

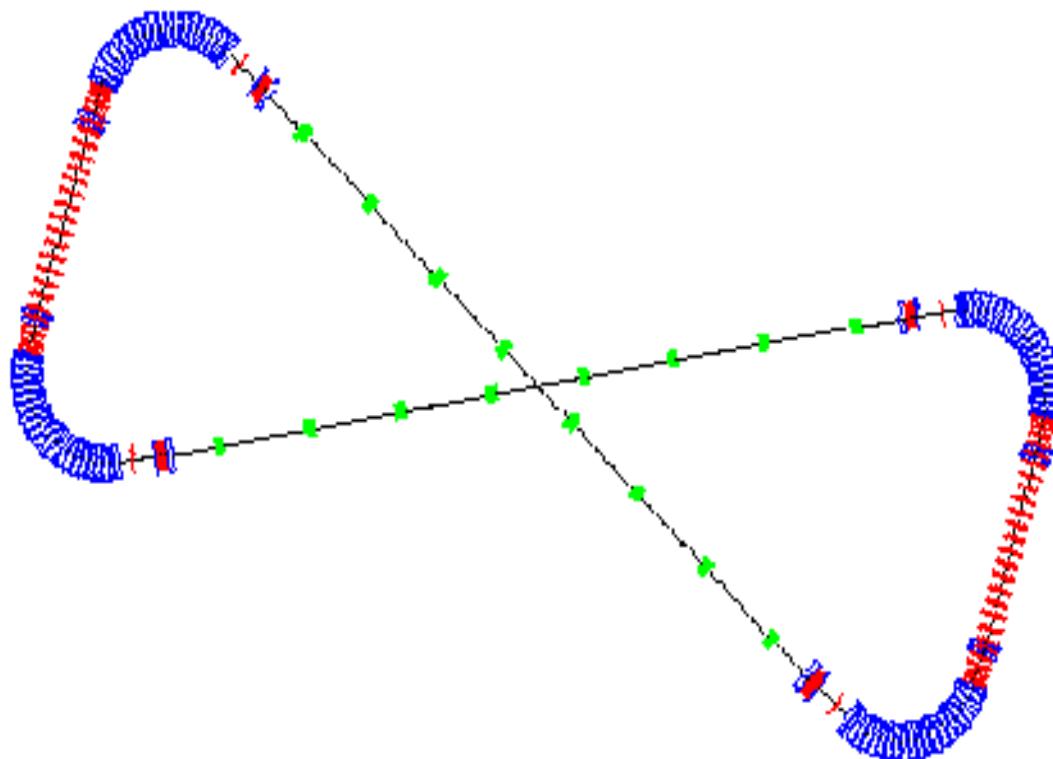
Neutrino Factory, μ^\pm Decay Rings

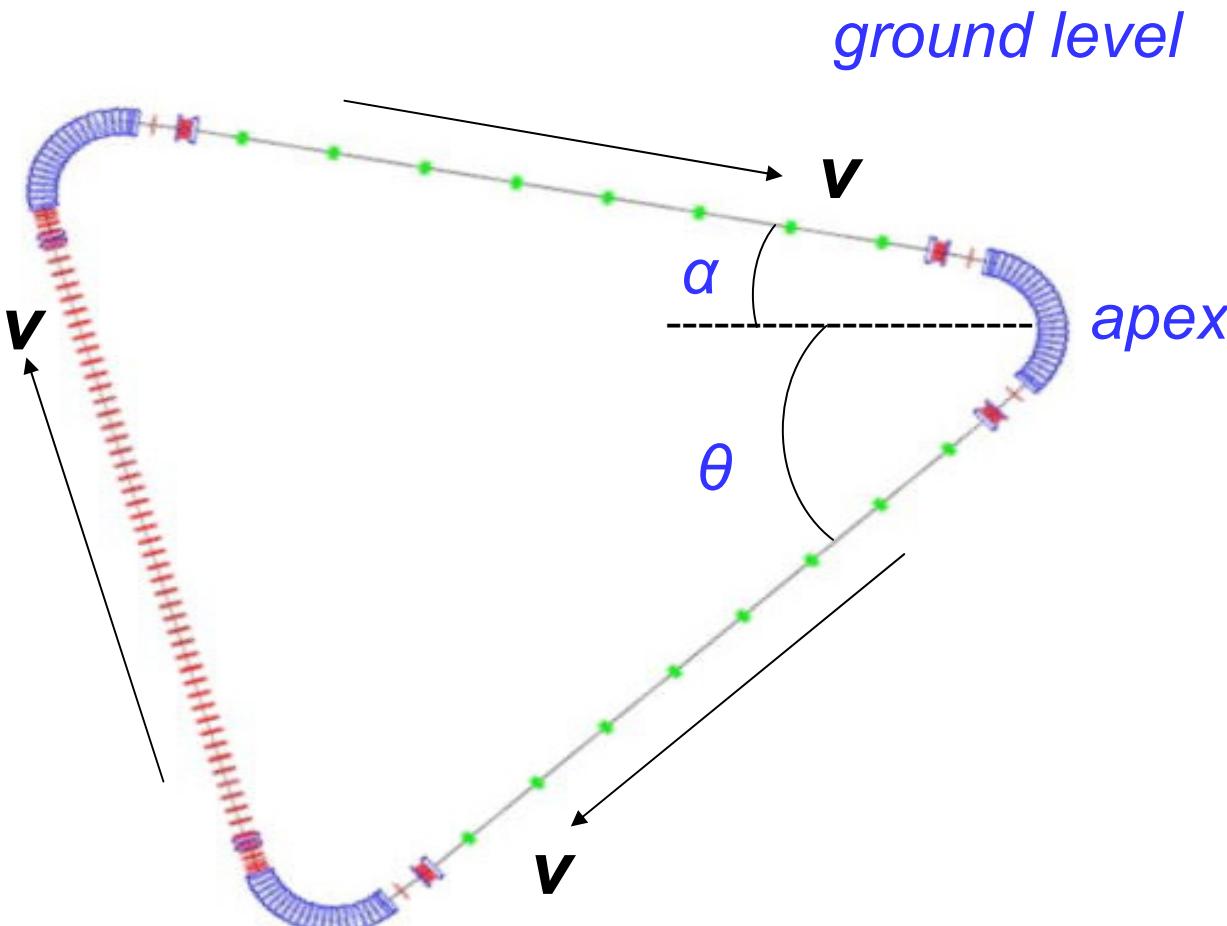
C Johnstone, FNAL, F Meot, CEA, & G H Rees, RAL

Decay Ring Tunnels

- Assume neutrino detectors at 7500 and ~ 3500 km
- The isosceles Δ and bow-tie designs have μ^+ & μ^- beams in two adjacent rings, all in a common tunnel
- Each ring has two production straights, and each of the detectors takes neutrinos from both μ^+ & μ^- rings
- The racetrack ring designs use separate tunnels and this eases the task of finding suitable detector sites
- Each racetrack ring has just one production region, so that each ring is aligned to its own neutrino detector

Bow-tie Decay Ring





$$\sin \alpha = L_1 / 2R$$

L_1, L_2 detector distances

$$\sin \theta = L_2 / 2R$$

R the equatorial radius

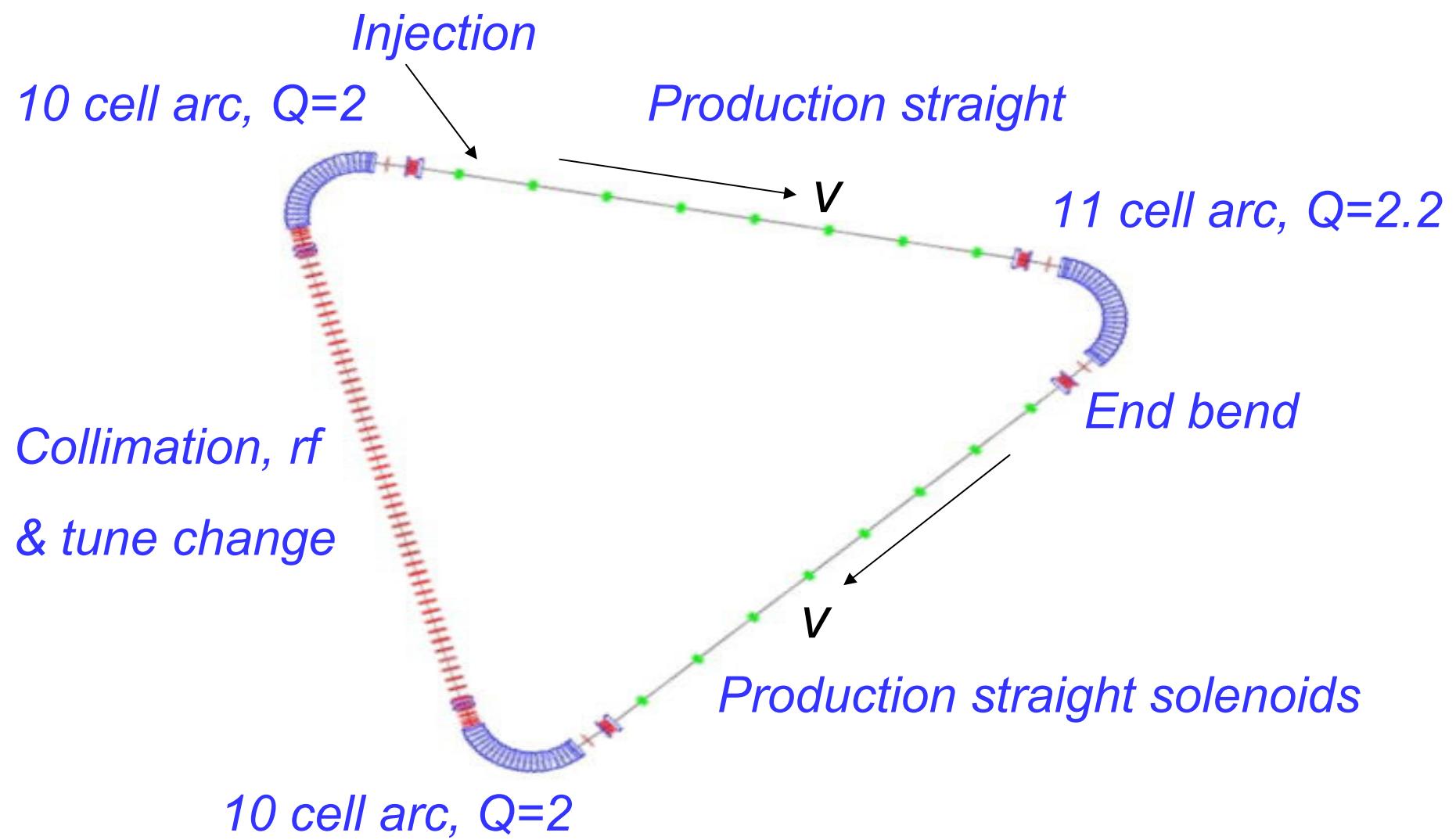
Vertical Plane Layout for 2 Isosceles Triangle Rings

Triangle Ring Production Efficiencies

Best for ν -production efficiency are vertically aligned, adjacent, triangular rings of minimum apex angle, with two detectors in opposite directions, in gnomonic projection. Some inclination to a vertical plane is expected for most pairs of detector sites:

For an RAL Neutrino Factory with two, 1608.8 km circumference decay rings, and neutrino detectors at Carlsbad (7513 km) and:

<i>2nd detector site</i>	<i>Vertical tilt</i>	<i>Apex angle</i>	<i>Production Efficiency</i>
Baksan (3375 km)	30.6°	60.2°	2 x 23.9 %
Cyprus (3251 km)	9.7°	51.7°	2 x 25.0 %
Crete (2751 km)	0.9°	48.6°	2 x 25.4 %



Schematic Plan of Triangle Ring

Triangle Apex Angles

- *The number of arc cells sets the apex angle of triangle*
- *Smallest apex angle is for a triangle in a vertical plane*
- *Detectors at 7500 & 3500 km need ~ 50° apex angles.*
- *Groups of five cells are used for control of chromaticity*

Arc cells	Apex angles	Circumf.	Prod. straight	Efficiency
10+10+10	~60.0°	1608.8 m	383.7 m	2 x 23.9 %
10+10+11	52.8°	1608.8 m	398.5 m	2 x 24.8 %
10+10+12	~45.4°	1608.8 m	415.3 m	2 x 25.8 %
10+10+16	~22.4°	1608.8 m	482.0 m	2 x 30.0 %

Features of Triangle & Bow-tie Rings

- *Designed for MW intensities:* $\beta\gamma A = 30 (1.5)^2 (\pi \text{ mm } r)$
- *Uses a beam loss collection system for the muons*
- *Uses combined not separated function magnets in arcs*
- *Uses solenoid focusing in the two production straights*
- *Uses bend units at the ends of the production straights*
- *Uses box-car stacking for trains of $80 \mu^+$ & μ^- bunches*
- *Uses matching section bends to suppress dispersion
(these influence the production straight orientations).*
- *Lattice is modified when upgrading from 20 to 50 GeV
(Some magnets changed & ring re-aligned for 50 GeV).*

Production Straight Focusing

- A figure of merit for lattice focusing is: $1 / (\gamma\beta_{max})$
For a FODO thin lens: $\gamma\beta_{max} = 2/(1 - \sin \mu/2) > 2$
- For an OSO lattice of weak solenoids: $\gamma\beta_{max} \approx 1$
So, β_{max} (OSO) may be one half of β_{max} (FODO)
- Eight, 4.8 m solenoids in 398.5 m straight sections:
At 20/50 GeV, $\beta_{max} \approx 99/163$ m for 4.3/6.4 T solenoids

Production Straight End Bends

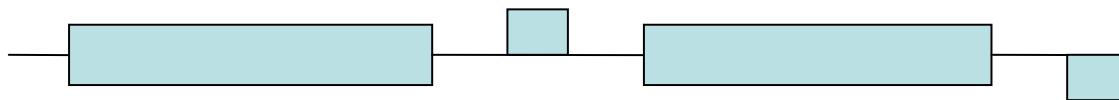
- *Neutrinos, from μ^\pm beyond the bends, miss detectors. Bends introduce dispersion, however, into the lattice.*
- *Matching of dispersion to arcs requires further bends, which are different for the 20 and the 50 GeV lattices.*
- *Small changes in the arc bend angles are required to preserve the orientation of the 2 production straights.*
- *Dispersion in the third straight is also affected and so modified matching is needed for the 50 GeV upgrade.*

Neutrino Production Straights

	20 GeV	50 GeV
<i>Muon norm rms emitt (π mm r)</i>	4.80	4.80
μ to ν divergence angle ratio, R	0.10	0.12
<i>Number of solenoids</i>	8	8
<i>Solenoid fields (T)</i>	4.27	6.37
<i>Length of solenoids (m)</i>	4.75	4.75
<i>Half of inter space (m)</i>	21.1	21.1
β value at beam waist (m)	~94.3	~160.3
β (max) in solenoid (m)	~99.1	~163.1

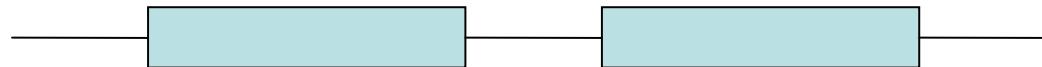
Arc Cell Design

Old CERN 10,10,10 FODO design:

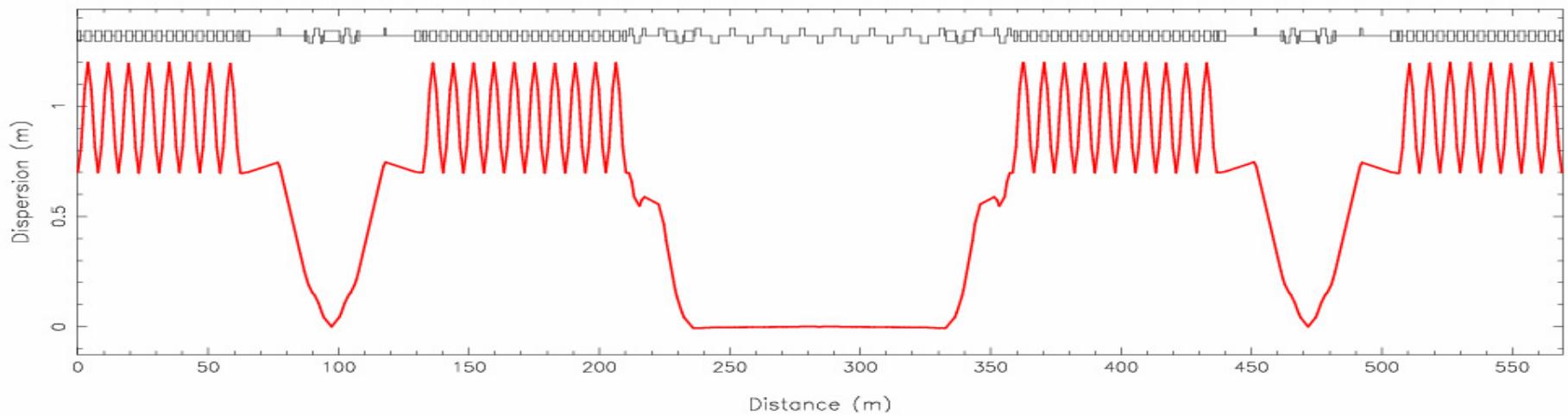
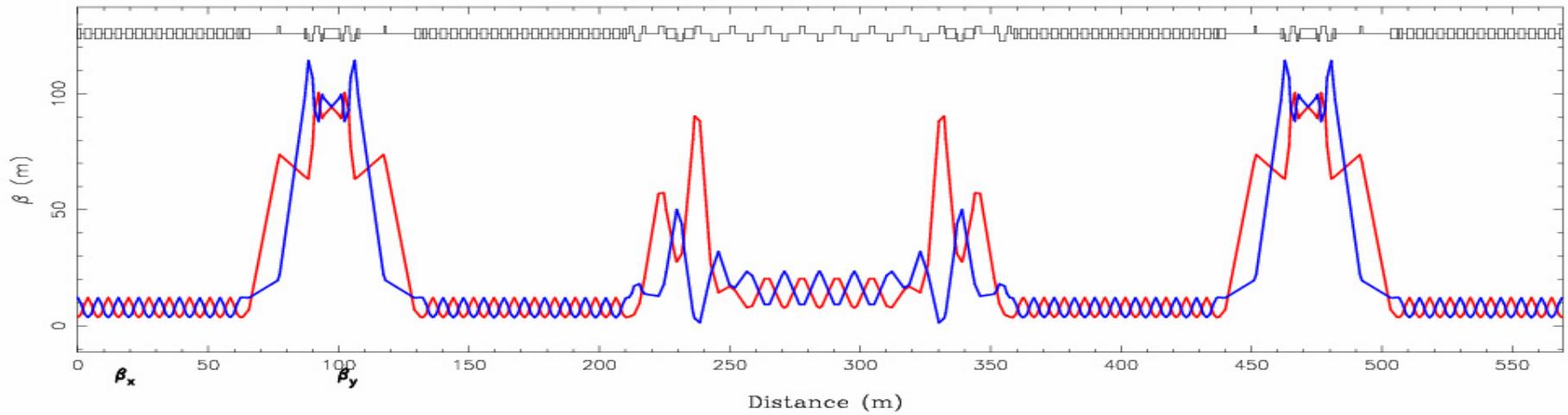


Lengths = 9.703, 0.7 m, $\mu = 90^\circ$, $\beta_{max} = 16.6$ m, $D_{max} = 1.4$ m.

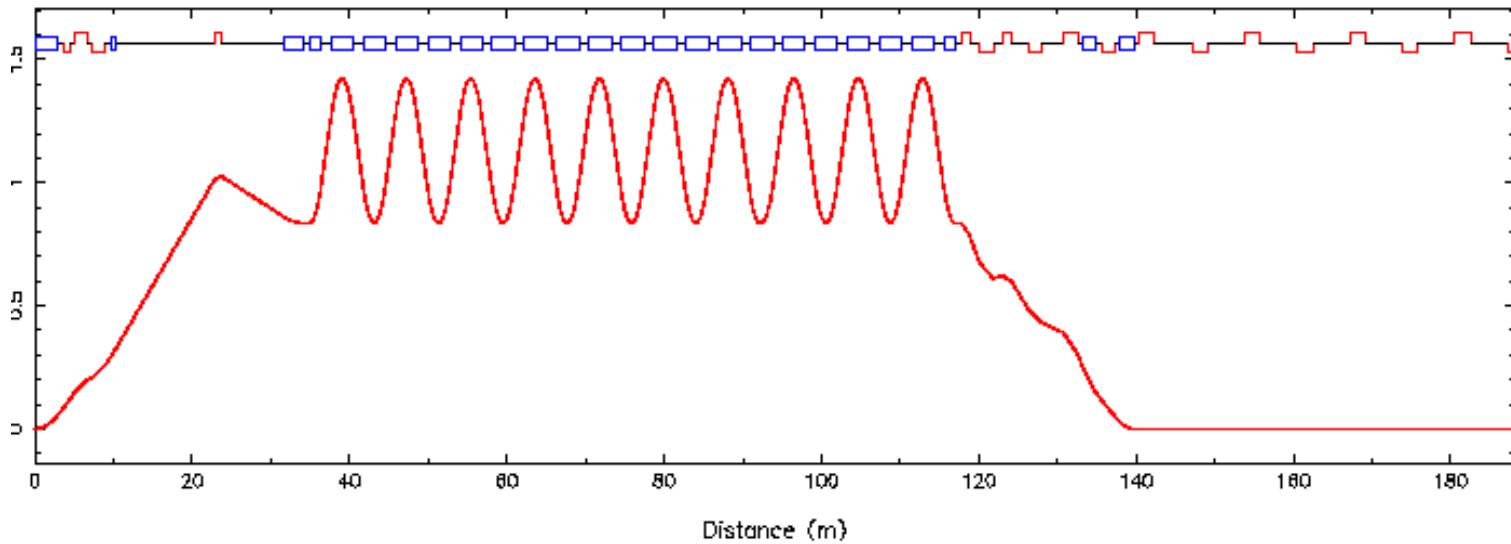
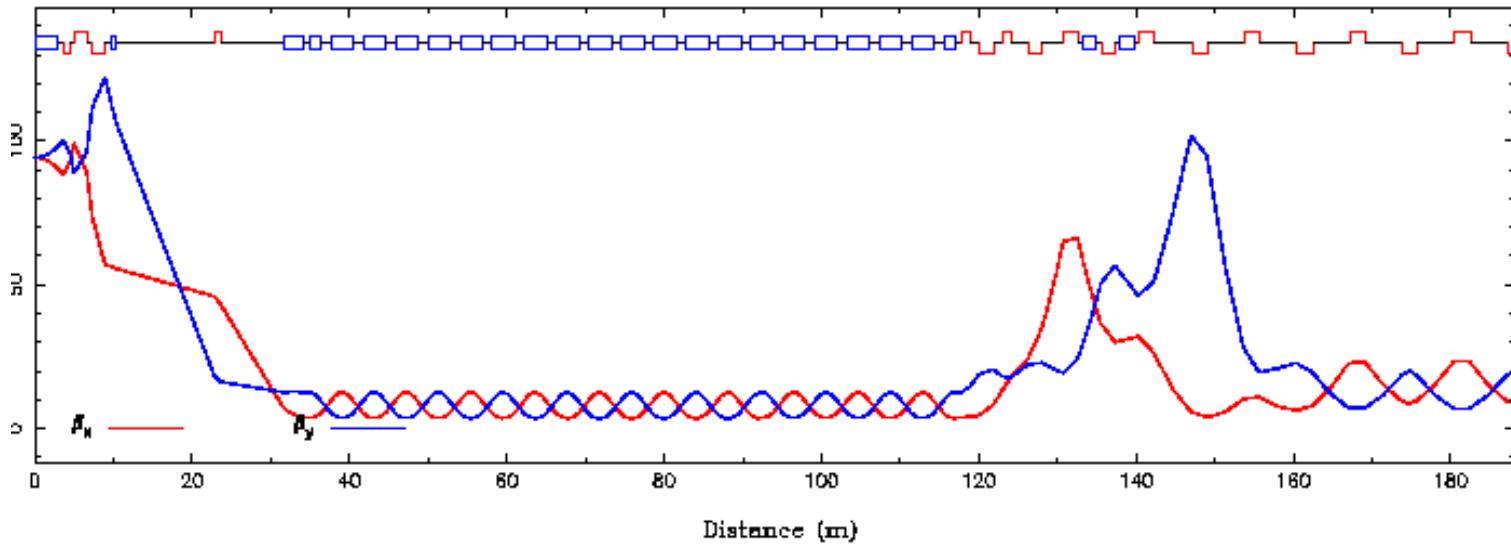
New 10,10,11 (BF)O(BD)O design:



*Lengths = 8.200, 1.2 m, $\mu = 72^\circ$, $\beta_{max} = 12.7$ m, $D_{max} = 1.4$ m.
(space for cryostat ends, valves, correctors, diagnostics, vacuum & cooling)*

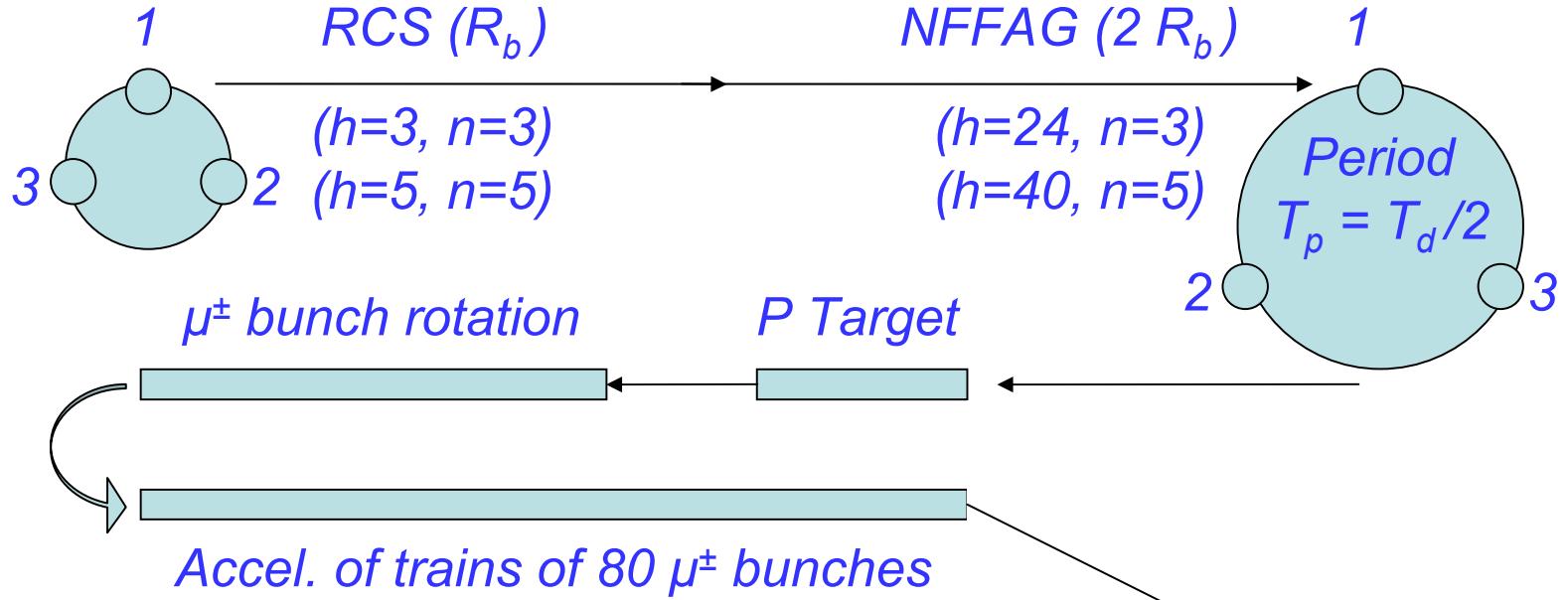


Triangle ring lattice functions outside production straight.



Bow-tie lattice functions outside production straight

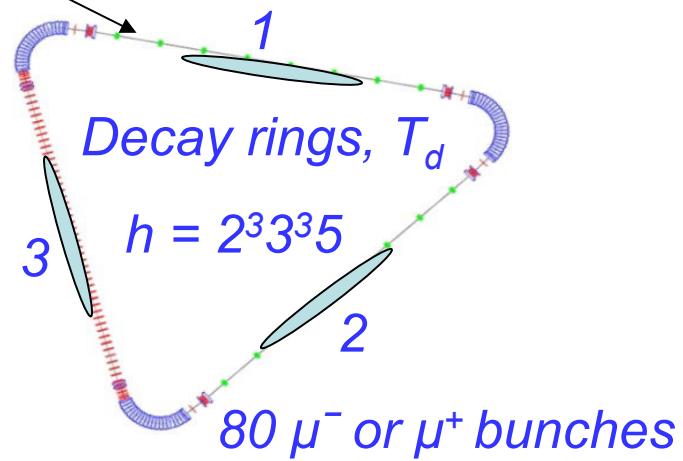
Bunch Train Injection



NFFAG ejection delays:
 $(p + m/n) T_d$; $m = 1$ to n ($= 3, 5$)

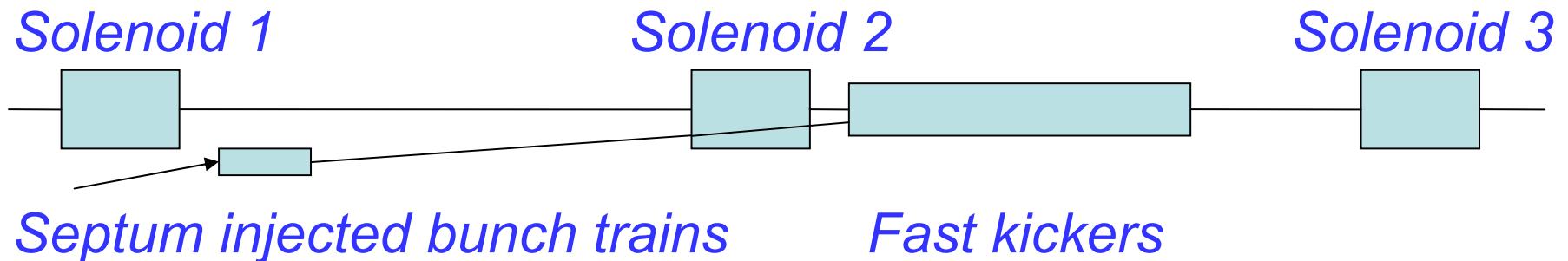
Pulse < 40 μ s for liquid target

Pulse > 60 μ s for solid targets



Injection of n Trains of $80 \mu^\pm$ Bunches

Production straight of superconducting solenoids



R & D is needed for the high stored energy & power, pulsed kickers, with n (5 or 3) injected bunch trains per 50 Hz cycle. Rise & fall times are ~ 650 ns for the large acceptance rings.

Injection Parameters

$$\theta_k \approx \sqrt{\beta_k} (\sqrt{A} + \sqrt{\varepsilon} + t_s / \sqrt{\beta_s}) / (\beta_k \sin \Delta\mu + \frac{1}{2} NL \cos \Delta\mu)$$

$$NLI \text{ (number, length, current)} = 2 (B\rho) \theta_k \sqrt{(A \beta_v)} / \mu_0$$
$$NTV \text{ (number, rtime, voltage)} = 2 (B\rho) \theta_k \sqrt{(A \beta_k)}$$

At 20 GeV, for $A, \varepsilon = 354.7, 157.7 \text{ mm mr}$, $t_s = 15 \text{ mm}$
 $\beta_s \approx \beta_k \approx \beta_v \approx 95.0 \text{ m}$, $\Delta\mu \approx 25^\circ$, $B\rho = 67.06 \text{ T m}$, $T = 460 \text{ ns}$:

Use 7, shorted, 3m, 10Ω delay line, push pull K with
14 x [50 kV PFN, 5 kA pulsers & 10Ω feeders] /ring.

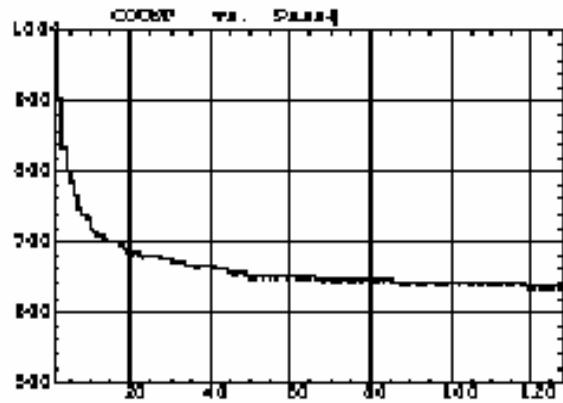
$$NL = 24 \text{ m}, \theta_k = 6.47 \text{ mr}, I = 5000 \text{ A}, NTV \sim 0.18 \text{ V s}$$

Muon Beam Loss Collection

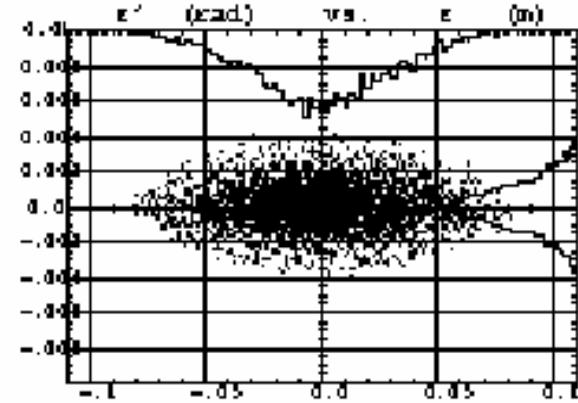
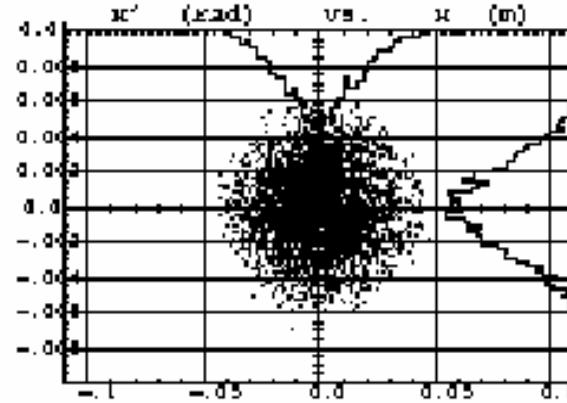
- Due to the e^\pm losses after μ^\pm decays, the warm bores of S/C arc magnets have to be cooled, & clad with Pb. (The cladding absorbs > 80% of the e^\pm beam power.)
- Direct μ^\pm wall loss also leads to magnet heating, and to minimise this, μ^\pm loss collection is proposed, with primary and secondary collimators in 4 FODO cells at the centre of the short straight section of the ring,
- Primary collimators are set for : $\beta\gamma A = 30$ ($\pi \text{ mm } r$). and ring acceptances are: $\beta\gamma A = 30 (1.5)^2$ ($\pi \text{ mm } r$).

RF System to Contain Bunch Structure

- An RF system is needed only if $n = 5$ & $\Delta p/p > \pm 2.5\%$
Injected bunches may expand in phase until $\Delta\varphi = \pm 90^\circ$
- The inductive wall fields are defocusing as γ is $> \gamma_t$
The required net RF containing field scales as $(\Delta p/p)^2$
- 30 MV, 201 MHz containing fields/ring for $\Delta p/p = \pm 1\%$
3 cavities, 2x1 MW input couplers for ~ 5.4 MW per ring
- Cavities on tune; loading alters with each injected train
Reflected power is dissipated in the circulator loads
- The dynamic aperture improves for lower $\Delta p/p$ beams



Survival ($\varepsilon=60$ (π) mm r , $\Delta=\pm 4\%$) Horizontal phase space



Vertical phase space

Tracking of μ^\pm with sextupoles in the triangle ring arcs.

Tracking the linear machine shows very weak coupling and well-behaved transverse motions for $\Delta p/p = \pm 4\%$. The effect of machine errors is next to be determined.

Parameters for 52.8° Apex Angle Triangle Rings

- Circumference of decay rings: 1608.8 m
- Length of production straights: 398.5 m
- Production straight efficiency: $2 \times 24.8\text{ \%}$
- μ to ν angle ratio at 20 GeV: 0.098
- μ to ν angle ratio at 50 GeV: 0.119
- Max β in the ring at 20 GeV: 120.0 m
- Max β in the ring at 50 GeV: 184.0 m
- Q_h and Q_ν values at 20 GeV: $13.37, 13.18$
- Q_h and Q_ν values at 50 GeV: $13.19, 12.82$

Triangle Design Summary

- An outline design has been made for 2, isosceles triangle, 20 (potentially 50) GeV, μ^\pm storage rings
- The MW rings have large $\beta\gamma A$, at $30 (1.5)^2 (\pi \text{ mm } r)$.
 $C = 1609 \text{ m}$, $L = 398 \text{ m}$, $\xi = 2 \times 24.8\%$, 52.8° apex Δ .
- Production straight solenoids give lower beam sizes.
 μ to V angle ratios are 0.10 & 0.12, at 20 & 50 GeV.
- Injection difficult for uncooled ($45 \pi \text{ mm } r$) μ^\pm beams.
F Meot is tracking to find dynamic aperture with errors.

Vertical Bow-Tie Decay Rings

Advantages:

- *A reduced vertical tunnel depth of ~ 300 m (~ 435 m for triangular and racetrack rings)*
- *A higher V production efficiency of 52.6% (49.6% for triangular rings and 38.2% for racetracks)*
- *A greater choice of the opening angle around 50°*

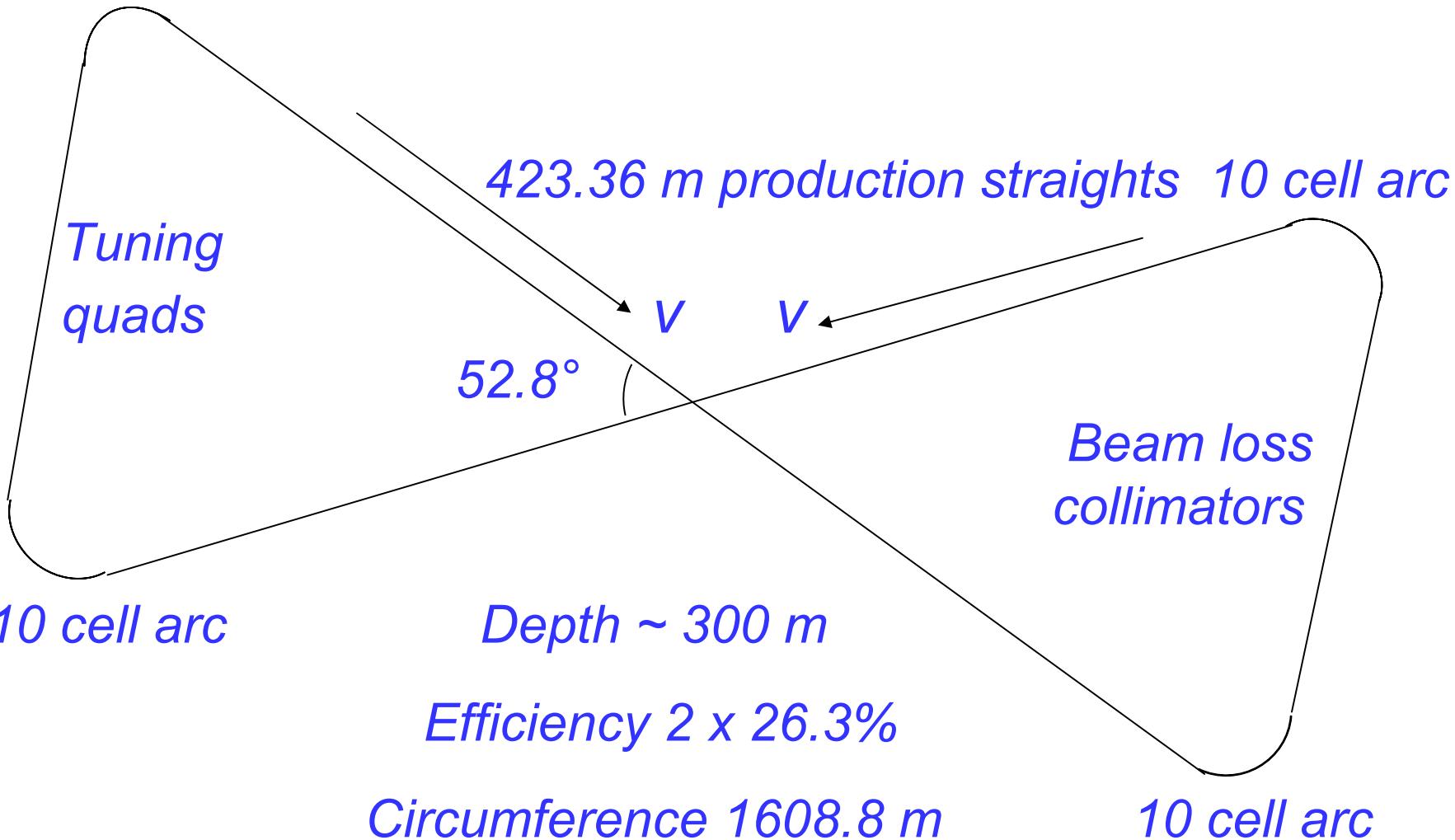
Disadvantages

- *A larger number of main bend cells are required (40) (31 for comparable isosceles triangle, shaped rings)*

*Solenoids to give decay of the muon polarisation?
Possibility to sit on intrinsic depolarising resonance*

Vertical Bow-Tie Decay Rings

10 cell arc



Relative Costs

Ring designs have arcs, match sections & production straights all interchangeable (in principle). Thus, the cost issues are:

The additional bending and fewer quads for the bow-tie rings.

The reduced depth of the tunnel needed for the bow-tie rings.

The additional tunnel (smaller diameter) for the racetracks.

The extra beam lines and services for the racetracks.

For equivalent yield racetracks, power increases needed are:

38% for proton driver (4 to 5.5 MW) and for μ^\pm accelerators.

Ring Comparisons

1. *If suitable detector sites can be found, the triangle or bow-tie shapes are favoured.*
2. *If suitable detector sites are not available, racetracks in separate tunnels are needed.*
3. *If designs 1 and 2 are both proposed, the former has the following advantages:*
the need for only one tunnel and a larger neutrino production efficiency (which is > the gain of adding μ^- beams).