

Beam Window Analysis
Muon Collider Project
Experiment 951

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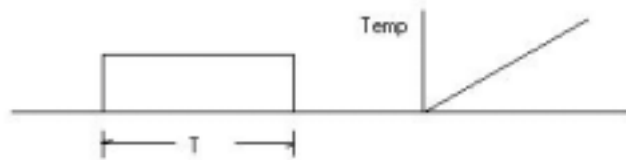
E951 Window Analysis Overview

- **Proton Beam Structure**
 - 15 TP, 24 GeV, Gaussian profile
 - smallest beam spot size assumed = 1mm RMS sigma
 - pulse structure and length
- **Beam/window interactions**
 - A3 Line Windows
 - E951 Target enclosure windows
 - thermal shock
 - material behavior
- **Benchmark analysis and simulation verification using experiment 951 targets**

Proton Beam Structure

- **Proton Beam Structure**

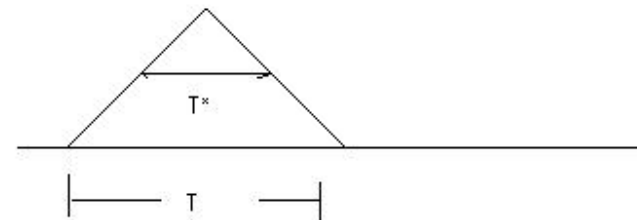
- 15 TP, 24 GeV, Gaussian profile
- smallest beam spot size = 1mm RMS sigma
- pulse structure and length



T = pulse length

Proton distribution uniform in time
Beam profile is Gaussian

Energy deposition (thermal input rate) constant

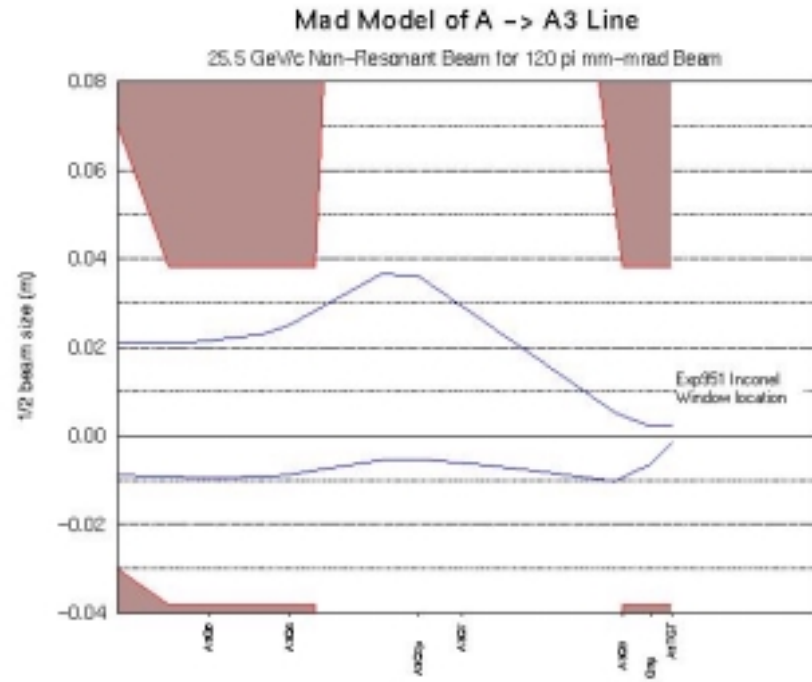
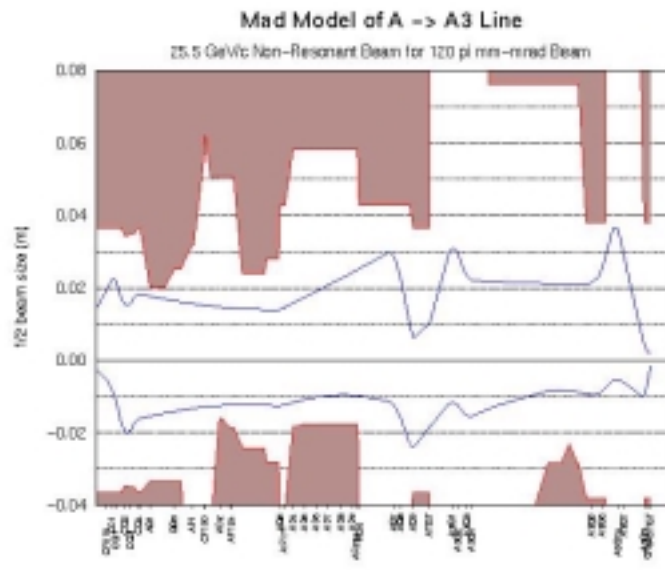


Proton distribution in time space (real beam !!)
Beam = Gaussian in space

T for AGS beam ~ 100 ns

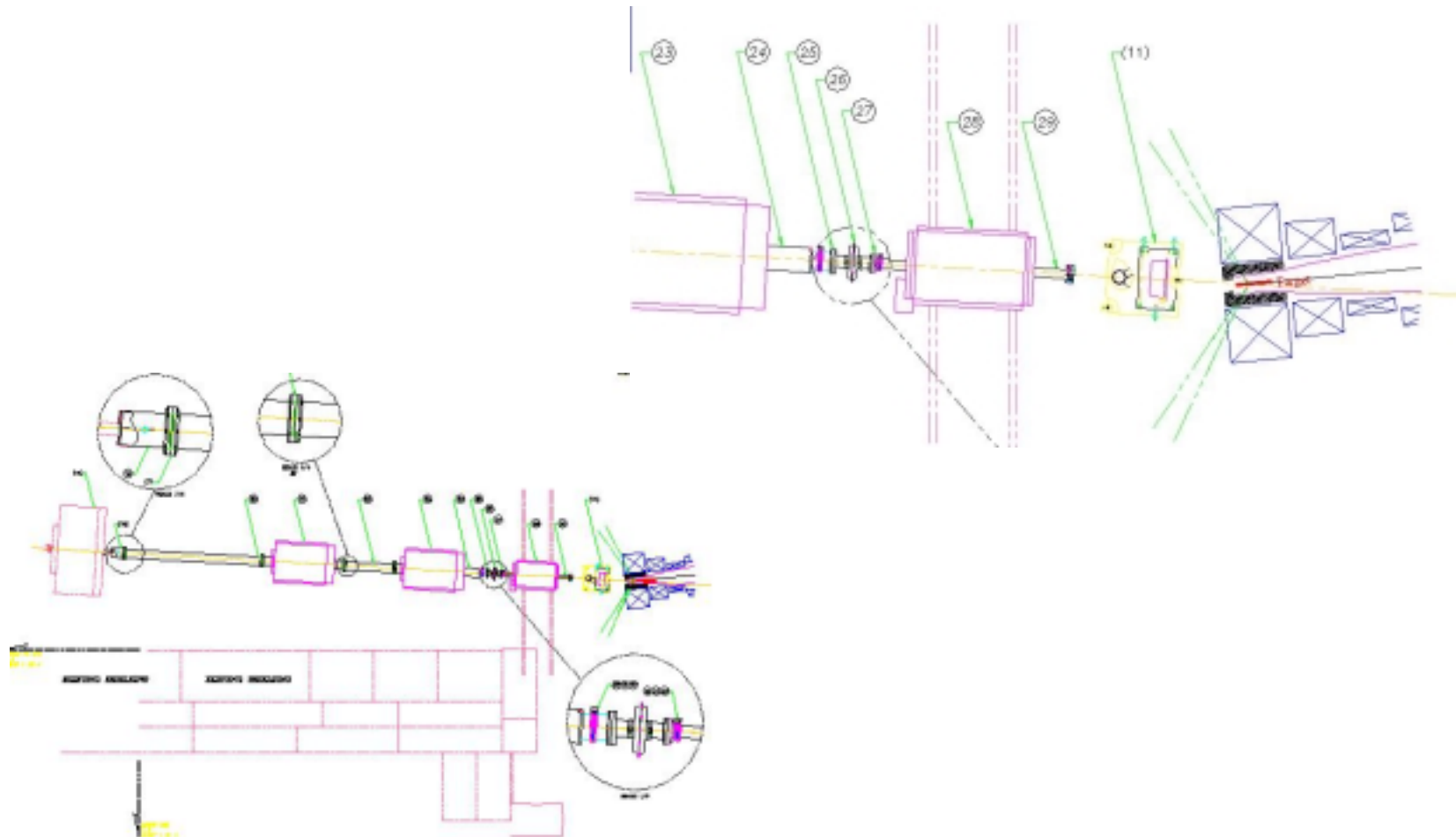
T^* $30 \sim 40$ ns

A3 Line Beam Size



A3 Line

- A3 Line near E951



A3 Line Windows

- **Material used is different series Aluminum**
 - 5052 series available in 3-mil thickness
- **Concern is the TP per pulse coupled with a small spot size**
- **Experience from previous experiments showed good window response**
 - an order of magnitude higher in single-pulse TP for E951

E951 Enclosure Windows

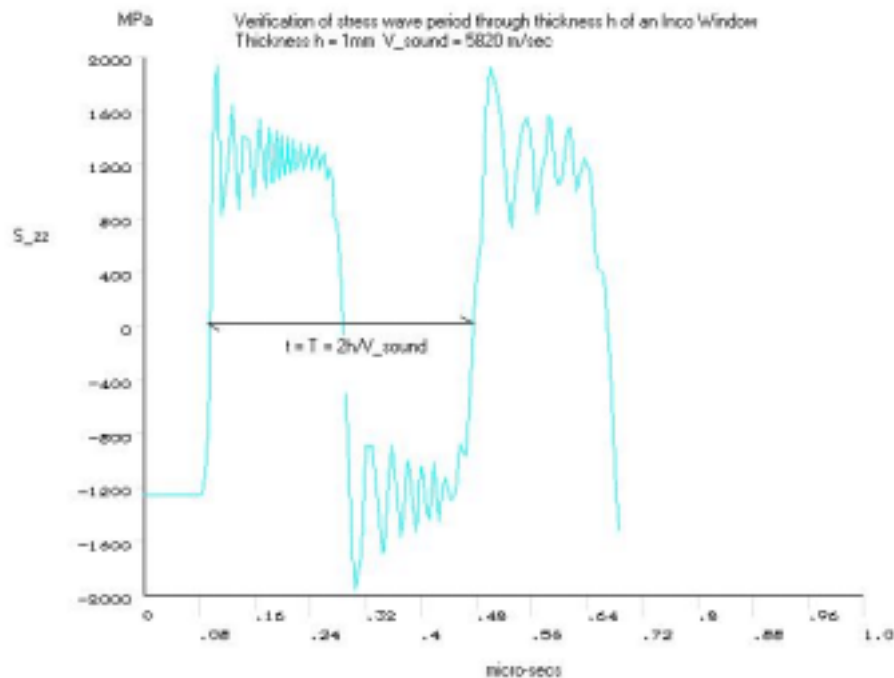
- **Family of materials assessed**
 - INVAR
 - SS316
 - Inconel-718
- **Beam spot size same as on target**
 - Estimates based on 1mm RMS sigma
 - Beam spot may actually be SMALLER !!
 - E951 window positioning
 - Window material monitoring and failure verification

Background on Thermal Shock and Window Failure Estimation

- Quasi-static thermal stress from energy deposition is a 3-D affair no matter how thin the window is
 - directional stress in 3-D world = $E \cdot \alpha \cdot \Delta T / (1 - 2 \cdot \nu)$
- Two-dimensional simplification of a thin structure does not quite apply
 - directional stress in 2-D = $E \cdot \alpha \cdot \Delta T / (1 - \nu)$
 - 1-D = $E \cdot \alpha \cdot \Delta T$
- Of concern is NOT the level of directional stress but the deviation from the hydrostatic state of stress (VonMises stress)
- Directional stresses are coupled through the Poisson's ratio
 - dynamic changes in one direction affect all others
- Build-up of thermal stress in the course of proton pulse
- Propagation and attenuation of shock or dynamic stress

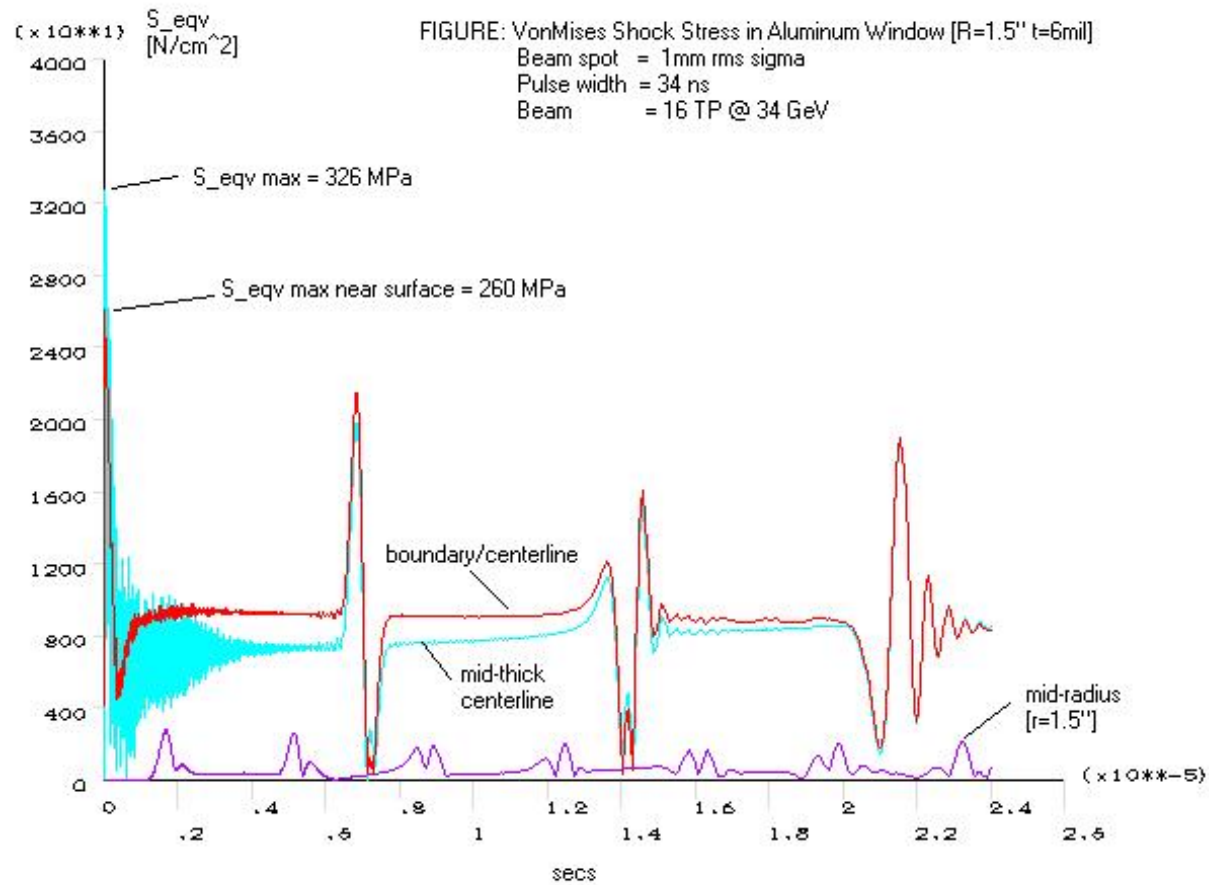
Background on Thermal Shock and Window Failure Estimation

- Based on 3-D stress state the effect of through-thickness RINGING is accounted
- Its effect is **dominant** in the response of the heated window region
- Governed principally by the propagation of stress waves in 1-D space
 - **stress**(t) = f(x-ct) + f(x+ct) [c = speed of sound in material]
 - **period** of ringing = $2 \cdot h/c$ [h = window thickness]



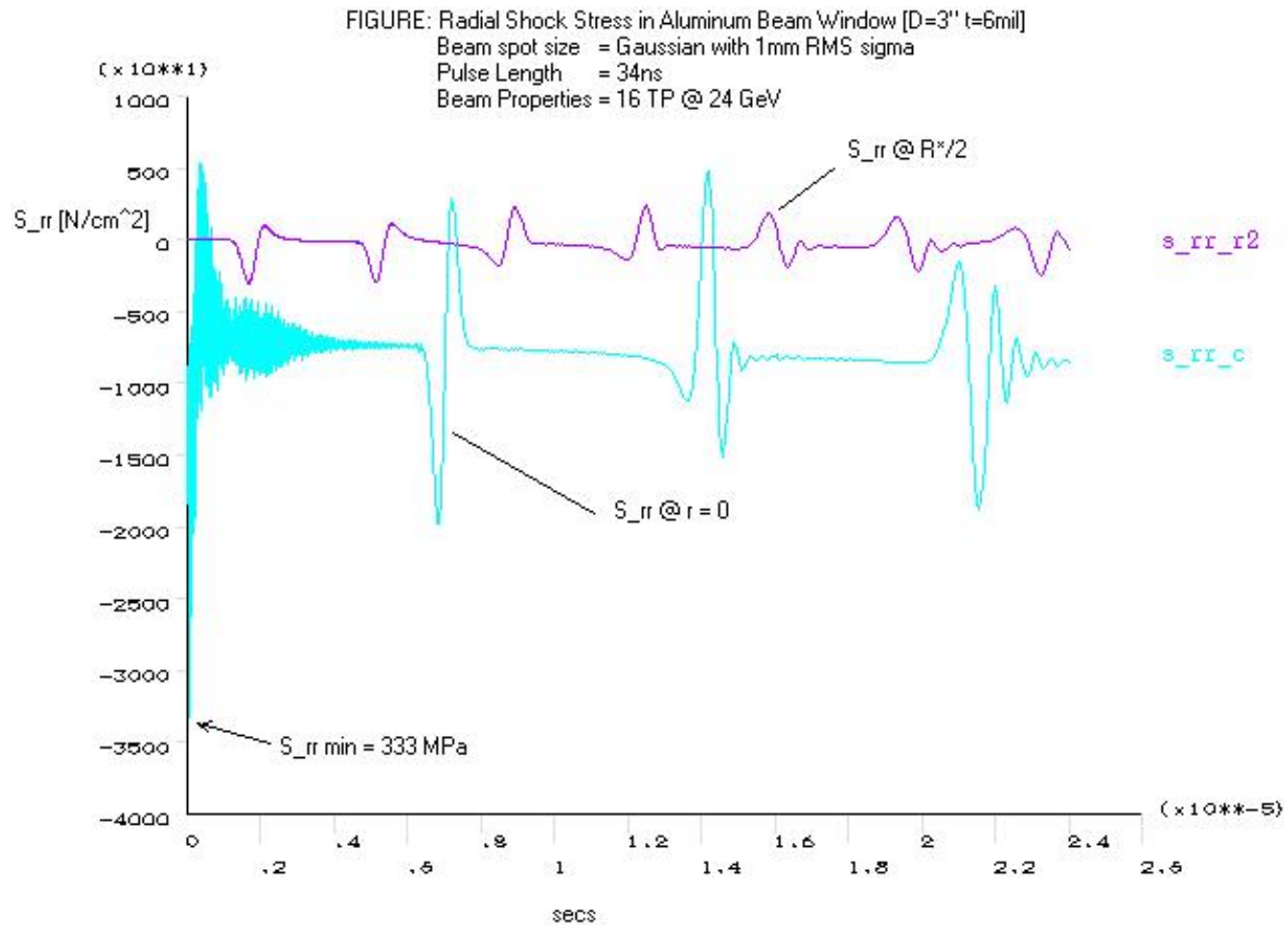
Thermal Shock Analysis of the Exp951 Windows

A3 Line 3-inch diameter and 6-mil thick Aluminum Window



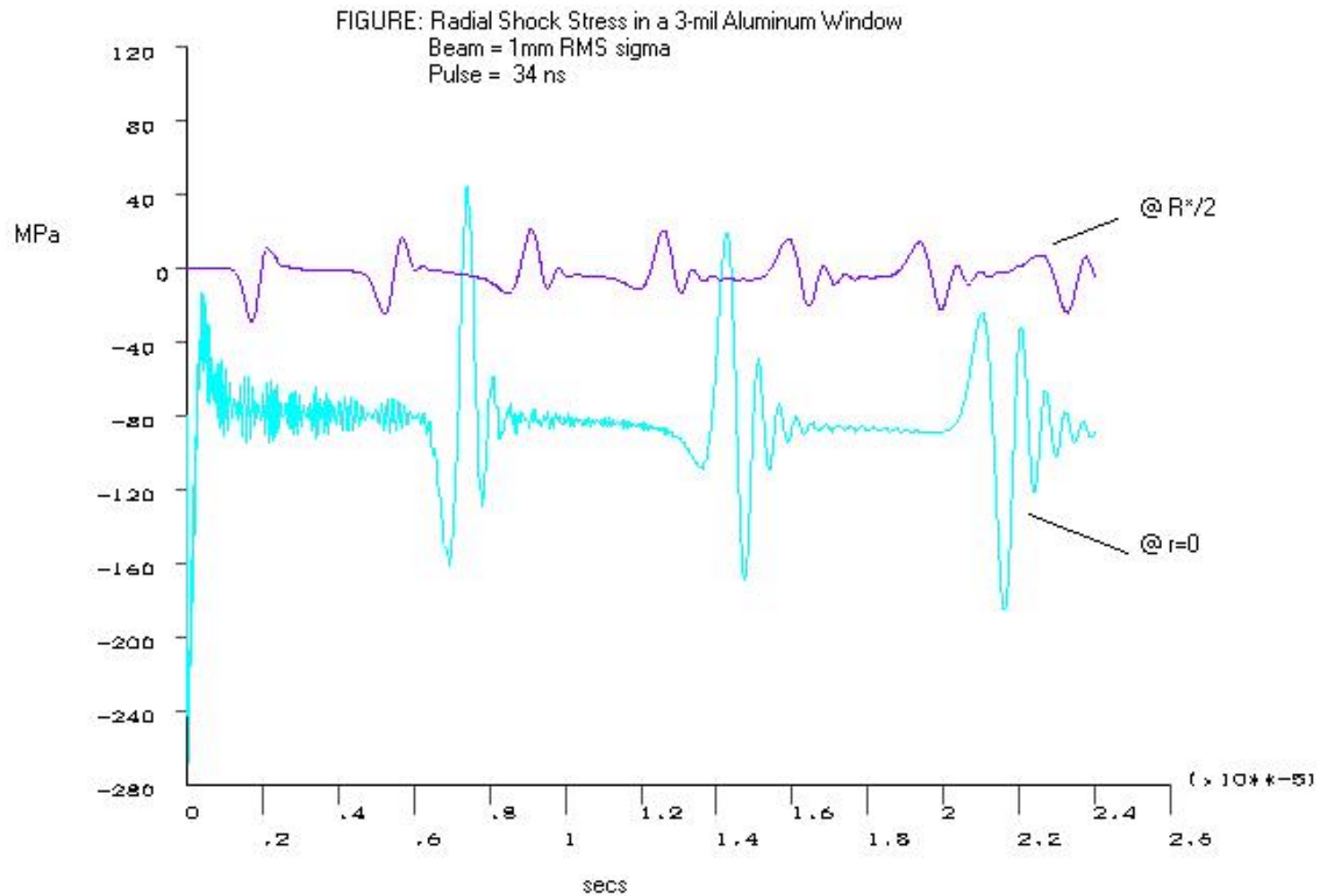
Thermal Shock Analysis of the Exp951 Windows

A3 Line 3-inch diameter and 6-mil thick Aluminum Window



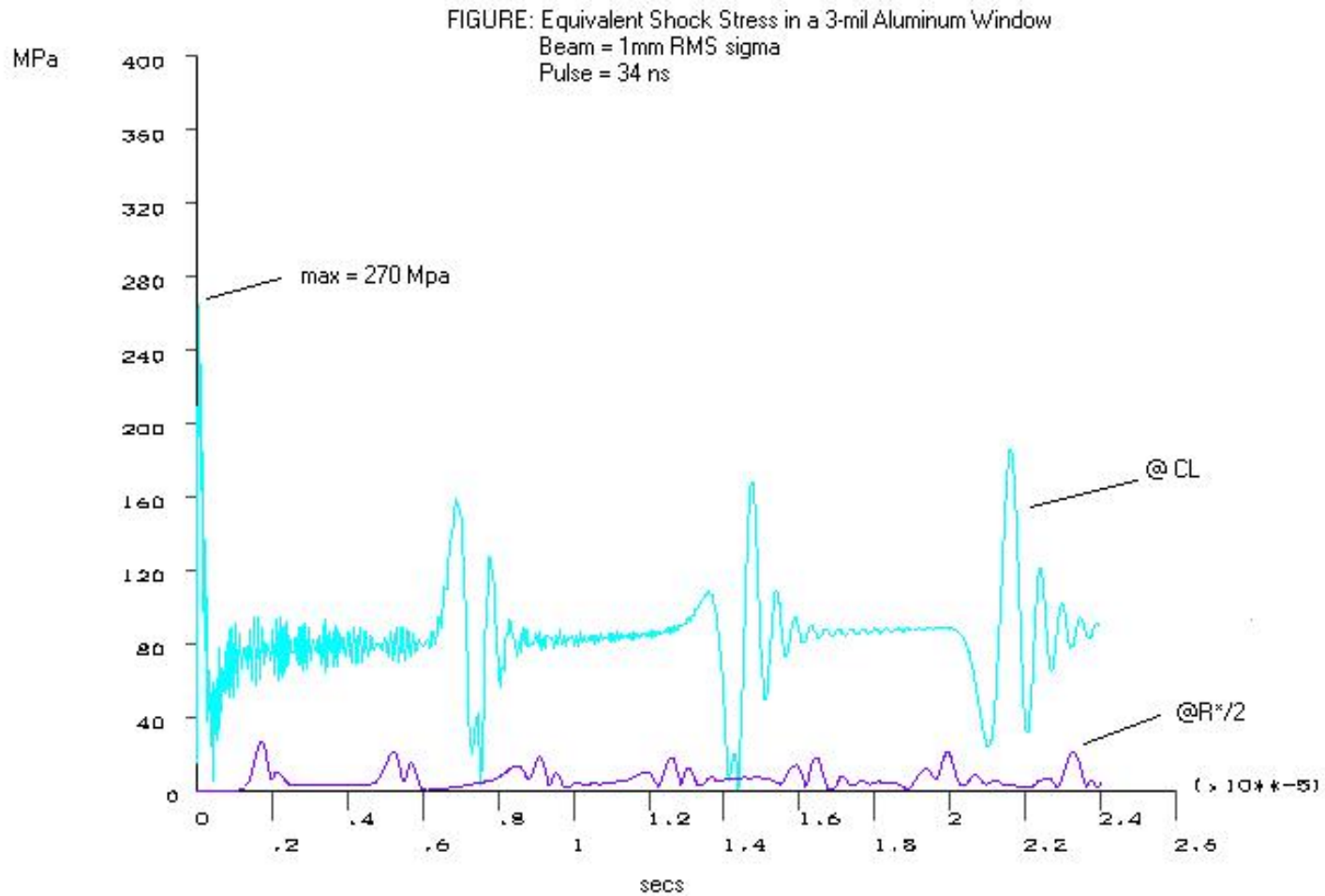
Thermal Shock Analysis of the Exp951 Windows

A3 Line 3" 3-mil Aluminum Window



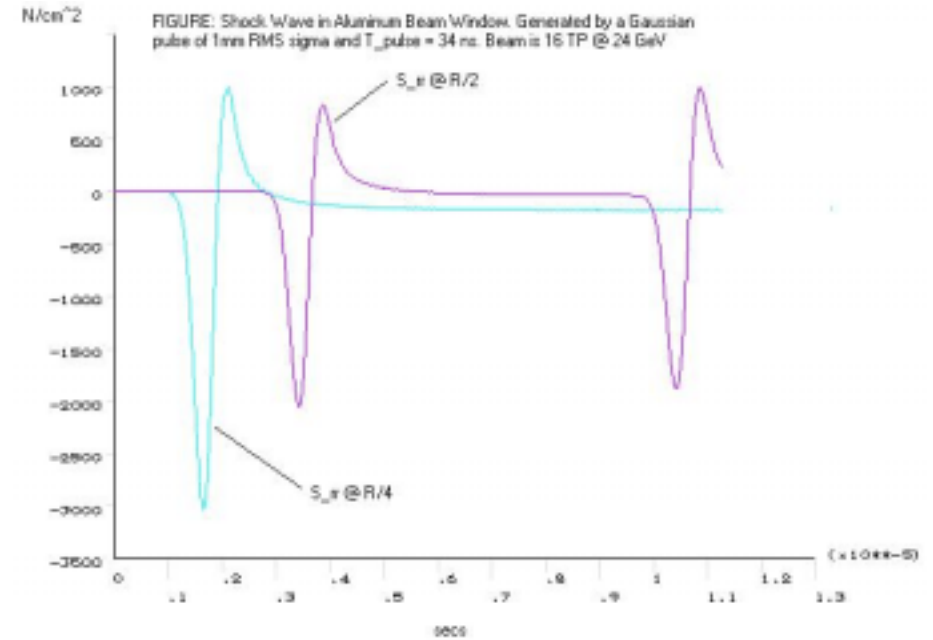
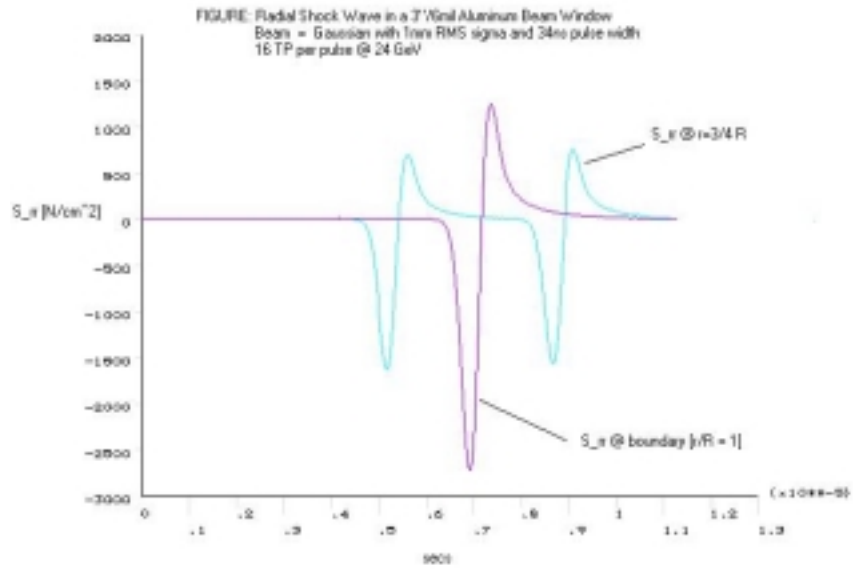
Thermal Shock Analysis of the Exp951 Windows

A3 Line 3-inch diameter and 3-mil thick Aluminum Window



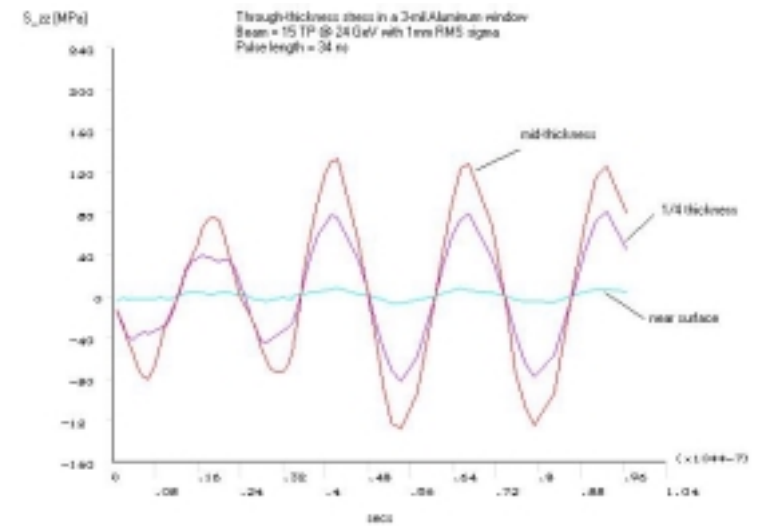
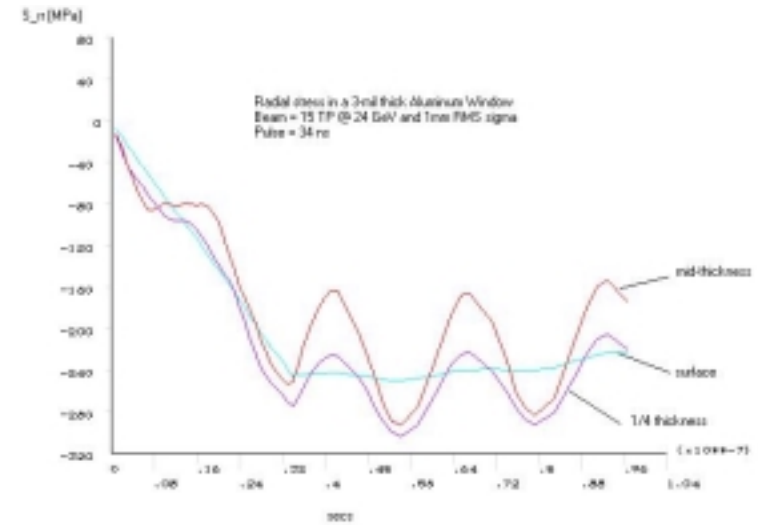
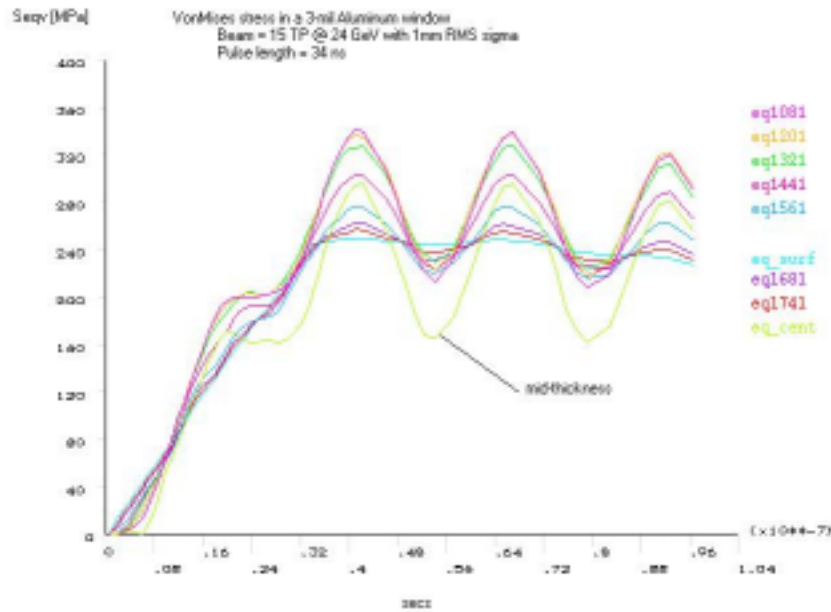
Thermal Shock Analysis of the Exp951 Windows

A3 Line 3-inch diameter ; 6-mil Aluminum Window



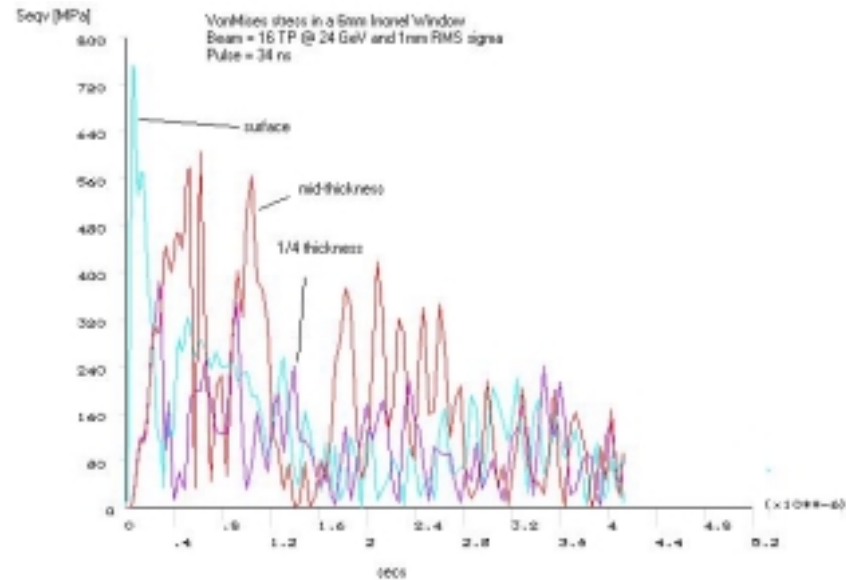
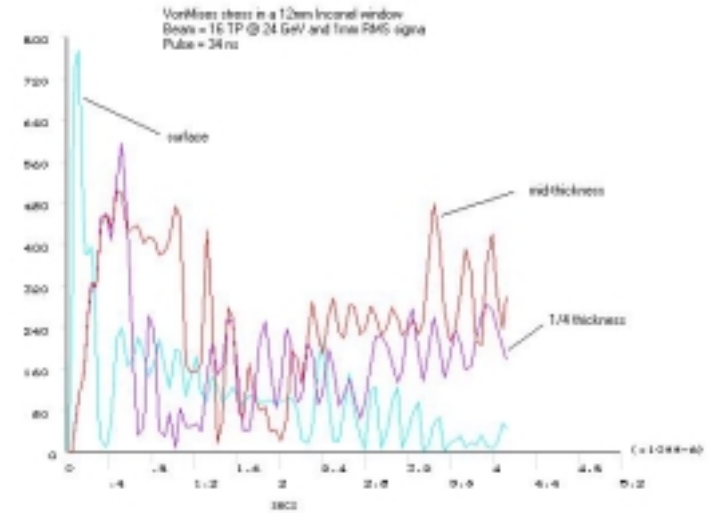
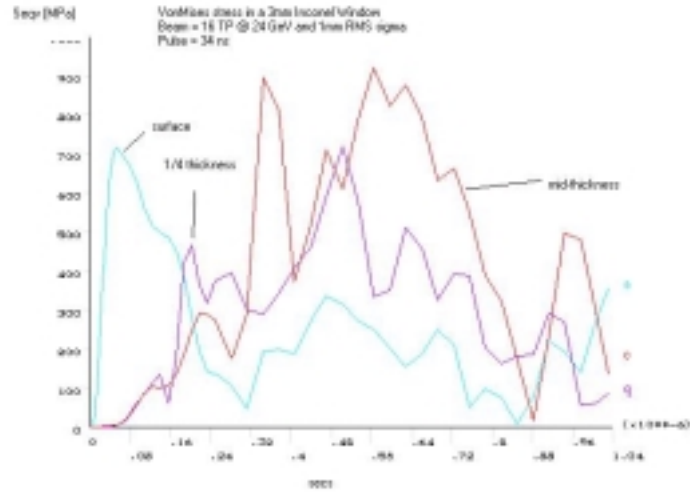
Thermal Shock Analysis of the Exp951 Windows

A3 Line 3-inch diameter ; 3-mil Aluminum Window



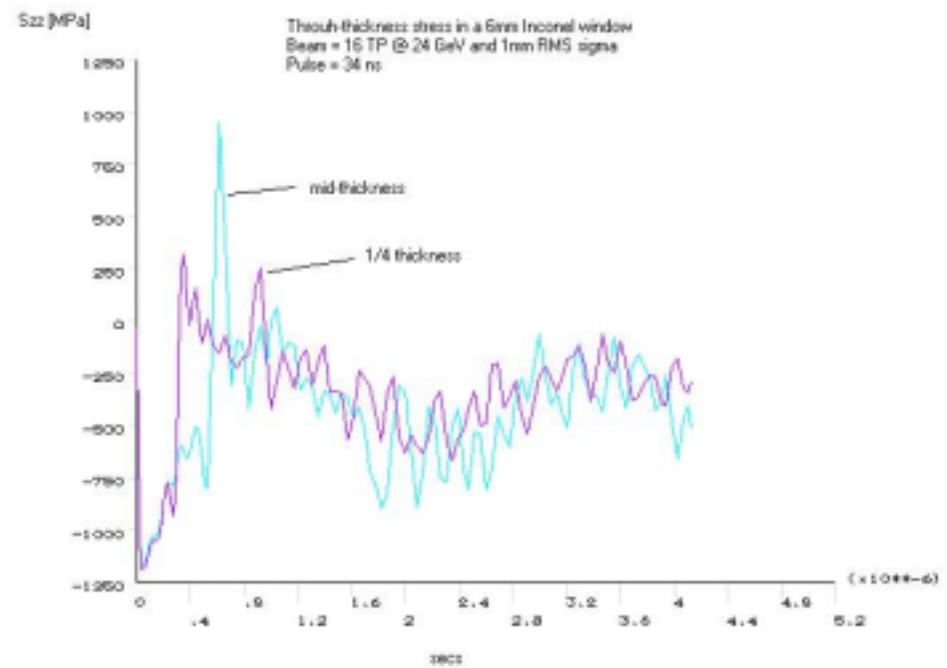
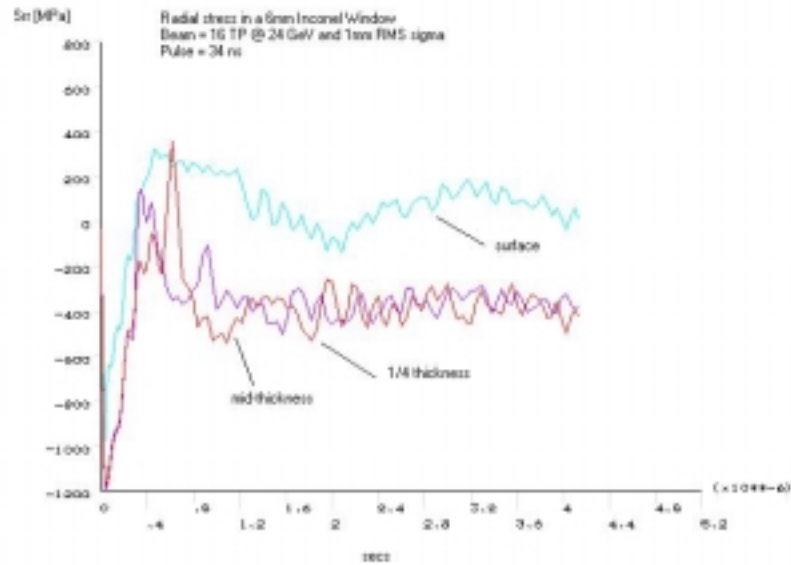
Thermal Shock Analysis of the Exp951 Windows

Inconel-718 Window Analysis



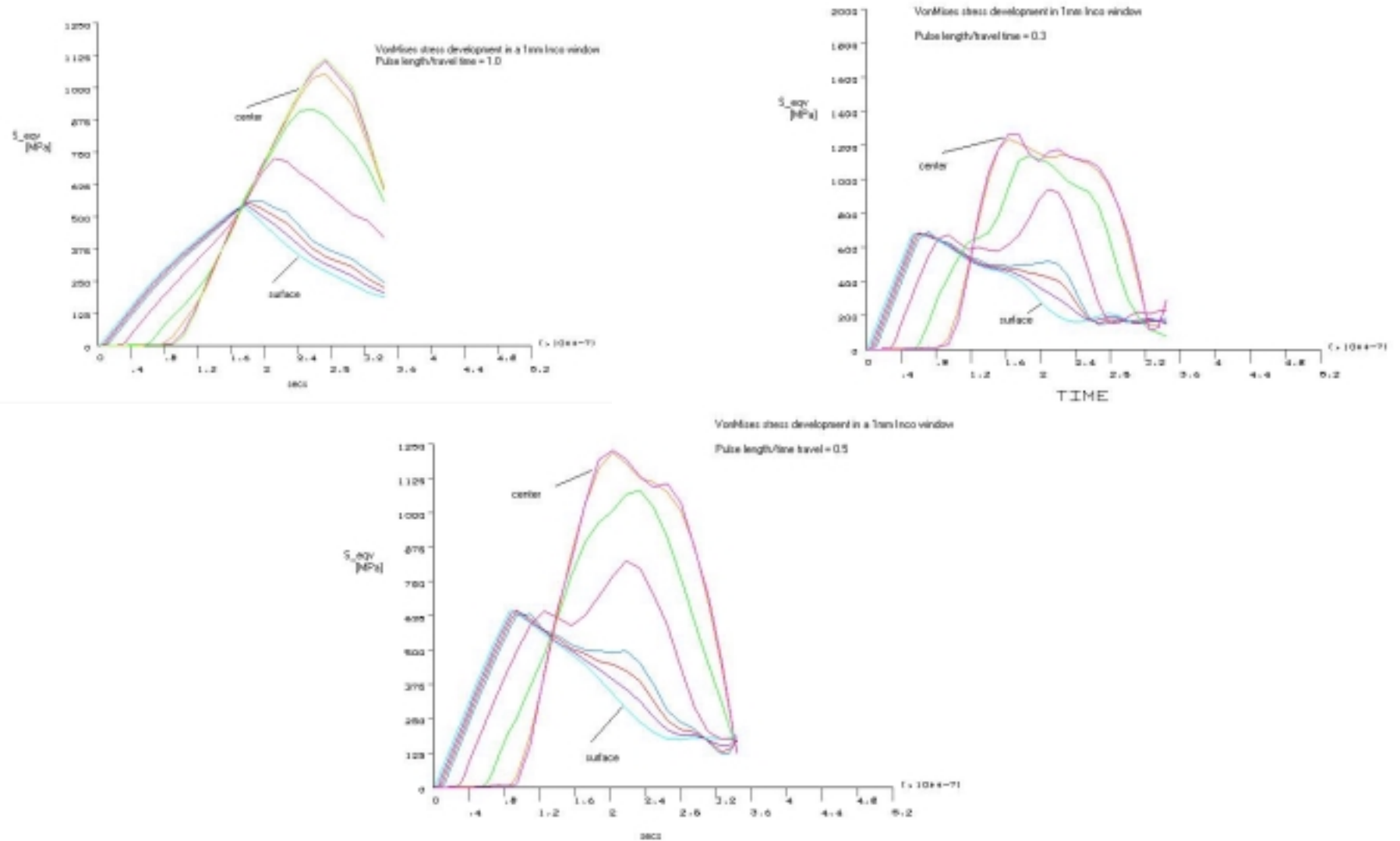
Thermal Shock Analysis of the Exp951 Windows

Inconel-718 Window Analysis



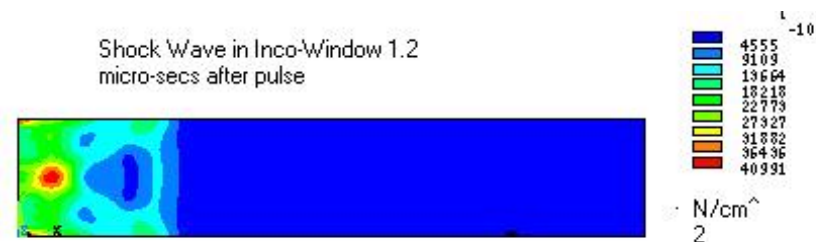
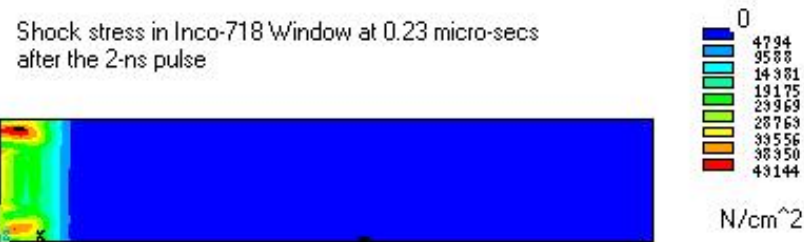
Inconel-718 Window Analysis

Effect of ratio [pulse/period] on shock stress development



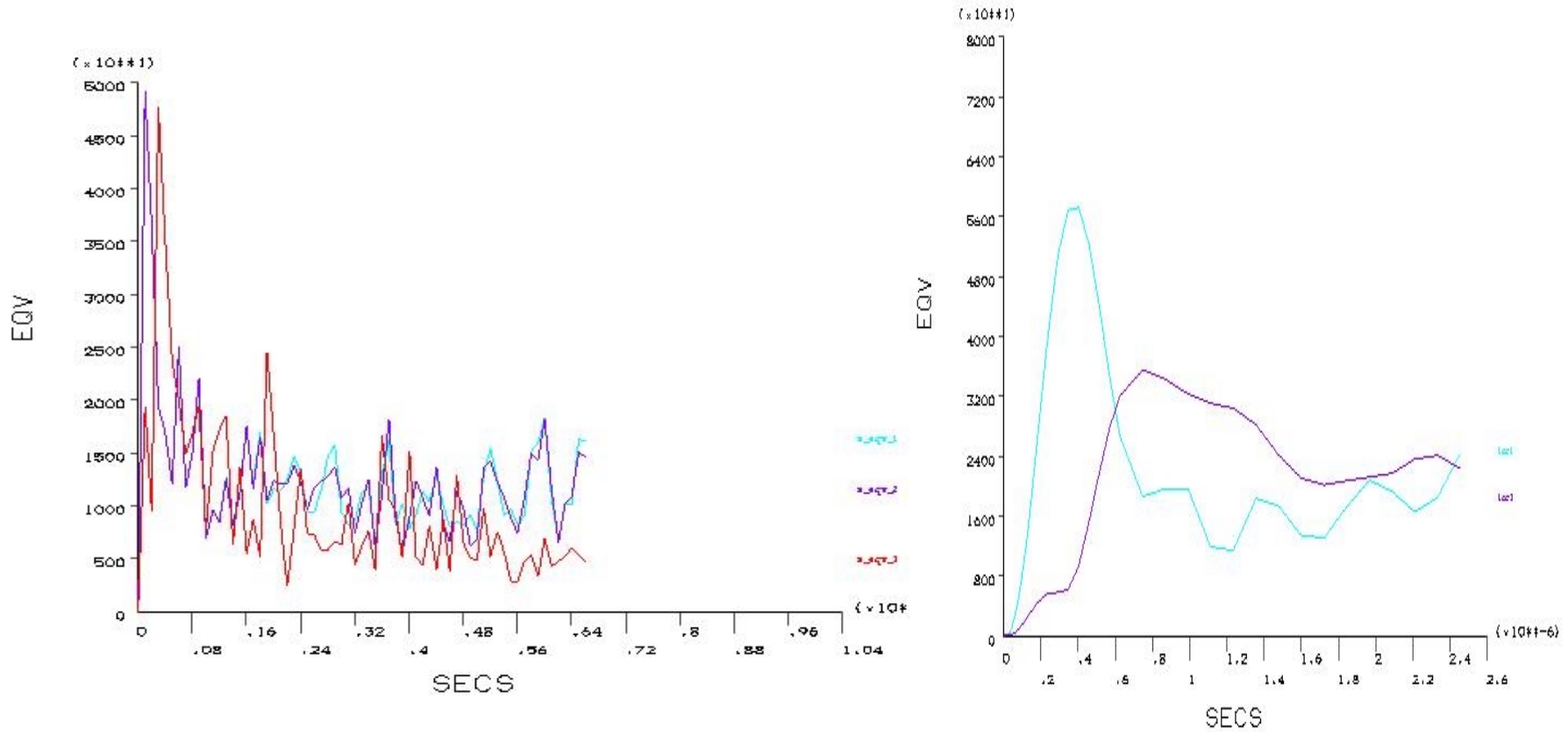
Thermal Shock Analysis of the Exp951 Enclosure Window

Von-Mises stress profiles for Inco -718 window and 2-ns pulse length



Thermal Shock Analysis

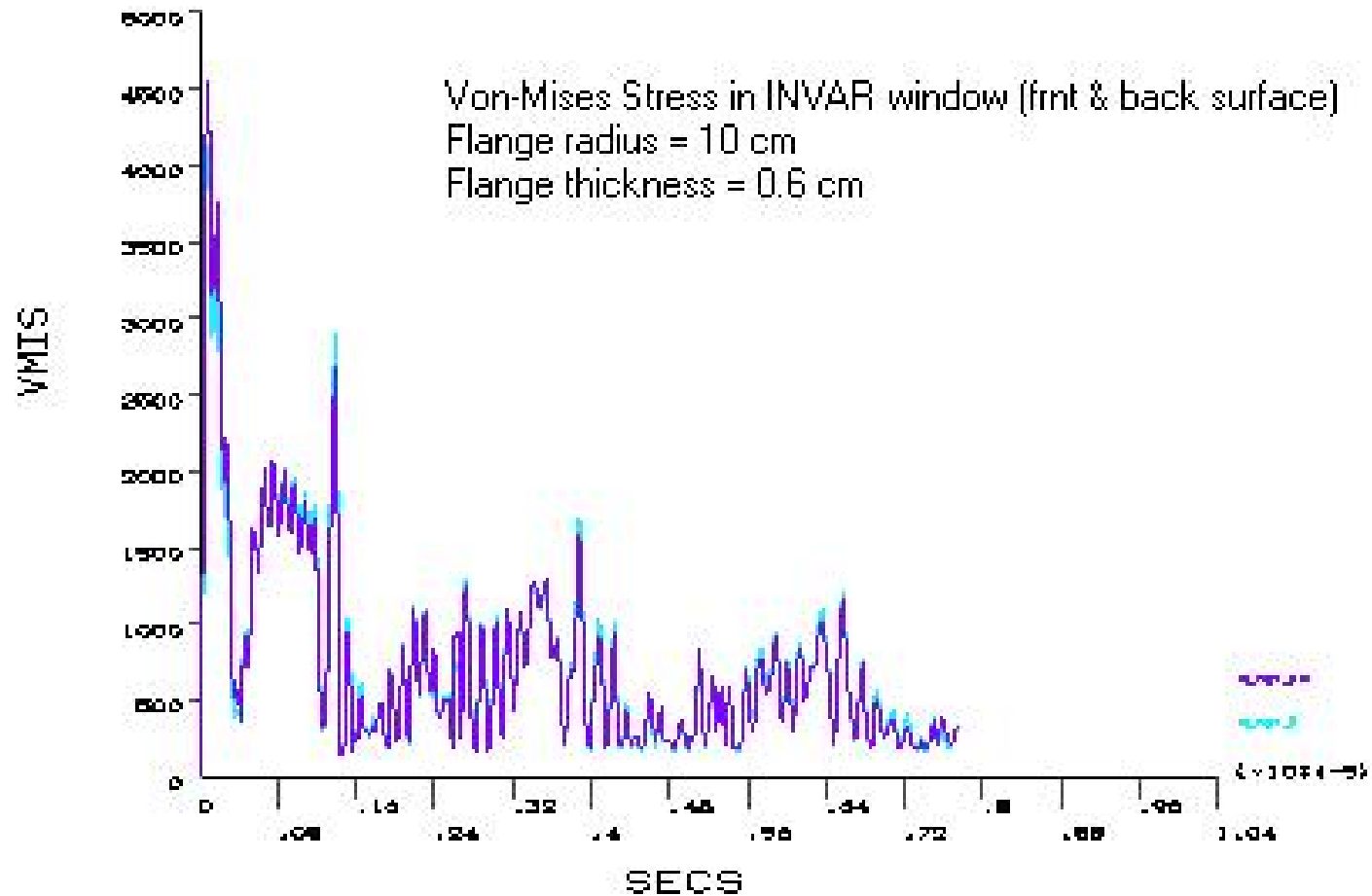
Von-Mises stress profile for steel window



-Mises Stress at locations 1 & 3 following pulse

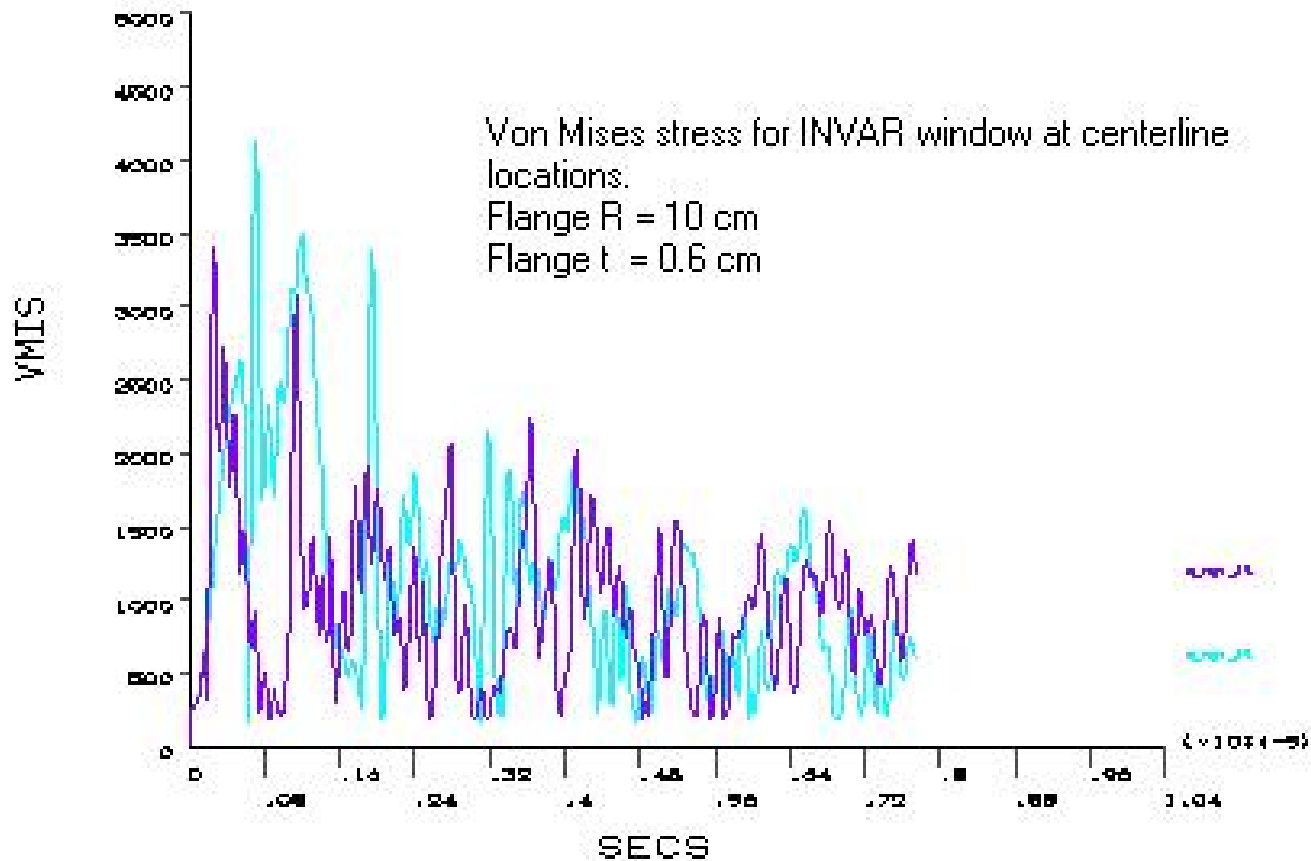
Thermal Shock Analysis

Von-Mises stress profiles for INVAR window



Thermal Shock Analysis

Von-Mises stress profiles for INVAR window



What is Window Failure and how it Impacts on Material Selection & Design

- **Vacuum Window Safety Factor dictated by Buckling Failure**
 - A safety factor of 4 is typical
- **Thermal Shock Failure**
 - enable material to withstand a single pulse
 - design against fatigue failure
- **Conservative estimate of trouble is exceeding the yield strength of material**
 - for catastrophic failure need to exceed ultimate strength
- **Fatigue failure can be short or long-term process**
 - one can barely overcome single-pulse safety and fatigue failure can arise after just few pulses !
 - Through-thickness ringing very important in estimating fatigue due to many cycles of stress it introduces before it dies out

Failure Assessment of E951 Windows

A3 Line Aluminum Windows

- Based on 16 TP/24 GeV beam, **1mm RMS sigma** & pulse = 34ns the peak vonMises stresses are for various thicknesses:
 - 3-mil = 303 Mpa
 - 6-mil = 360 Mpa
 - 12-mil = 436 Mpa
 - 24-mil = 368 Mpa
- Aluminum 5052 has $S_y = 255$ Mpa & $S_u = 290$ Mpa
- Based on latest optics calculations, smallest beam spot in the Aluminum windows of A3 line are much larger than the 1mm RMS sigma providing ample safety factor
- Real beam pulse is triangular (in time space) with larger width (base ~ 100 ns)

Failure Assessment of E951 Windows

Experiment Windows

- Based on 16 TP/24 GeV beam, **1mm RMS sigma** & pulse = 34 ns
 - 1-mm (inconel) = 1360 Mpa
 - 2-mm = 1172 Mpa
 - 3-mm = 920 Mpa
 - 6-mm = 736 Mpa (640 MPa for 68 ns pulse !)
 - 12-mm = 860 MPa
- **Inconel 718 Strength: $S_y = 1034$ MPa & $S_u = 1240$ MPa**
- **Based on latest optics calculations, smallest beam spot at target is smaller than 1mm sigma [0.5mm for x and y]**
 - this will leave no safety factor
 - windows may move upstream and downstream
 - re-consider INVAR or Beryllium
- **Real beam pulse is triangular (in time space) with larger width (base ~ 100 ns)**