Workshop on High-power Targetry for Future Accelerators

Summary

Solid Targets

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•There were many presentations with useful information concerning solid targets even if not specifically about solid targets.

•It is not possible to cover every presentation - pick out the important points as I see it.

Crucial information for designing a target (and surroundings):

- •the energy density distribution
- •the radioactivity inventory
- •materials and irradiation properties
- •safety issues

Nikoli Mokhov

Very detailed presentation on target interactions, energy depositions etc and accuracy of the various codes and their areas of strength and weakness.

Lauri Waters MCNPX and TRAC codes

Richard Werbeck Safety issues - some real life examples

John Haines Safety issues at SNS

Eric Pitcher Fuels and materials test station.

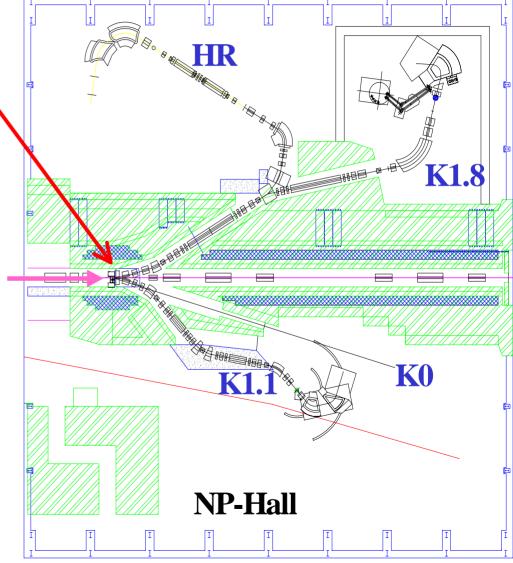
Yoshikazu Yamada, (KEK) JPARC Main Ring Targets

Rotating nickel target for kaons with an energy density of 5300 Jcm⁻³. Water cooled (gas cooling also considered). Novel design - simple water cooling. Consideration of total design, windows, containment, activation, shielding and remote handling.

Possible problems due to corrosion.

Target and secondary beam lines

Production target : T1 Rotating Nickel disks •thickness: ~54 mm •radius: ~24 cm cooled by water developed by Y.Yamanoi et. al. **Proton** beam



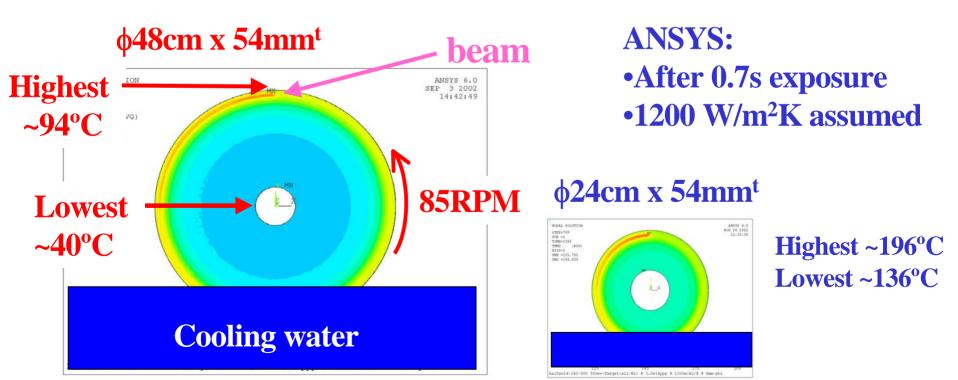
Design of T1

- **1.3x10²¹** protons/year on Target (4000 hours/year)
- •Radiation shielding
- •Kadiation shielding •Max. yield of secondary beam $\} \Rightarrow 30\%$ interaction
- •Temperature rise
- •Temperature rise •Point source for secondary beam } ⇒ Ni target *no rotation*

	length of 30% interaction (cm)	max. heat density (J/cm ³)	density (g/cm ³)	specific heat (J/g/K)	temperature rise by a pulse (K)		
Pt	3.15	25000	21.5	0.14	8590		
Ni	5.31	5280	8.9	0.44	1340		
Al	14.06	1940	2.7	0.87	820		

Water cooling of T1

•Rotating Ni disks •Diameter : 48cm, Thickness : 54 mm (9mm-t×6disks) •1 rotation per 0.7s (slow extraction period) : 85 RPM •Partially cooled by water



Gas cooling of T1

\$48cm x 54mm^t **\$48cm x 54mm**^t NODAL SOLUTION NODAL SOLUTION ANSYS 6.0 ANSYS 6.0 JAN 21 2003 JAN 26 2003 STEP=1041 STEP=9999 14:03:16 11:13:30 SUB =1 SUB =1 TIME=1779 TIME=17097 TEMP (AVG) TEMP (AVG) RSYS=0 RSYS=0 SMN =409.186 SMN =39.558 SMX =148.33 SMX =601.585 68.564 97.57 126.576 460.493 563.105 511.799 54.061 83.067 112.073 148.33 601.585 434.839 486.146 537.452 kaiten14-480-8 50Gev-Target(all-Ni) @ 3.0e14ppp @ 100w/m2/K @ 6mm-phi kaiten14-480-2 50Gev-Target(all-Ni) @ 3.0e14ppp @ 10w/m2/K @ 6mm-phi

Natural convection 10 W/m²K assumed ⇒ Highest ~ 602°C: too high Lowest ~ 409°C Forced convection 100 W/m²K assumed ⇒ Highest ~ 148°C: still high Lowest ~ 40°C

R&D for T1

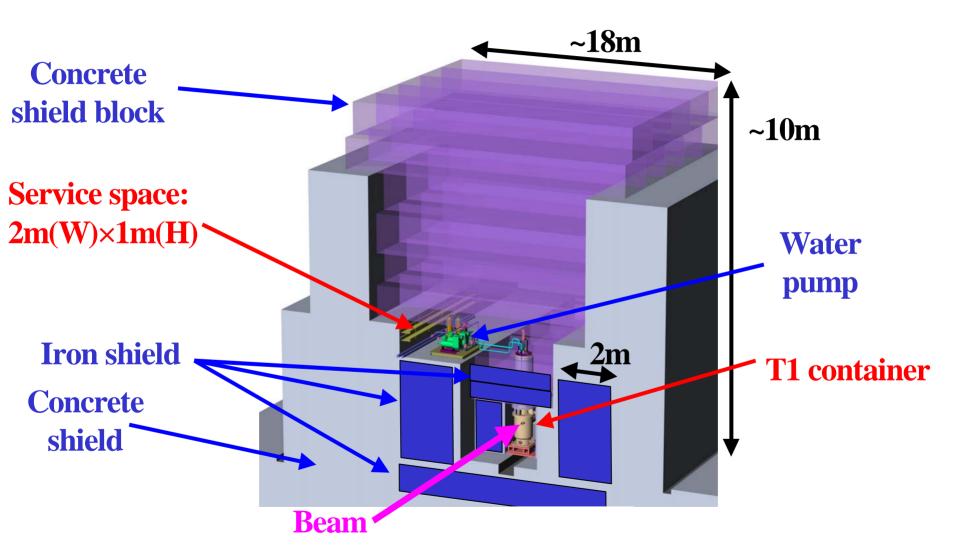
Items

- •Optimization of diameter, thickness, # of disks(gaps)
- •Rotation speed, Method of rotation
- •Durability
- •Container & shielding
- •Cooling system
- •Beam window & vacuum sealing
- •Maintenance method
 - Prototypes
 - Mockup

Nickel disks (\$\$\phi24cm x 6mm^t x 9, 24kg)



Shield around T1

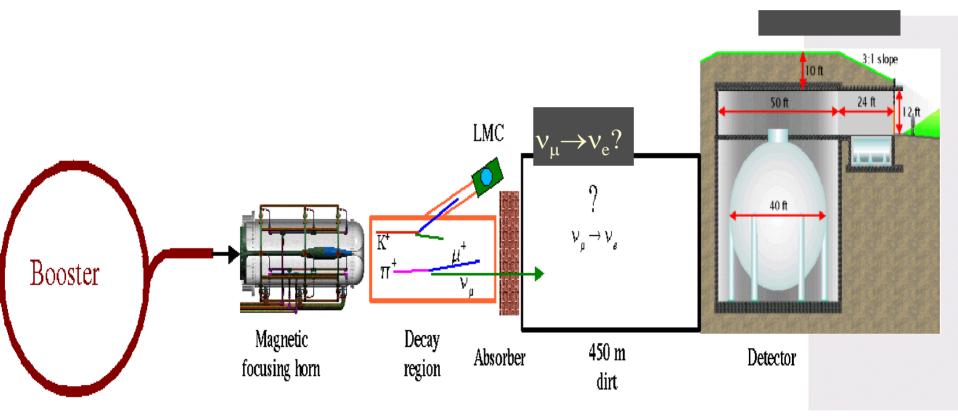


The whole system will be tested by the T1 mockup.

Geoff Mills - The MiniBoone Proton Target (FNAL)

Fully constructed and operational beryllium target for pion production with magnetic horn. Air cooled. Segmented to avoid any possible shock problems. 600 W at 5 Hz. Energy density 35 J cm⁻³.

The MiniBooNE Neutrino Beam

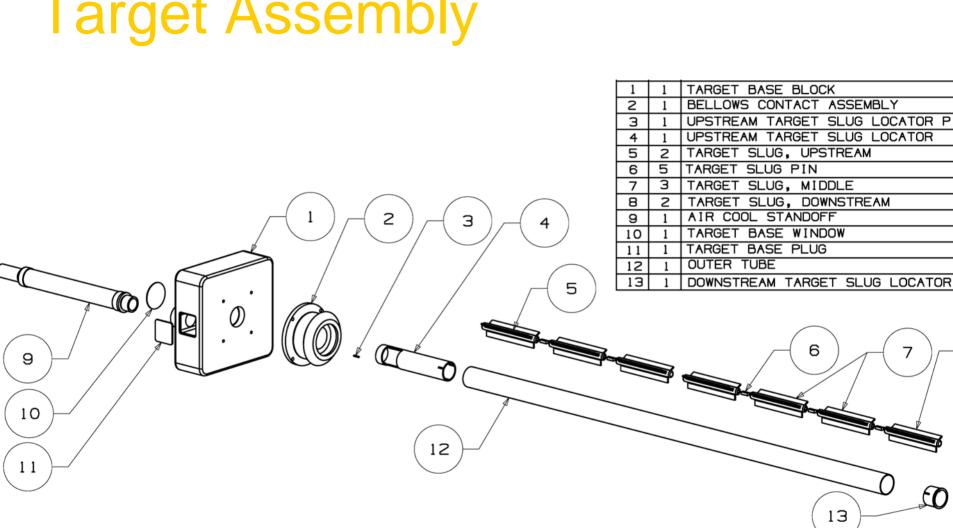


MiniBooNE Target Requirements

- Maximize pion yield
- Long lifetime (~10²² p.o.t.)
- $5x10^{12}$ p.o.t. @ 5 Hz and 8 GeV/c
- Separately removable from horn
- Fit inside 3 cm horn inner conductor
- Low residual activity

Design

- 3/8 inch diameter segmented Be target material
- 1.5mm beam spot sigma
- 1.75 interaction length target material
- Longitudinal air-flow for cooling



Target Assembly

Beryllium Parts



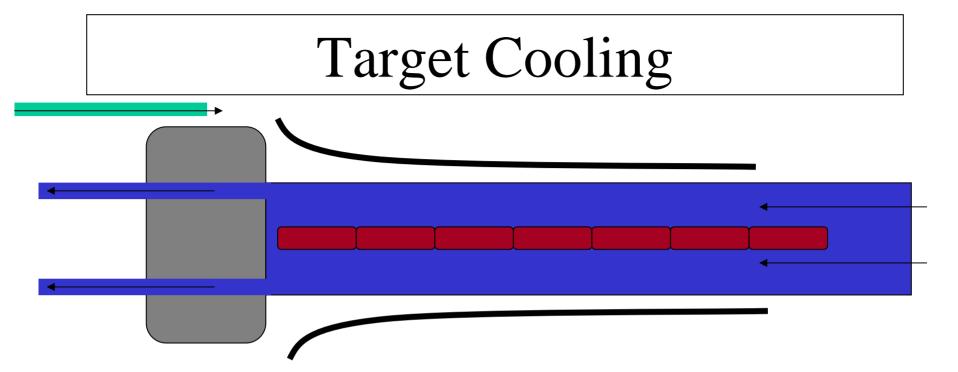






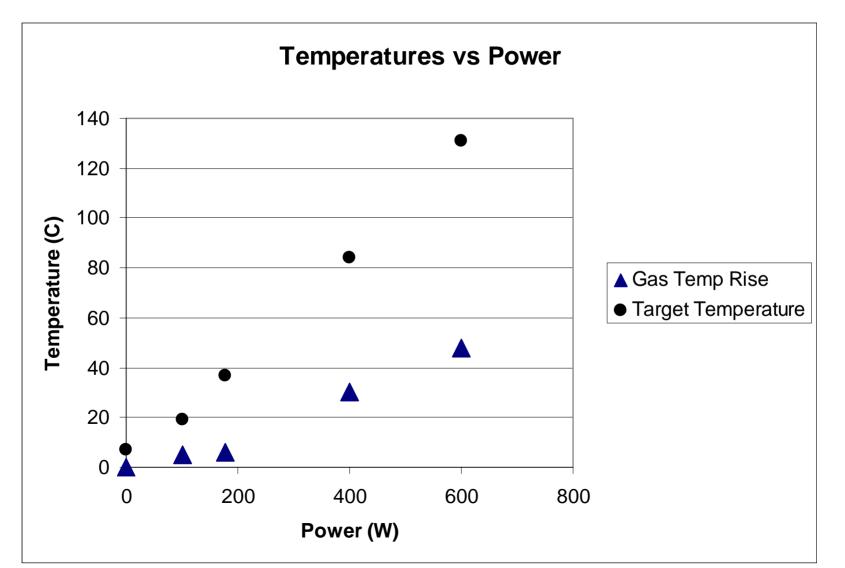
Assembled Target





Beam heating: 610 W Operating temperature ~100 C Air temperature rise ~25 C (depends on flow...)

Measured Temperatures



Summary of Cooling Tests

• Achieved flow rates of > 20 liters/second

• 131 °C target temperature rise @ 600 W

• 55 °C gas temperature rise @ 600 W

Operation

- First beam delivered September 1, 2002
- Typical rates ~4-4.5x10¹²p.o.t. @ ~3 Hz
- > 35 million horn pulses
- > 10^{20} protons on target
- Still going...

Richard Werbeck - Performance of a Clad Tungsten-rod Spallation-Neutron-Source Target -LANCE

Tests on SS clad Tantalum rods

Conclusions

• The success of the irradiation of slip clad tungsten rods as a spallation neutron target is based on the following observations:

– The spallation target performed without incident at a peak power density of 2.25 kW/ cm 3 and a peak heat flux of 148 W/ cm 2 . Peak fluence reached 4 x 10 21 particles/ cm 2 .

– The target design produced very low stress and post irradiation testing showed that the properties of the target materials far exceeded design requirements throughout the irradiation.

- Target geometry is not restricted, especially with further verification that the hydrogen gas created by spallation will not overpressure the volume between the tungsten rod and the clad.

• These observations, coupled with the extensive use of slip clad technology other nuclear applications, demonstrate that future spallation neutron sources should seriously consider using water cooled, slip clad tungsten rod bundles in the target assembly.

Roger Bennett (RAL) Large Solid Targets for a Neutrino Factory

- Table placing existing high power targets in relation to the neutrino factory. Pbar target over 20 times the energy density of neutrino factory target.
- Rotating toroidal target thermal radiation of over 10 MW capability depending on size etc.
- Possible problems with shock or thermal non-uniform heating seen in other solid targets e.g. ISOLDE.
- Could make target from small pieces "shot" through the beam and recirculated.
- Target programme in the UK based on solid targets applying to PPARC funding agency.
- Need a high power target test facility.

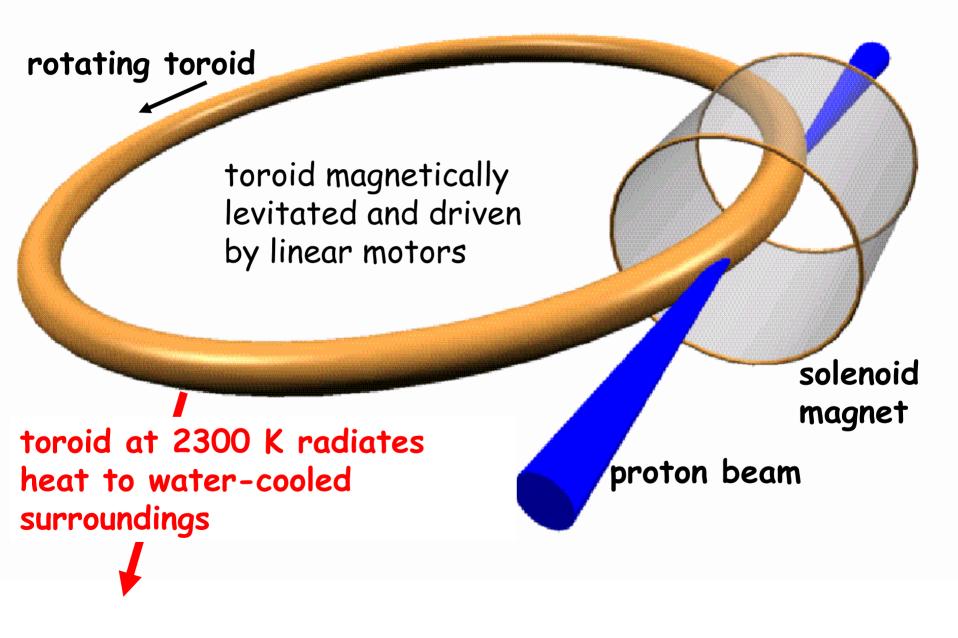
Table comparing some high power pulsed proton targets

Facility	Particle	Rep. I	Power	Energy		Bean	n and	Targe	t size		Energy	Life	Number	
		Rate		/pulse							density		of pulses	
											/pulse		_	
		f	Р	Q	height	width	length	volume	thick	material	q		N	
		Hz	W	J	cm	cm	cm	cm ³	cm		J cm ⁻³	days		
NuFact	protons	50	1E+06	20000	2	2	20	63	20	Та	318	279	1.E+09	
				Number	lumber of pulses on any one se						e section of the toroid			
ISOLDE	protons	1		3675	0.6	1.4	20	13	0.05 to	Та	279	21	2.E+06	
ISIS	protons	50	180000	3600	7	7	30	1155	0.0002 0.7	Та	3	450	2.E+09	
Pbar	protons	0.3		1797	0.19	0.19	7	0.25	~6	Ni	7112	186	5.E+06	
Run I	3E12 pp	p		(Cu, SS, Inconel)								Damage		
Run II	5.E+12			Damage	mage in one or a few pulses 13335									
Future	1.E+13				0.15	0.15					30000			
NuMI	protons	0.53			0.1	0.1	95		2	С	600			
	120 GeV				Radiation Damage - No visible dama						age at 2.3	3E20 p	o/cm ²	
		Shock - no problem up to 0.4 MW (4												
	4E13 pp 8.6 μs				Sublimation -OK									
					Reactor tests show disintegration of graphit								E22 n/cm ²	
					NuMI will receive a max of 5E21 p/cm ² /yea									

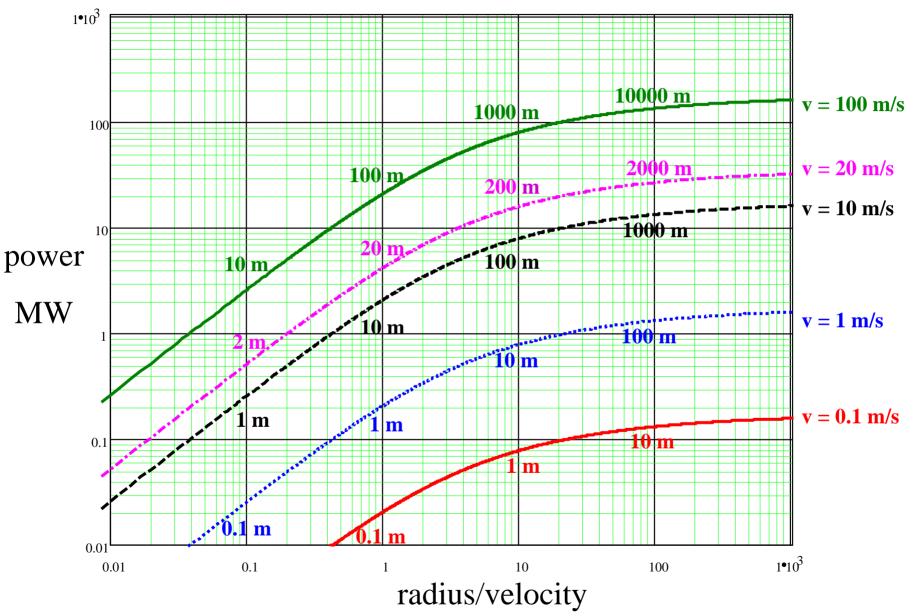
Table comparing some high power pulsed electron targets

Facility	Particle	Rep.	Rep. Power	Energy		Beam and Target siz			t size		Energy	Life	Number
		Rate		/pulse							density		of pulses
				-							/pulse		-
		f	Р	Q	height	width	length	volume	thick	materia	-		N
		Hz	w	J	cm	cm	cm	cm ³	cm		J cm ⁻³	days	
NuFact	nrotons	50	1E+06	20000	2	2	20	63	20	Та	318	279	1.E+09
				Number	_							210	7.E+06
SLC	е	120	5.E+03	42	0.08	0.08			2	W/Re	591	1500	6.E+05
SLAC	33 GeV			Rotating disc, 6.35 cm diameter, 2cm thick 26% Re									
				Target designed to withstand shock									
		Radiat	tion dam	age leadi	ng to l	oss o	f strer	ngth a	nd fail	ure wł	nen subje	ected t	to shock
FXR	е									Та	160		100
LLNL	17 MeV									Та	267		10
											No damage		
RAL/TWI	е	100	4.E+04			0.2			25 μm	Та	500		up to 1E+06
	150 keV					Thin foil 0.4 cm wide Range ~10 μ m							-
					Failures probably due to oxidation in							poor v	acuum

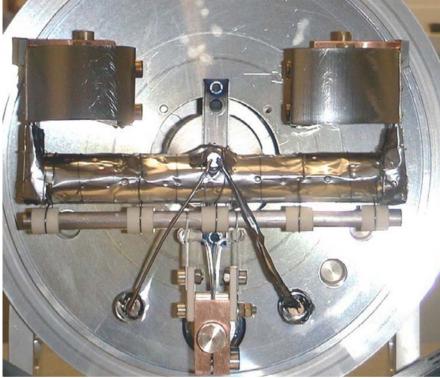
Schematic diagram of the rotating toroidal target



POWER DISSIPATION



ISOLDE converter targets



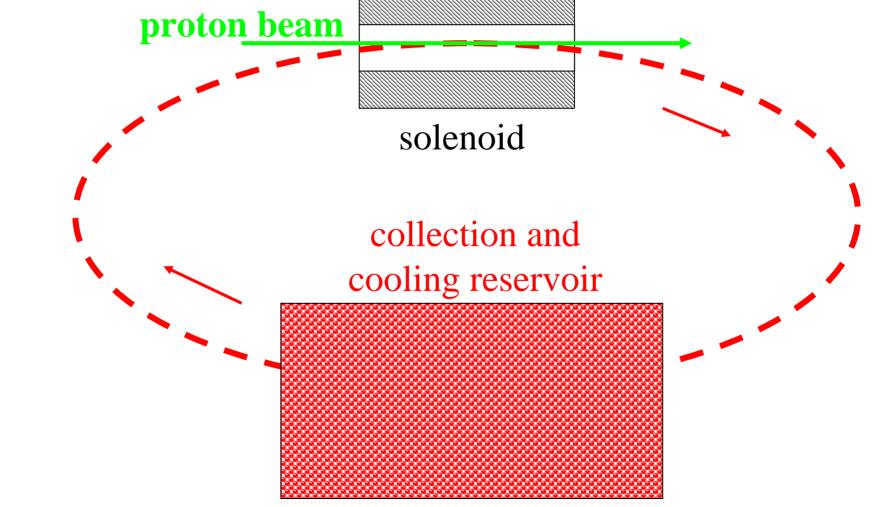
Ta-converter mounted below the UC target before irradiation

Ta-rod after irradiation with 6E18 protons in 2.4 μ s pulses of 3E13



Individual free targets

Levitated target bars are projected through the solenoid and guided to and from the holding reservoir where they are allowed to cool.



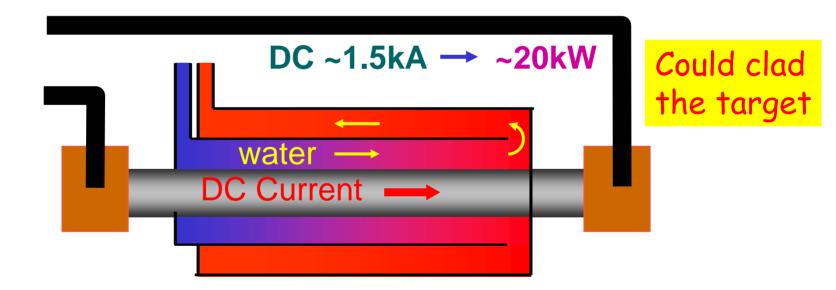
Yoshinari Haito (KEK) The JPARC neutrino Target

Water cooled carbon target, 300 Jcm⁻³. 3 cm diameter 90 cm long. Thermal stress evaluated by ANSYS - OK - but need to use dynamic analysis. Radiation damage lifetime unknown.

Cooling test

According to the results from the calculations, heat transfer rate \rightarrow larger than \sim 6kW/m²/k.

Heat up the target with DC current and try to cool by the flowing water.



measure water flow rate and temperature at various points — estimate the heat transfer rate.

Summary (I) For the JPARC v experiment, solid target R&D is now ongoing. Graphite (or C/C composite ?) material dimensions diameter ~30mm 900mm (2 interaction length) length Water (direct or put in the case?) cooling Heat transfer rate > $\sim 6 kW/m^2/K$ cooling method Direct cooling \longrightarrow seems to work Water flow rate $\sim 20 l/min$. temperature rise ~ 175 °C (center) ~ 25°C (surface) thermal stress ~ 9MPa (for G347) [Tensile strength (G347) ~ 31MPa]

Summary (II)

R&D Items (We want to test/check the following items.)

Cooling test

Set the water flow rate at 20l/min. and confirm the method. Measure the heat transfer rates with a target container.

Stress test

Beam test (with same energy concentration) Where?

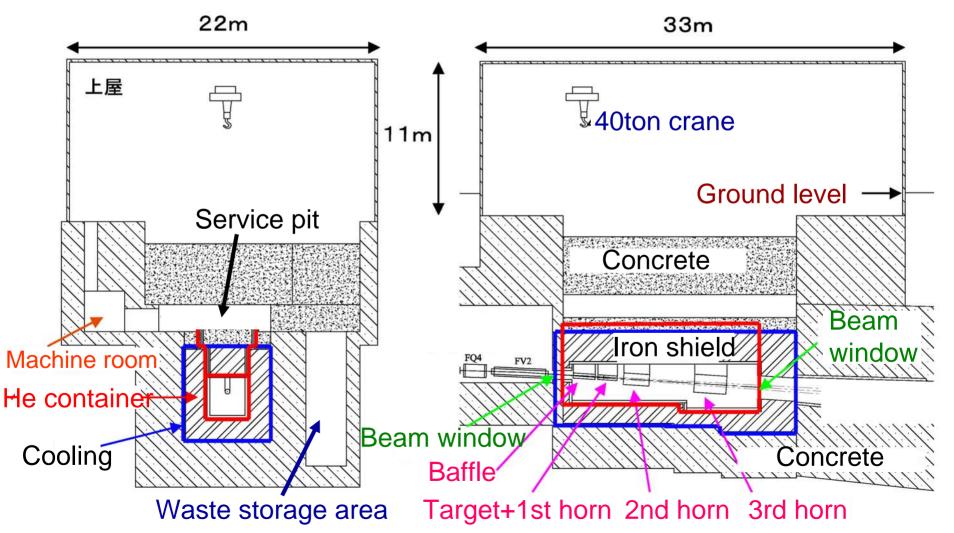
- Irradiation effects other than the thermal conductivity
- Search for the best material (Usually, graphite, whose tensile strength is large, has large Young's modulus.
 - \rightarrow the thermal stress is also getting larger.)

Temperature dependences of the material properties.

Summary (III)

• Design of the entire system has to be fixed.

How to fix (support) the target, alignments etc...



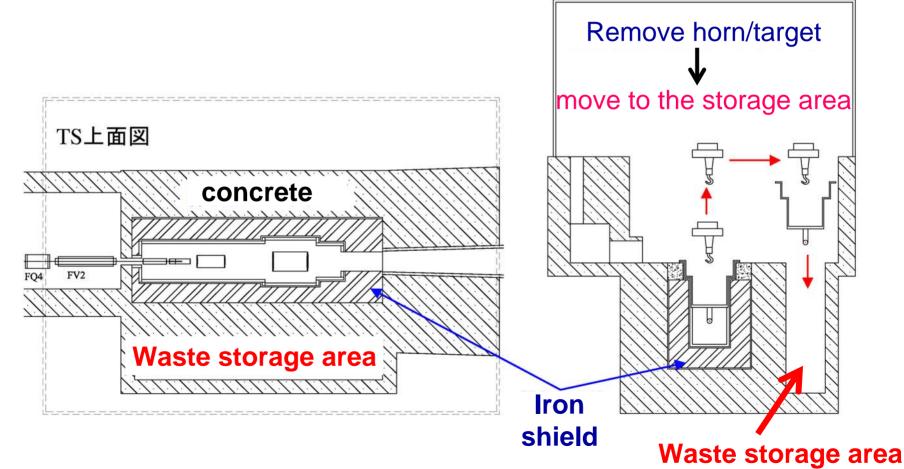
Summary (IV)

• Target handling

How to remove the target from the horn remotely?

(It may be necessary to remove the target from the horn

when the target part is broken.)

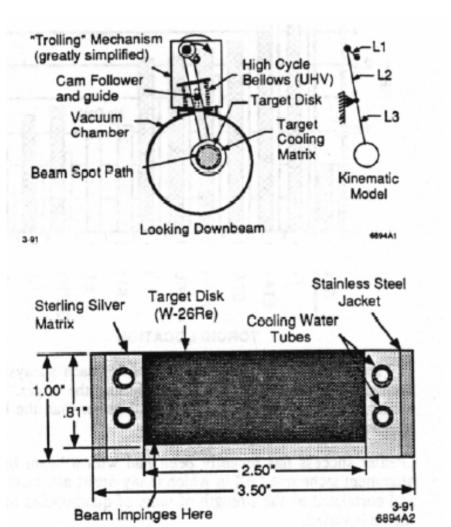


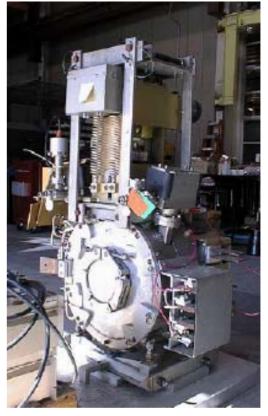
- Nikoli Mokhov (FNAL) NuMI Target (Jim Hylen & Jim Morgan)
- Water-cooled graphite, segmented. Energy density 640 Jcm⁻³. Shock limit in graphite ~ 2000 Jcm⁻³. Radiation damage lifetime unknown. Proton beam.

- Vinod Bharadwaj (SLAC) NLC Positron Production Target
- Tungsten/25Re rotating target disc, water-cooled.
- Energy density 600 Jcm⁻³. Electron beam.
- Damage caused failure after 5 years. Damage thought to be due to radiation deterioration of strength and pulse stress failure.
- HIGHLY SUCCESSFUL TARGET!!

NLC target - to have multiple targets to reduce stress in target to acceptable level.

SLC Positron Target





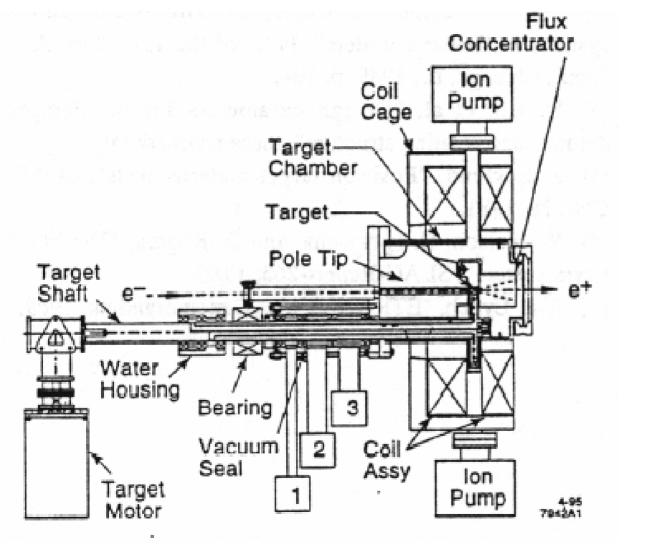
The NLC target design uses the operational experience gained from the SLC.

SLC positron target made of 6 r.l. W-Re. "Trolling target". Was made so that average heating would not damage the target

SLC drive beam is 30 GeV, 4 x 10¹⁰ e⁻/bunch, 1 bunch/pulse, 120 pulses/sec, 24 kW

NLC Positron Target

NLC positron target design – extrapolated from the SLC positron target



NLC spinning target design. 20 cm. dia. W Re target ring. 23 kW deposited

Oscillating at 1/2 Hz.

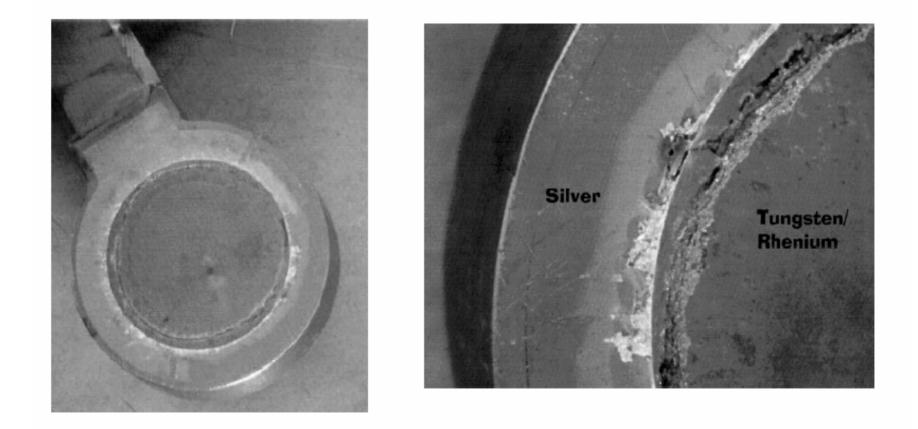
Beam rate is 120 Hz.

Spinning shaft with water and vacuum seals.

Extrapolation to NLC Drive Beam Power

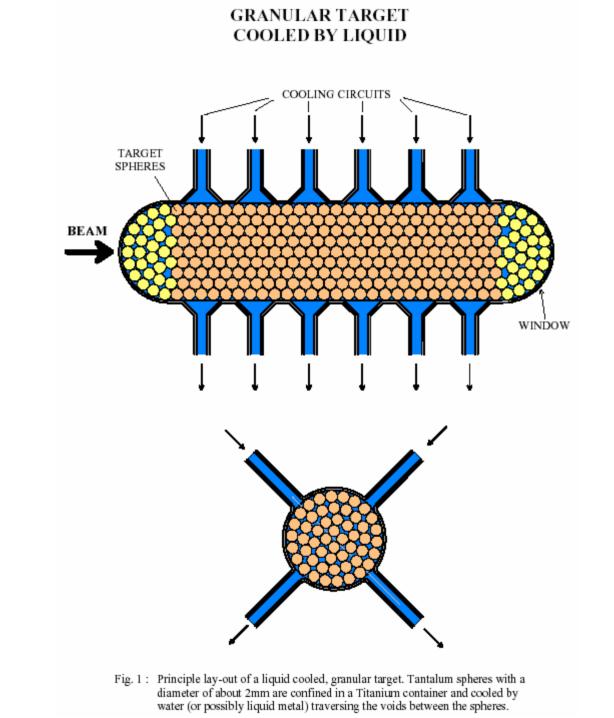
- NLC target made bigger to allow for greater average beam power (340 kW as compared with 24 kW)
- The energy deposition for a single pulse in the NLC target is calculated to be below the level that will damage the target material.
- The SLC was thought to be a factor of two below damage threshold
- BUT
 - The SLC positron target failed (after 5 years of operation)
 - Failure lead to a detailed analysis of materials properties: radiation damage, shock and stress, fatigue, etc.

SLAC Target Damage



SLC target damage studies were done at LANL. Results show evidence of cracks, spalling of target material and ageing effects.

- *Peter Sievers* (CERN) Moving and Stationary High-Power Targets for Neutrino Factories.
- Multiple (4) granular targets (Ta, WC, Pt) to alleviate thermal shock (4MW proton beam). Cooled by helium gas. Can be used with horns and the beams combined.



Nick Simos (BNL) Simulations of Proton Beam Induced Pressure Waves

Modelling of shock in solid targets (graphite) and windows. On the whole fairly good agreement. Vital work must be continued to reduce the need for expensive in-beam tests.

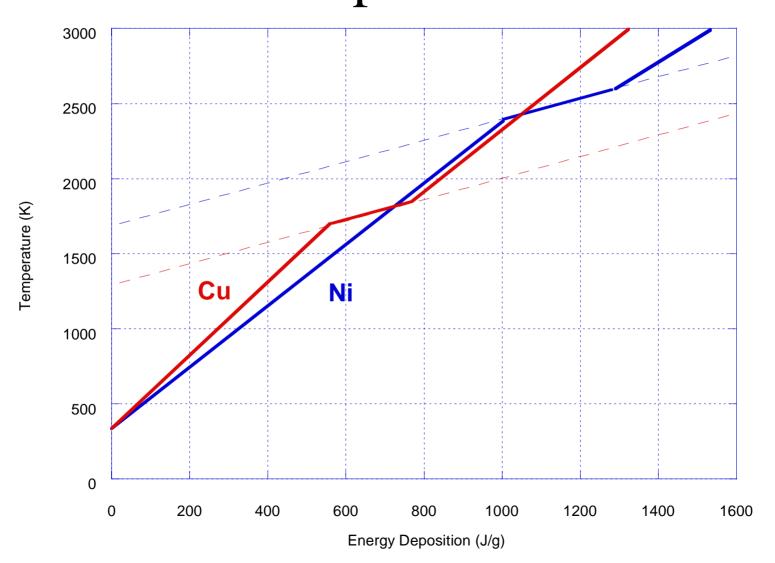
Long term (many pulses) failure may not be easy to predict.

- Jim Morgan (FNAL) Pbar Target
- Very high energy density dissipation 2000 Jcm⁻³.
- Targets melt on beam centre!
- But the system works!
- Some damage seen. Is it melting or shock or a combination of both?

Target material comparison

Target Material	Iridium	Rhenium	Tungsten	Nickel	Copper
$A^{1/3}/\rho (m^3/Kg)$.255	.271	.295	.437	.445
$A^{1/3}/\rho$ (Normalized)	1.71	1.61	1.48	1	.98
Observed Yield (Normalized)			1.05	1	.99
Melting Point Energy (J/g)	460	610	630	1,250	770
Yield Strength (kPa)	160	270	500	230	72
Gruneisen parameter (kPa Kg/J)	80.6	66.0	31.0	15.8	17.2

Energy deposition vs. peak target temperature



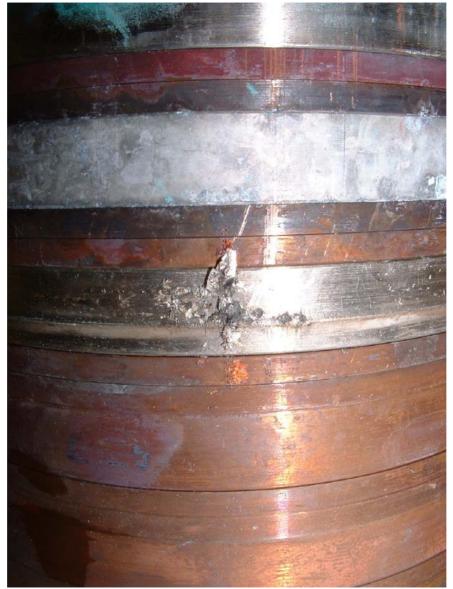
Damage to Tungsten-Rhenium target



Damage to Tungsten target



Target damage to nickel target (entry)



Helge Ravn (CERN) Eurisol and Beta Beam Target Issues.

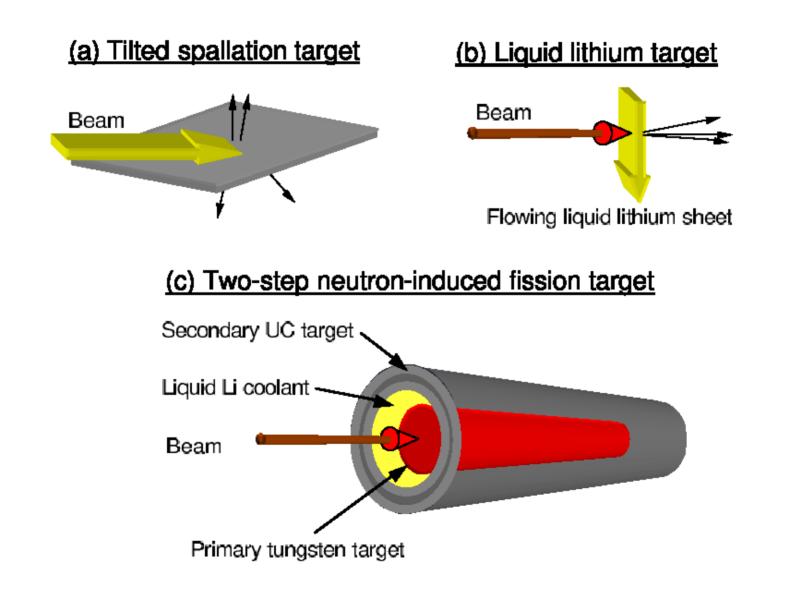
Solid targets for ISOL targets up to ~100 kW (250 kWcm⁻³). Radiation cooled. (I believe 500 kW max is possible.)

Experience with tantalum converter target test - not good experience!!

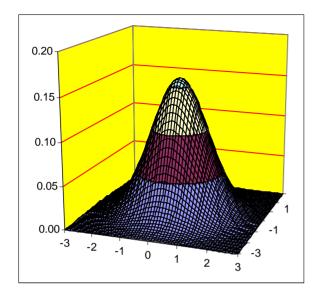
Kirk McDonald (Princeton) Neutrino Factory Targetry Concept Summary of solid targets for neutrino factories.

Jerry Nolan (ANL) High Power Targets for RIA A variety of Targets for radioactive beams - some solid.

A Variety of Targets and Production Mechanisms



- *Harold Kirk and Peter Thieberger* (BNL) Moving Solid Targets in a Multi-Megawat Beam Environment
- Benefit of flat beam profile over a Gaussian to reduce the peak energy density.
- Metal chain link moving target design.
- Selection of target material for low thermal expansion to reduce shock stress. Super Invar excellent - BUT radiation damage! Thus Super Invar no good.
- Vascomax very strong but magnetic.
- Inconel 718 is a good choice.



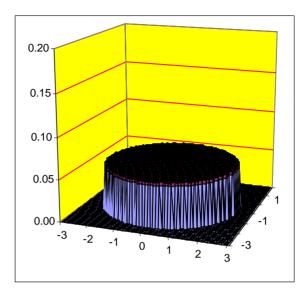


Fig 12a

Fig. 12b

Comparison of a doubly Gaussian beam profile (a) with an ideal flat profile (b) containing the same number of particles.

A perfectly flat beam such as shown in Fig. 12b can of course not be realized, but using octupole lenses one can generate profiles which are fairly close to this goal. Fig 13 shows one of the projections of such a distribution which was calculated¹¹⁾ for larger "uniform" beams required for the irradiation of biological materials.

