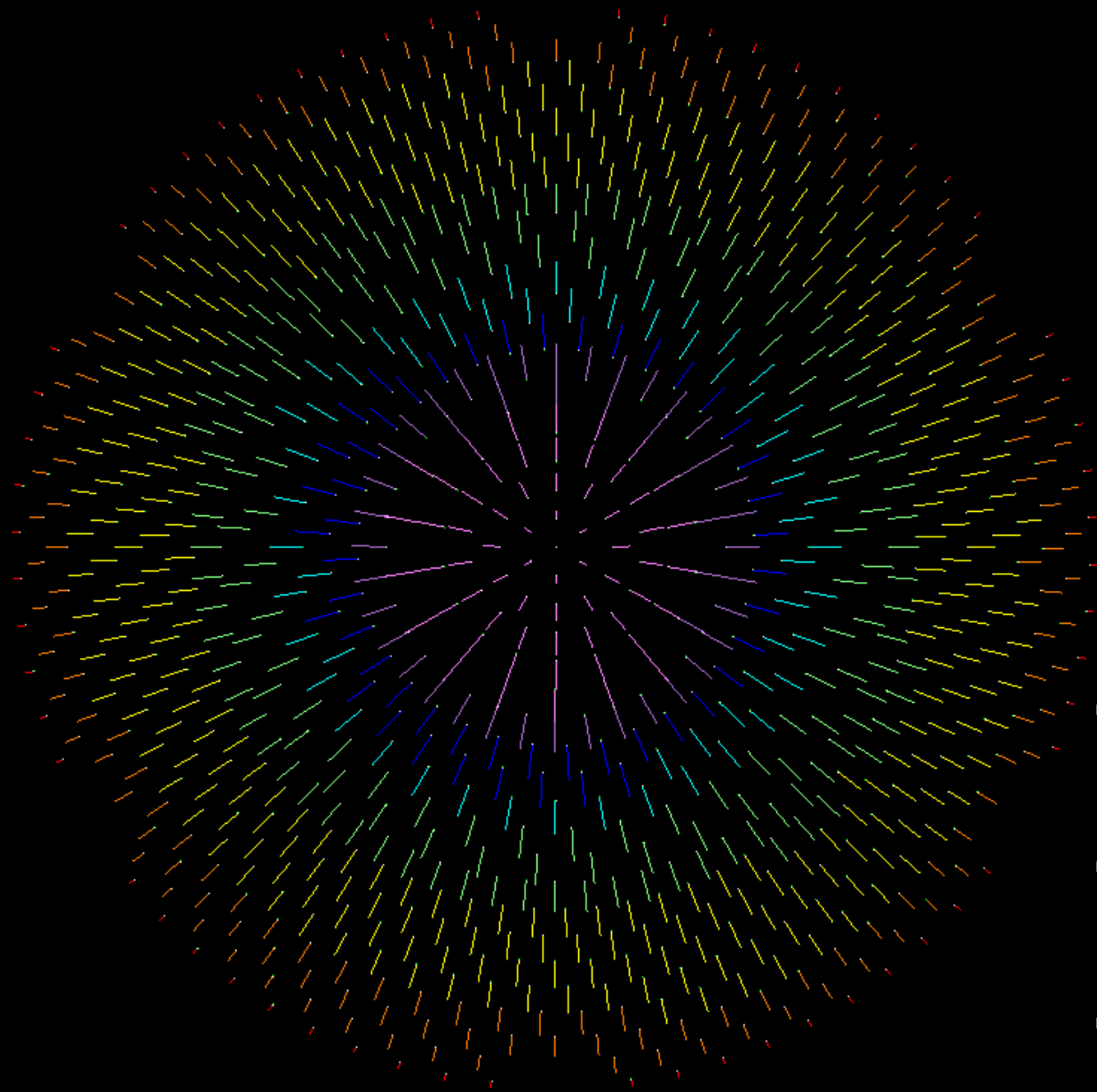
020130 110psi



020130 115psi



020130 120psi





# *Mucool history of photogrammetry*

- Compare the window's *performance* to FEA
- Observe *characteristics* of the window's performance
- Compare the window's *shape and thickness* to design specifications

# Advantages of photogrammetry over CMM

Non-contact

Greater surface coverage

# Non-contact



CMM

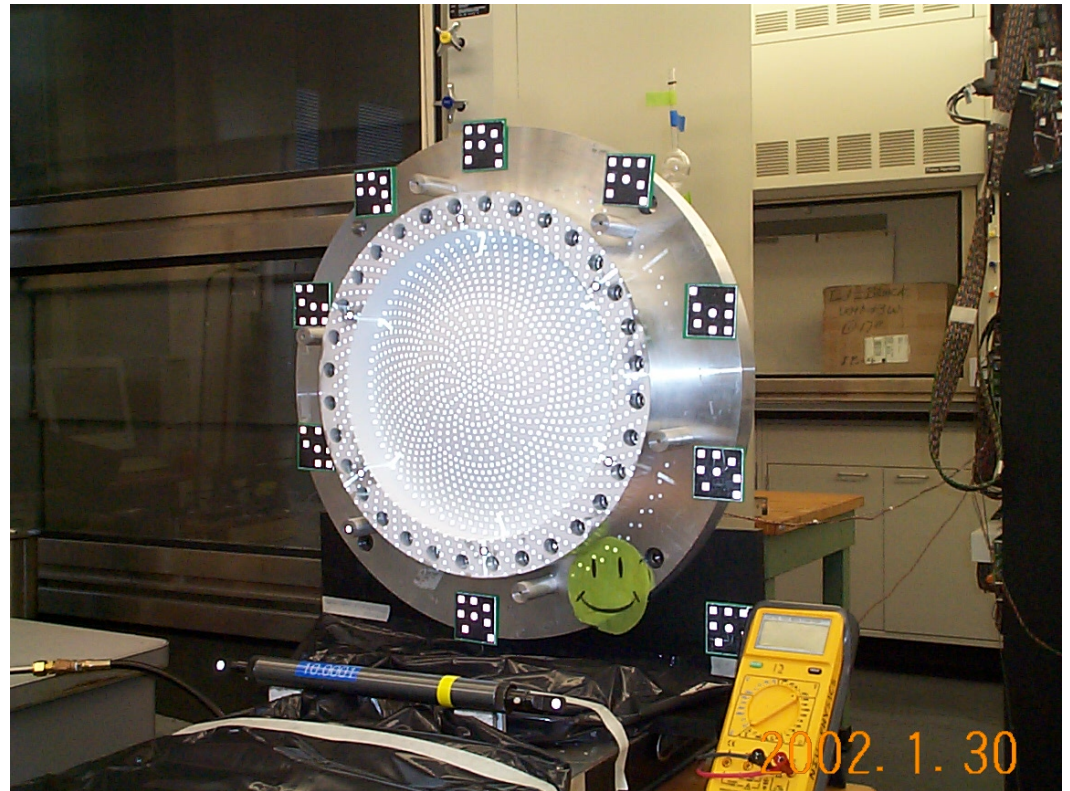


Photogrammetry

# Greater coverage



CMM ~30 points



Photogrammetry ~1000 points

# Setup to measure window shape

Measure the concave and convex sides of the window by moving the camera and projector from one side of the window to the other.

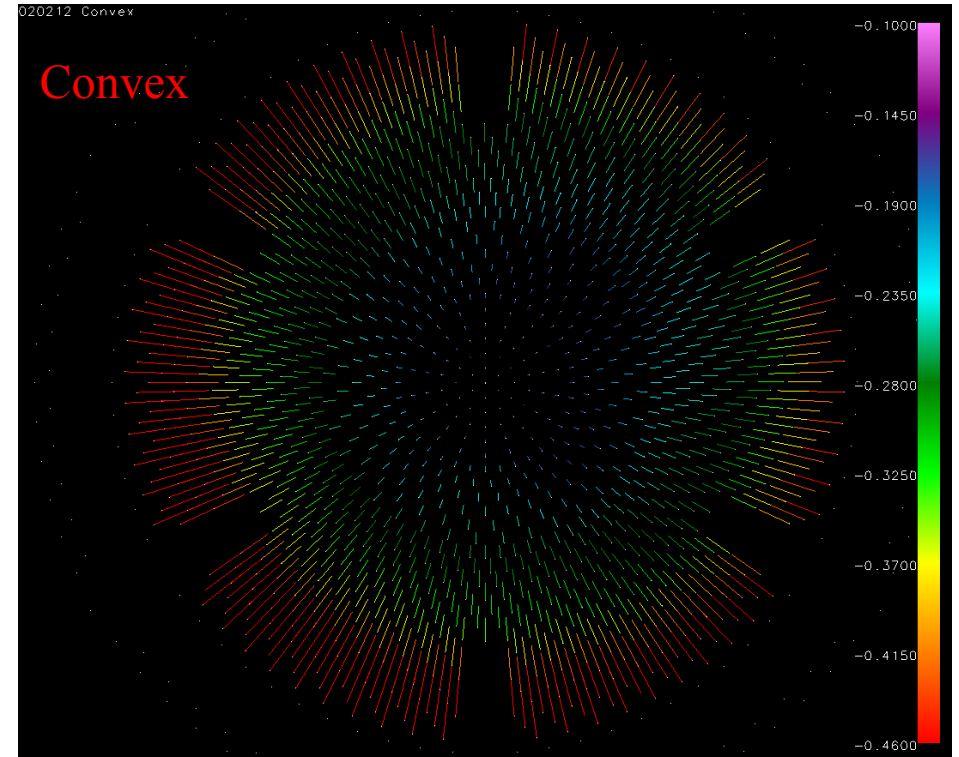
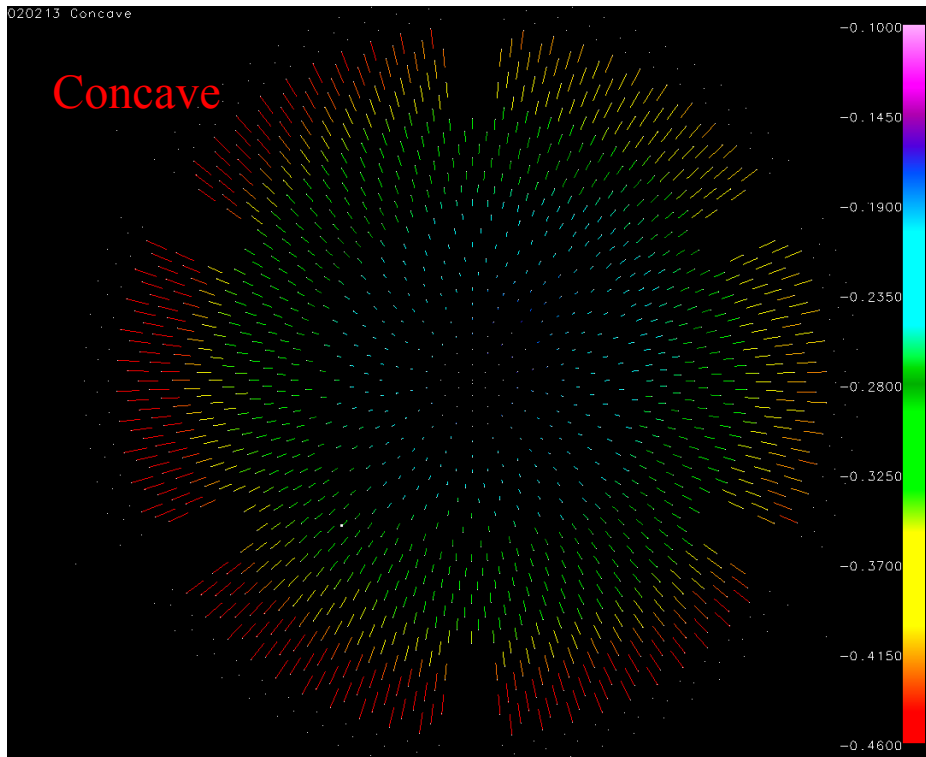


# Need for a surface model

Do *not* need to model the surface to compare the window shape with design.

Calculate design  $z$  for the  $x,y$  of each target & compare to measured  $z$ .

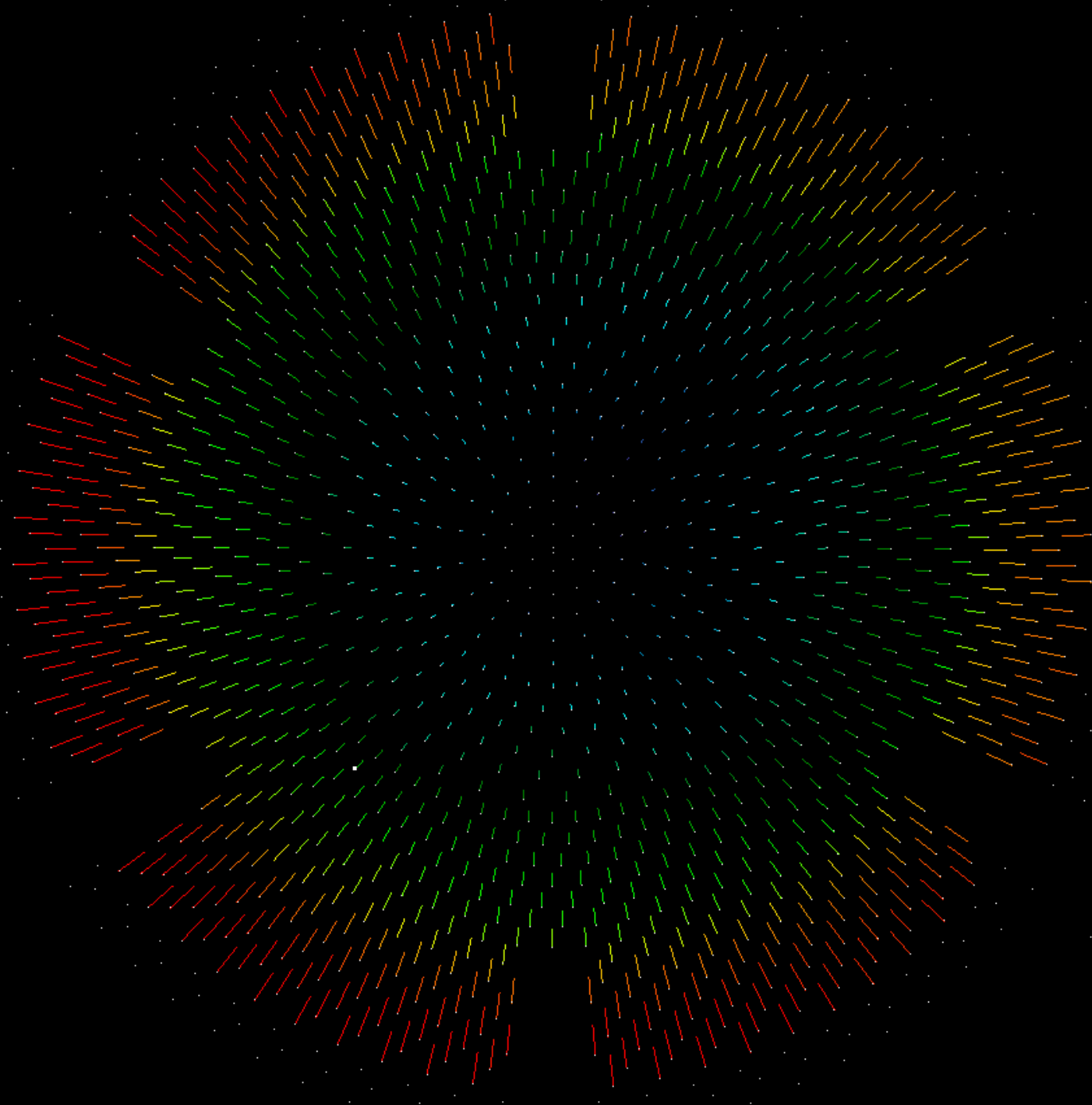
# Difference between measured shape and design



$$\text{Whisker} = z(\text{measured}) - z(\text{design})^*$$

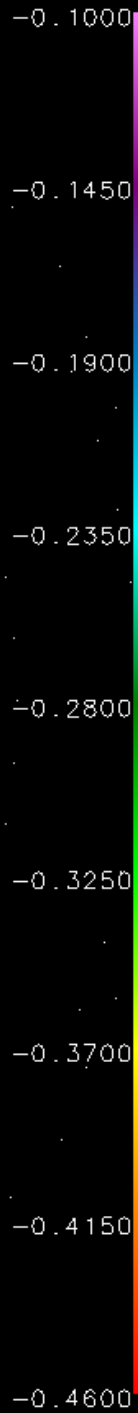
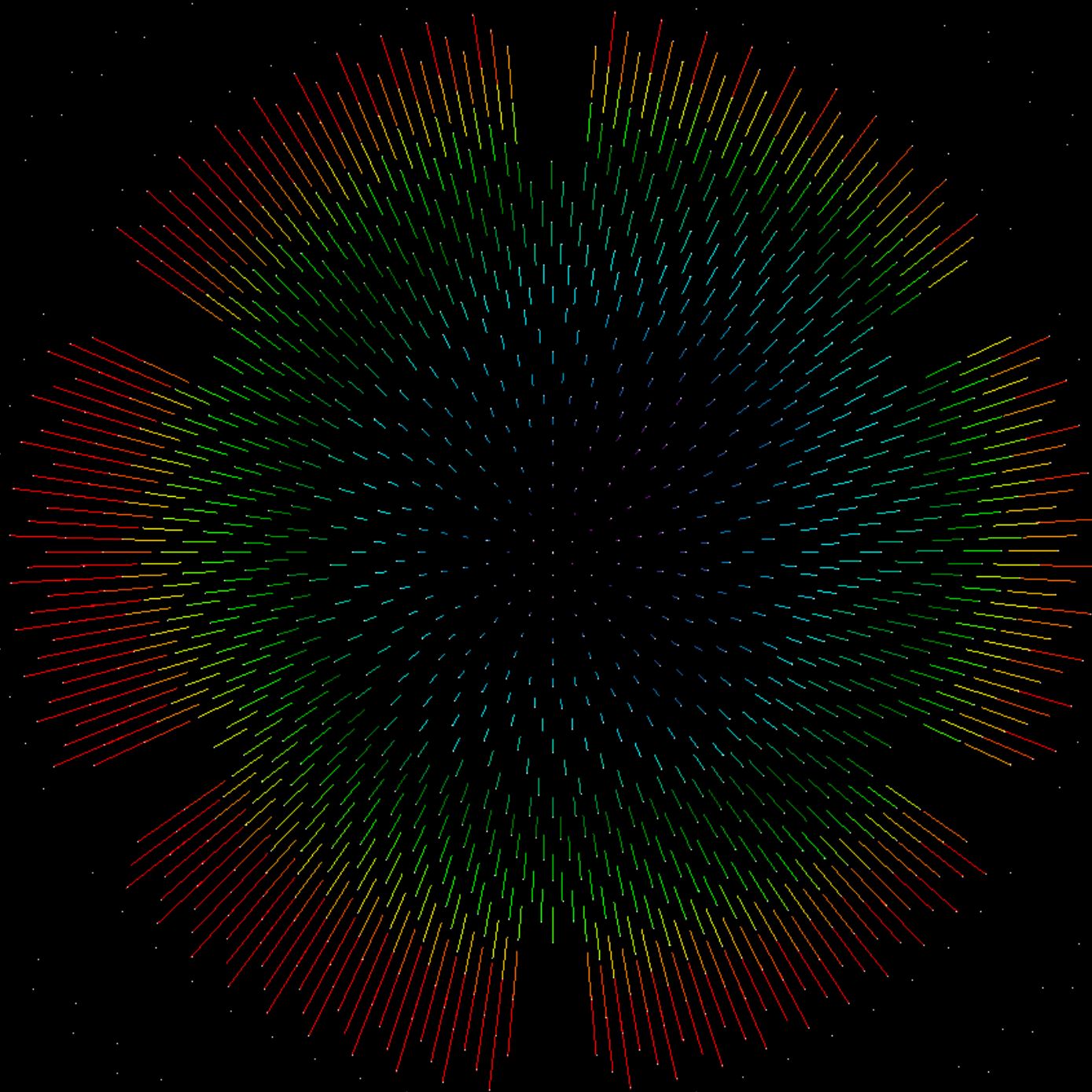
\*Given the design radius of curvature of the concave and convex surfaces,  $z(\text{design})$  was calculated for the  $(x,y)$  position of each target

020213 Concave





020212 Convex



The FEA sensitivity analyses emphasize the need to accurately determine the thickness of the window.

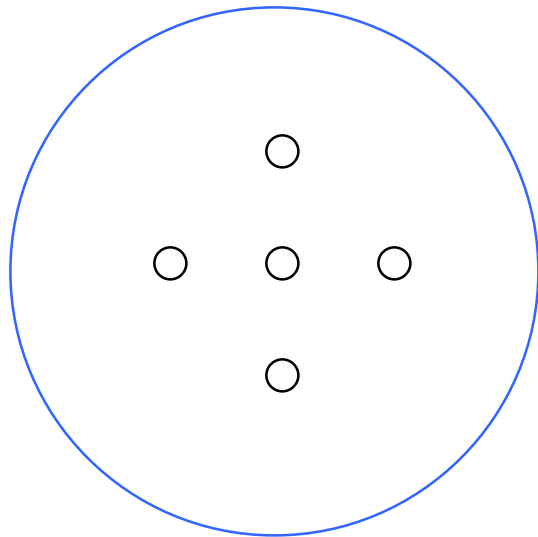
# Need for a surface model

A surface model *is* needed to determine the thickness

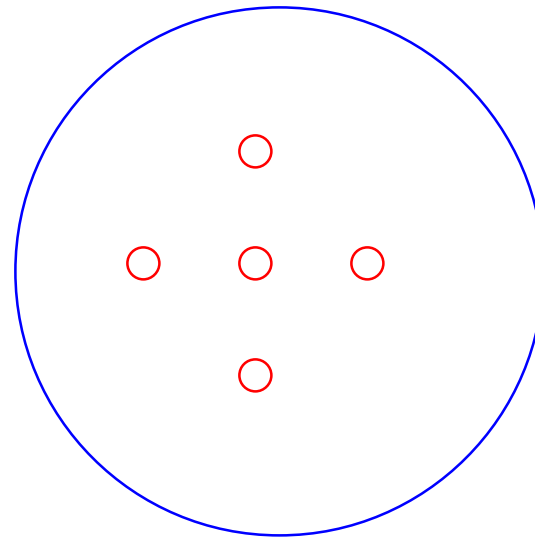
It is necessary to determine  $z$  for *matching pairs* of  $x,y$  on the concave and convex surfaces or the window.

*The required positions may be different from the target locations.*

# Problem of convex and concave alignment

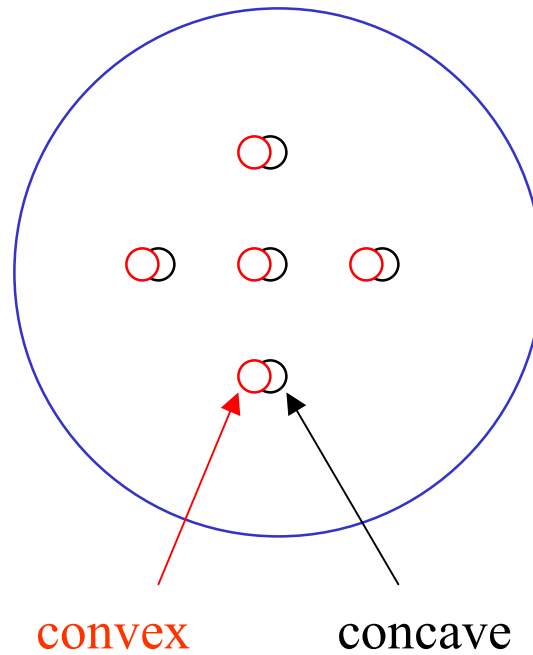


convex



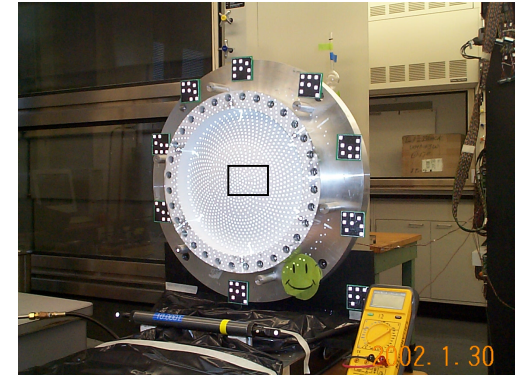
concave

# Problem of alignment

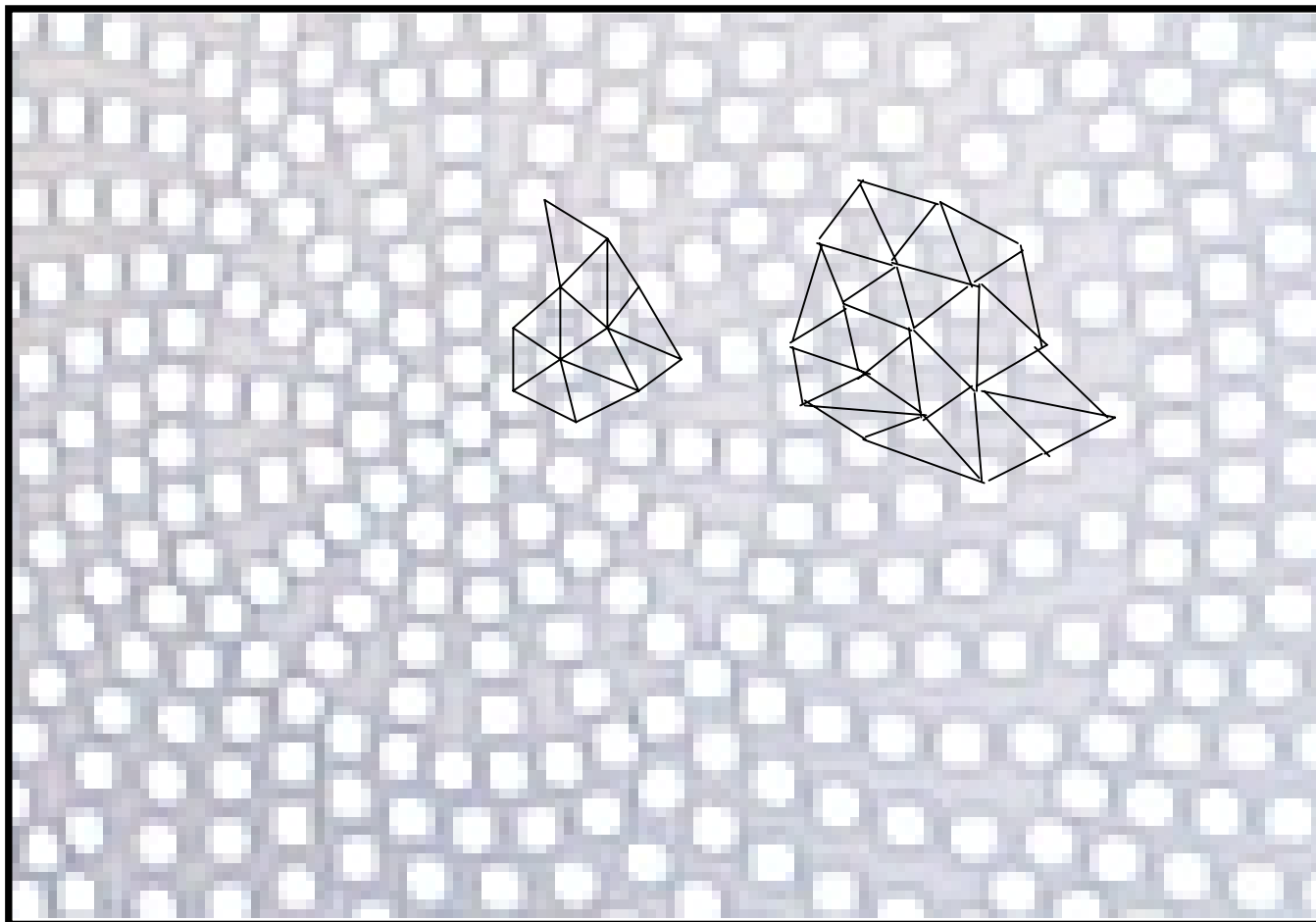


This makes it difficult to determine the window thickness

# VANGO



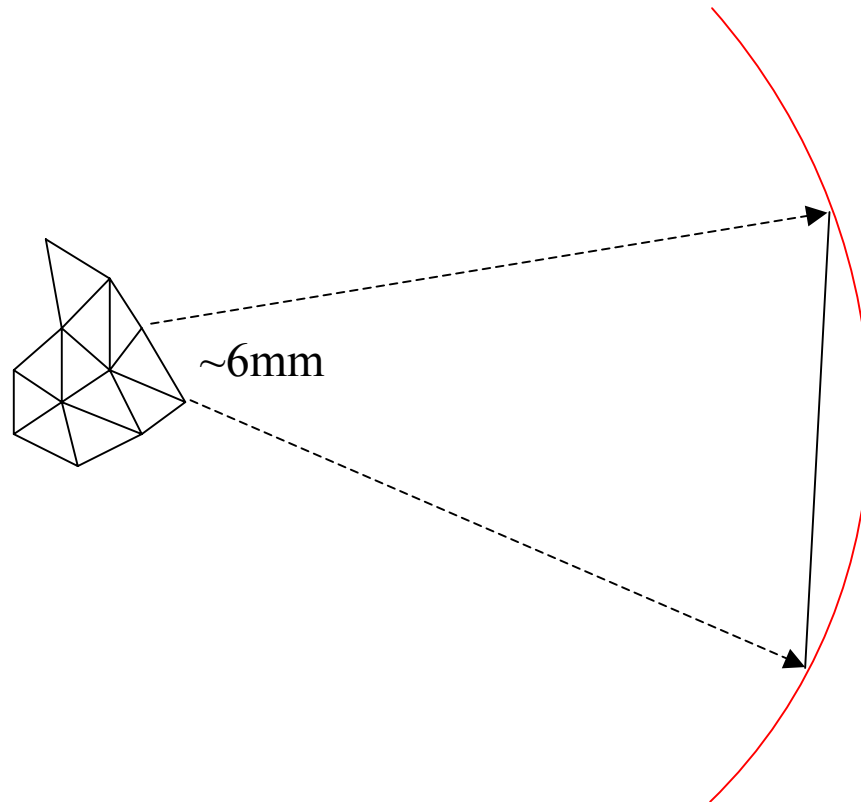
VANGO uses a TIN (Triangular Irregular Network) to create a surface model.



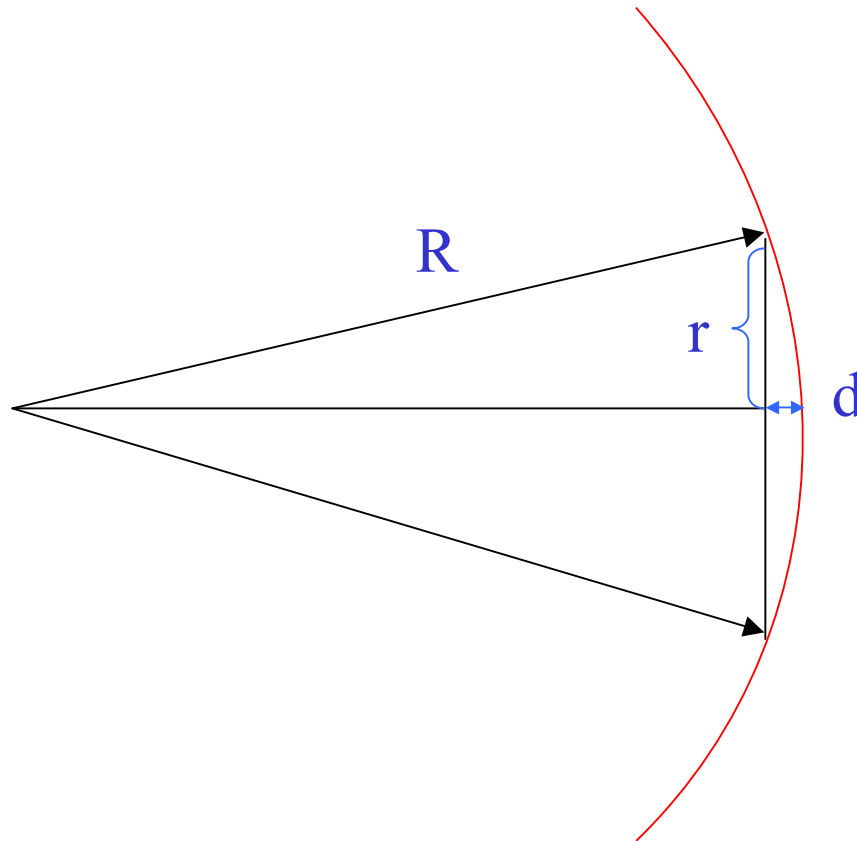
# VANGO

Point on triangle is always  $<$  true point.

This is important to interpret any periodicities seen in the data;  
period of an oscillation caused by the TIN would be  $\sim 6\text{mm}$



# VANGO error



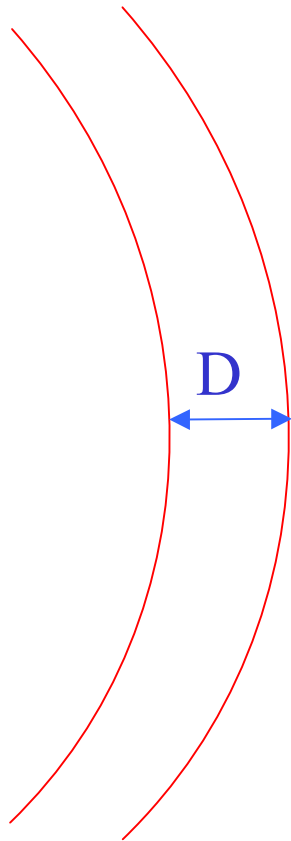
$$\frac{\theta}{2} = \sin^{-1} \left( \frac{r}{R} \right)$$

$$d = R - R \cos \left( \frac{\theta}{2} \right)$$

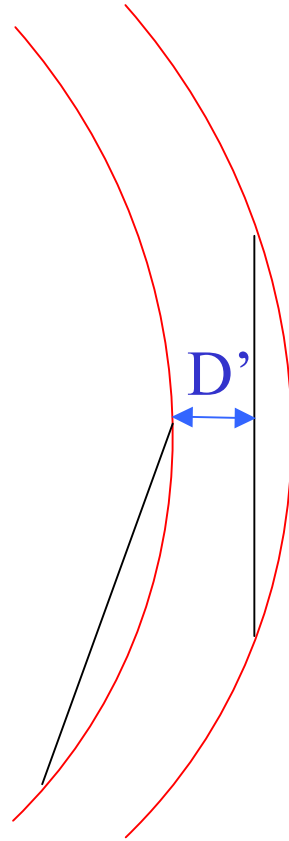
$d = f(\text{radius of curvature, size of triangle})$



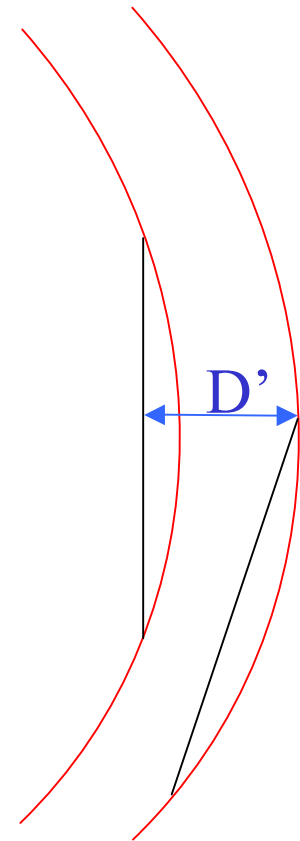
# Errors in thickness due to VANGO TIN worst case geometry\*



IDEAL



$$D' = D - 14.6\mu\text{m}$$

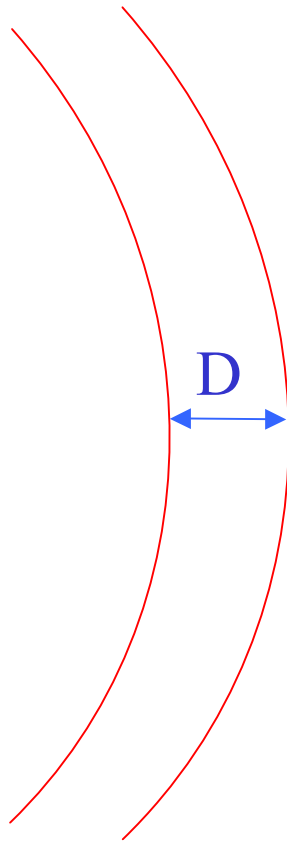


$$D' = D + 15\mu\text{m}$$

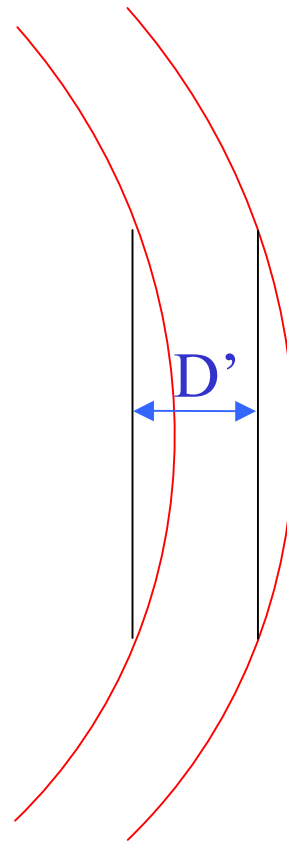
\*Assumes 6mm chord and design radii 30.000cm and 30.844cm

Note: Nominal thickness (D) = 330μm

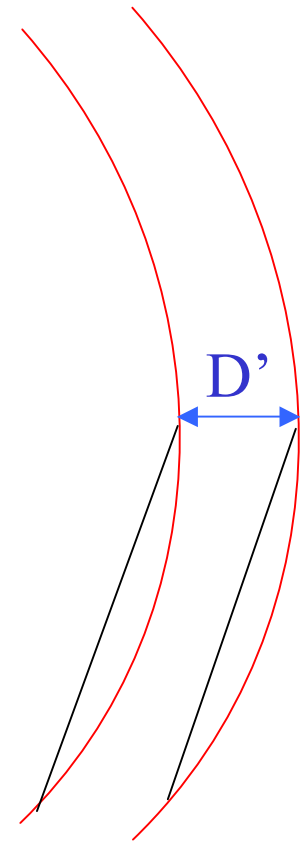
# Errors in thickness due to VANGO TIN: intermediate and best case\*



IDEAL



$D' = D - 0.4\mu\text{m}$

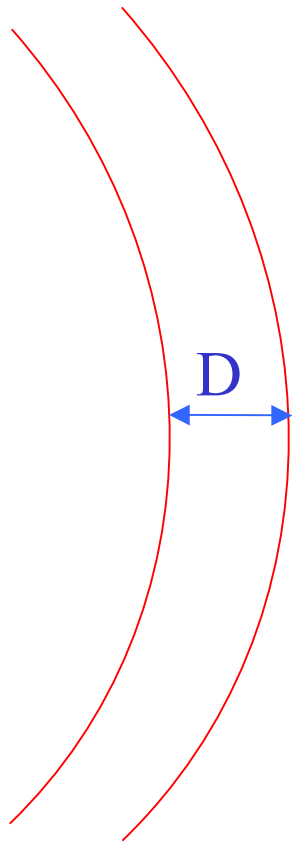


$D' = D$

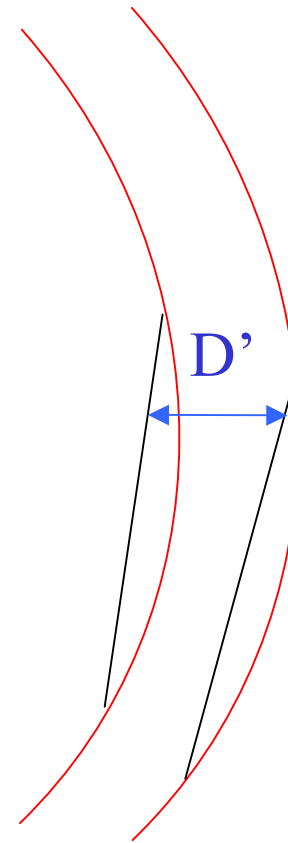
\*Assumes 6mm chord and design radii 30.000cm and 30.844cm

Note: Nominal thickness (D) = 330um

# TIN geometry for center of Window 4



IDEAL



$D' = D + (\sim 10\mu\text{m})$

# VANGO TIN

*Result for the center:*

Thickness = 341.0um ( $\pm 5.5$ um) + (- ~10um)

Convex RMS = 3.6um Concave RMS = 4.1um

The difference (thickness) should have an RMS of about 5.5um

# VANGO error bars

Each point requires a unique error bar.

Error = f(phase between concave & convex triangles,  
size of triangles,  
radius of curvature)

# Small patch sphere fit (SPSF)

Fit a sphere to the points near the point in question.

The sphere fit gives the equation of the sphere:

# Small patch sphere fit (SPSF)

$$(x'-x)^2 + (y'-y)^2 + (z'-z)^2 = r^2$$

where  $x, y, z$  are unknowns

Solve for  $z$  choosing desired  $(x, y)$

Do this for both concave and convex surfaces

The difference between  $z_{concave}$  and  $z_{convex}$  is the thickness

# Small patch sphere fit (SPSF)

To find the thickness at the center of the window,

solve for  $z$  choosing  $x=0$  and  $y=0$ .



# Small patch sphere fit (SPSF) errors

Intrinsic precision of the points used in the fit.

The basic assumption is that the intended shape was a sphere

# Small patch sphere fit (SPSF)

*Result for the center:*

Thickness =  $331.6\mu\text{m} \pm 5.5\mu\text{m}$

Error of spherical fit:

Convex RMS =  $3.6\mu\text{m}$    Concave RMS =  $4.1\mu\text{m}$

The difference (thickness) should have an RMS of about  $5.5\mu\text{m}$

# Summary of what we've done so far to determine thickness

Obtained two window thickness measurements *at the center*:

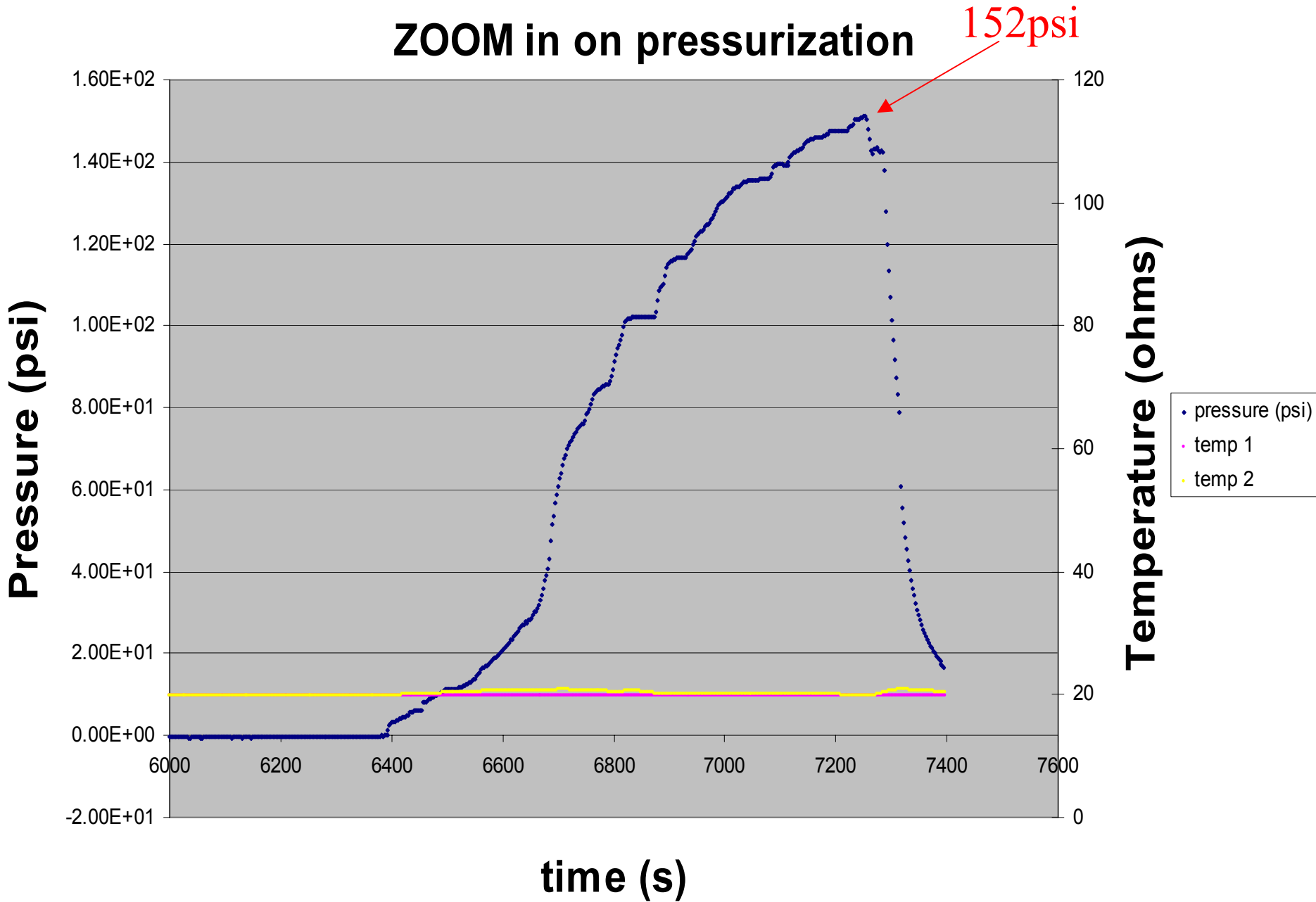
VANGO TIN 341.0um ( $\pm 5.5\text{um}$ ) + (-  $\sim 10\text{um}$ )

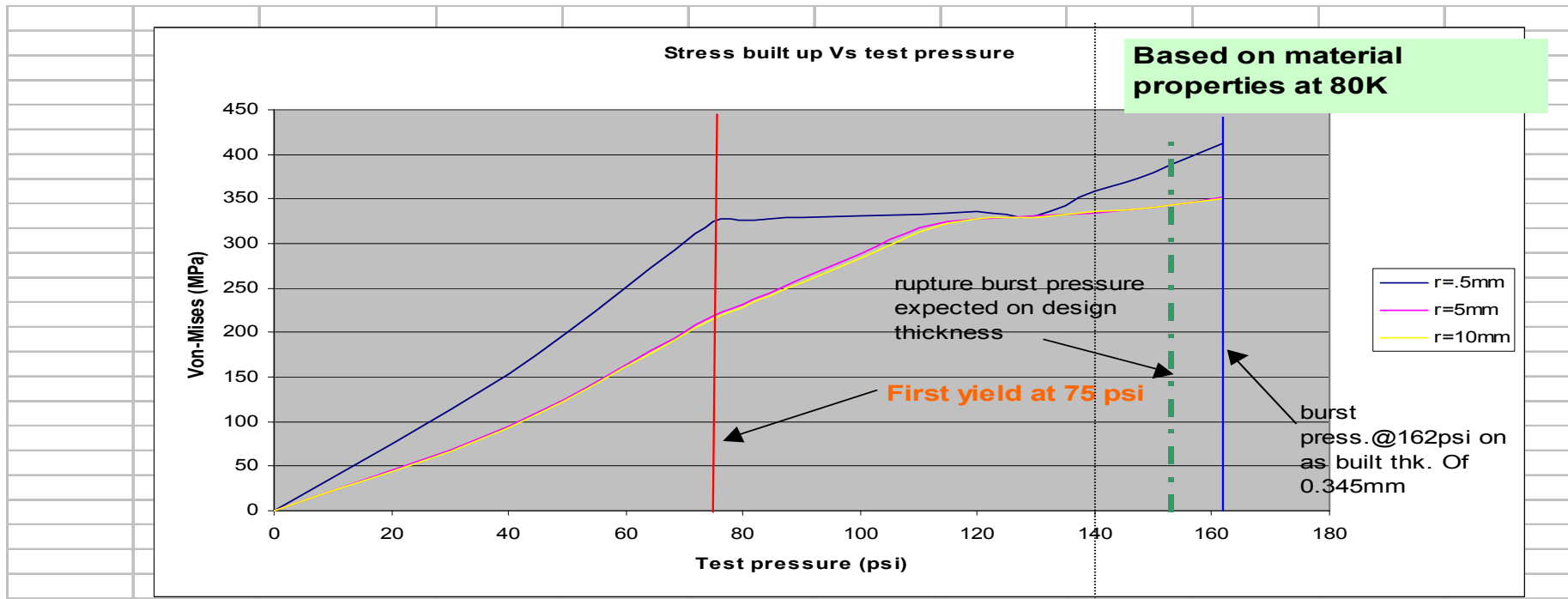
SPSF 331.6um  $\pm 5.5\text{um}$

Additional support for the thickness value  
derived from SPSF:

# LN burst Window 4

## ZOOM in on pressurization





The predicted burst pressure (162psi) was greater than the observed burst pressure (152psi).

This implies that thickness assumed in the FEA (345um) was greater than the true thickness.

This would be consistent with a measured thickness of 331um.

# What next?

We haven't found the *thinnest* part of window yet,  
only the thickness at a chosen point...which we chose to be the center.

# How to find the thinnest point?

- Extended application of SPSF
  - Perform SPSF at many points and search for the minimum

- Modified TIN
  - Use a sphere to approximate the triangular surface between measured points

