

# Acceleration Costs

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# Acceptances

|                              | Trans<br>$\pi$ mm   | Long<br>$\pi$ mm |
|------------------------------|---------------------|------------------|
| After Target                 | $.22/.105*0.08=170$ | -                |
| After Study-2 Phase Rotation | 100                 | 200              |
| After Study 2 Cooling        | 15                  | 150 <sup>1</sup> |
| After RFOFO Cooling Ring     | 15                  | 35               |
| After Low Beta Ring          | 4 <sup>2</sup>      | 35               |

1. Reduced by scraping
2. Achieved, but with poor transmission

# Possible New Acceleration Schemes

## Pulsed Synchrotron

1. Linac: .2 to 1 GeV/c
2. RLA : 1 to 4 GeV/c
3. Pulsed Synchrotron: 4 to 20 GeV/c

## FFAG

1. Linac: .2 to .6 GeV/c
2. FFAG : .6 to 2 GeV/c
3. FFAG : 2 to 6 GeV/c
4. FFAG: 6 to 20 GeV/c

# COSTS

## SC Cavities

| SC                 | cost<br>M\$/GeV                 |
|--------------------|---------------------------------|
| (Study-2) Cavities | $63.36/4.375=14.5 \times 16/G$  |
| Power              | $89.16/4.375= 20.4 \times g/16$ |
| Cryo               | $28/4.375=6.4 \times g/16$      |
| Total at 16 GV/m   | <b>41.3</b>                     |

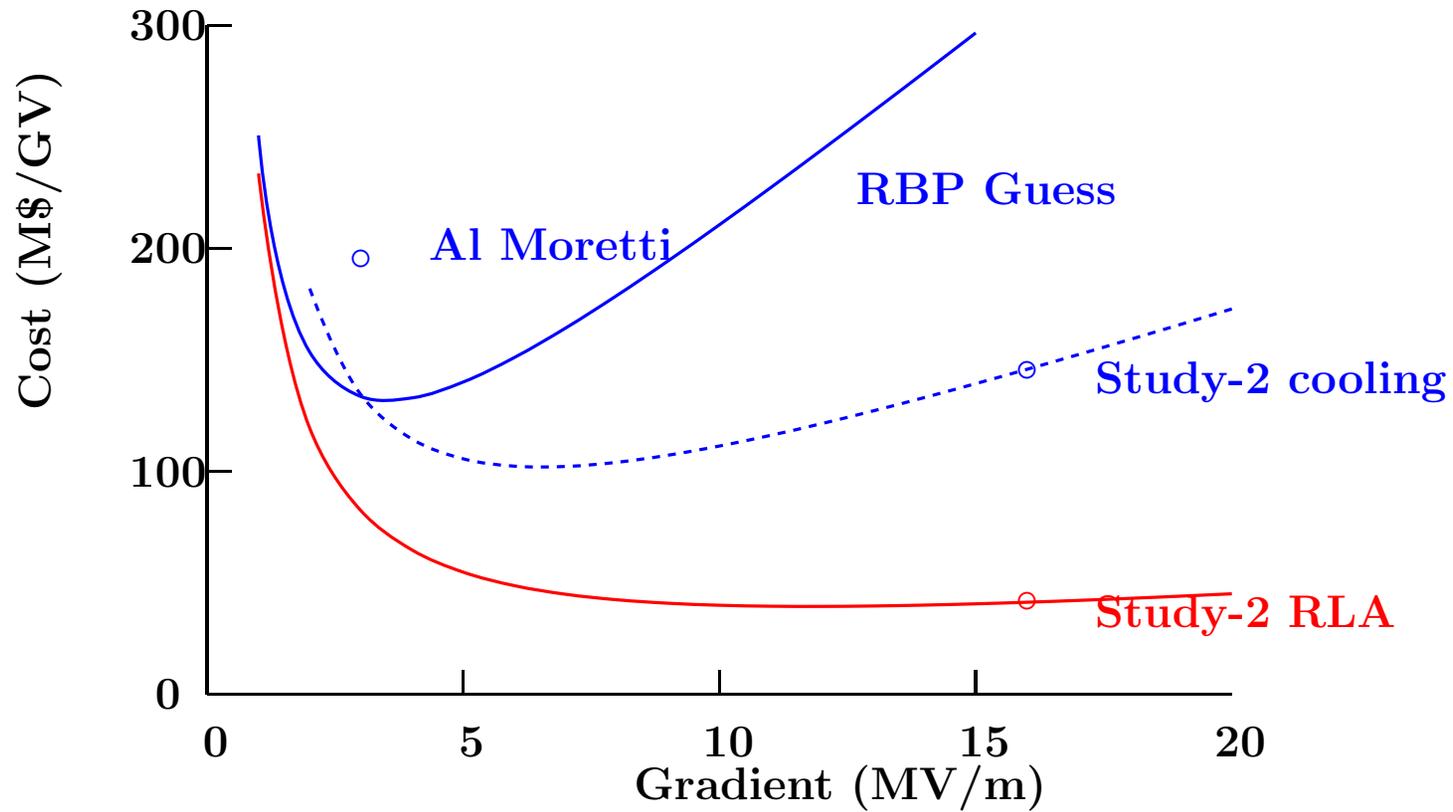
Note: TESLA Cavities + RF

$$\frac{\text{Cost}}{\text{GeV}} \approx \frac{2 \text{ B\$}}{500 \text{ GeV}} = 4 \text{ M\$/GeV}$$

# Cu Cavities

| Cu                   |                   | cost<br>M\$/GeV            |
|----------------------|-------------------|----------------------------|
| (study-2)<br>+ foils | Cavities          | $125/6=20.8 \times 16/G$   |
|                      | Power             | $750/6=125 \times G/16$    |
|                      | Total at 16 MV/m  | <b>146</b>                 |
|                      | Total at 6.5 MV/m | <b>103</b>                 |
| Open                 | Cavities          | $\approx 14.5 \times 16/G$ |
|                      | Power             | $\approx 250 \times G/16$  |
|                      | Total at 16 MV/m  | <b>314</b>                 |
|                      | Total at 3 MV/m   | <b>158</b>                 |
|                      | Total at 3 MV/m   | <b>133 (AM 195)</b>        |

- Foil cavities have  $\approx 2 \times$  better Shunt Impedance



If  $\mathcal{E}(\text{Cu}) = \frac{V/\text{turn}}{\Sigma \text{ gaps}} < 3 \text{ (MV/m)}$  Then fill a fraction to keep  $\mathcal{E}(\text{Cu}) = 3$

If  $\mathcal{E}(\text{SC}) = \frac{V/\text{turn}}{\Sigma \text{ gaps}} < 6 \text{ (MV/m)}$  Then fill a fraction to keep  $\mathcal{E}(\text{SC}) = 6$

# SC Magnets

$$\text{EST}_2(\text{RBP}) \text{ (k\$)} = 27.5 B^{1.3} R' (L + 20 R')$$

where  $R' = R + 0.003 B$

$B$  in T,  $R$  &  $L$  in m.

|        | L<br>m | R<br>m | B<br>T | G<br>T/m | cost<br>k\$ | cost/Est |
|--------|--------|--------|--------|----------|-------------|----------|
| RHIC Q | 1.1    | 0.04   | 5.3    | 91.0     | 29 *        | 0.95     |
| LHC    | 30.0   | 0.03   | 8.3    | 0.0      | 708         | 0.95     |
| RHIC   | 10.0   | 0.04   | 5.3    | 0.0      | 149 *       | 0.93     |
| Erich  | 18.0   | 0.02   | 5.6    | 0.0      | 178         | 1.03     |

\* Costs corrected for inflation of 2.5% for 11 years = 1.31

For Field Quality:

$$\text{Use } R = \frac{(\text{Max beam width})}{2} \times 1.3$$

## Cu Dipole Magnets

Rees 1.93\$/J

| Main Ring | B   | L | W    | H   | U  | cost | cost1 |
|-----------|-----|---|------|-----|----|------|-------|
|           | T   | m | m    | m   | kJ | k\$  | k\$   |
|           | 1.7 | 6 | .115 | .05 | 40 | 100  | 77    |

## Cu Quadrupole Magnets

Rees 5.45\$/J

| Main Ring | G    | L    | R    | Bmax | U    | cost | cost1 |
|-----------|------|------|------|------|------|------|-------|
|           | T/m  | m    | m    | T    | kJ   | k\$  | k\$   |
|           | 20.2 | 2.95 | .042 | 0.84 | 2.29 | 30   | 12.5  |

## Linear Costs

|             | source  | cost | L     | Cost/length |
|-------------|---------|------|-------|-------------|
|             |         | M\$  | km    | K\$/m       |
| Vacuum      | Study-2 | 15   | 3.26  | 4.6         |
| Diagnostics | "       | 4    | 3.26  | 1.2         |
| Civil       | "       | 19   | 1.446 | 13.1        |
| Total       |         |      |       | 18.9        |

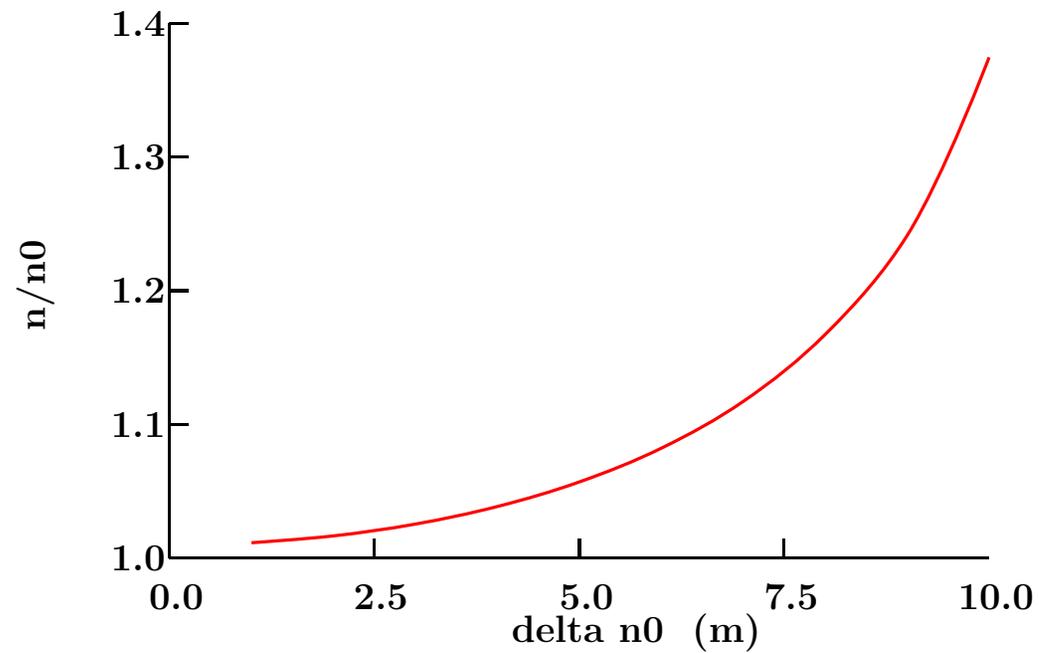
# Phase Slip

Find initial phase for minimum req turns

Plot  $\frac{\text{Req. Turns}}{\text{Circ/Volts}}$  vs  $\frac{\Delta E}{\text{Volts/turn}} \times \text{Circ.}$

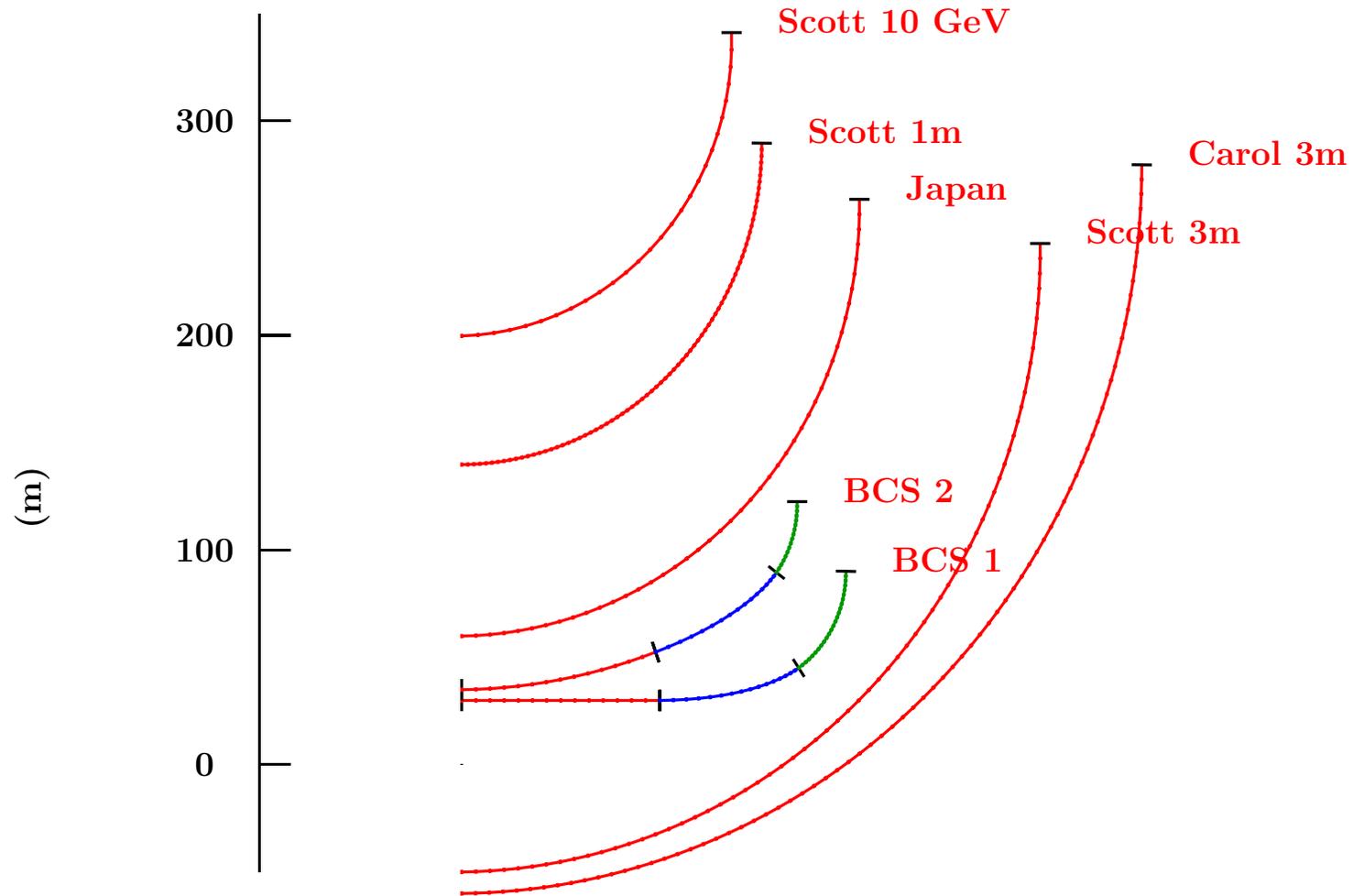
Typical

Req Turns/ ideal



# Lattices

1. Japan: Scaling FFAG for 10-20 GeV
2. Scott 10: Carol type n on-scaling FFAG for 10-20 GeV, with 3 m gaps for SC RF
3. Carol: Original Carol non-scaling FFAG for 6-20 GeV and 3 m gaps for SC RF
4. Scott 3: Modified Carol non-scaling FFAG for 6-20 GeV and 3 m gaps for SC RF
5. Scott 1: Modified Carol non-scaling FFAG for 6-20 GeV and 1 m gaps for normal RF
6. BCS 1: Bob, Carol, Scott non-scaling FFAG with adiabatic matching from arc to straight Linacs
7. BCS 2: Bob, Carol, Scott non-scaling FFAG with adiabatic matching from arc to curved Linacs



# Magnets

|                     | n   | cell<br>m | L<br>m | R<br>m | Bmin<br>T | Bmax<br>T | G<br>T/m | /mag<br>k\$ | Tot<br>M\$ | delta<br>m | circ<br>km |
|---------------------|-----|-----------|--------|--------|-----------|-----------|----------|-------------|------------|------------|------------|
| <b>Japan</b>        | 180 | 6.99      | 1.53   | 0.156  | 2.5       | 6.4       | 9.4      | 237.9       |            |            |            |
| 10 20               | 180 | 6.99      | 1.96   | 0.156  | 2.5       | 6.4       | 9.4      | 256.2       | 88.9       | 1.29       | 1257       |
| <b>Scott 10 GeV</b> | 108 | 8.00      | 1.00   | 0.157  | -2.1      | 4.3       | 15.3     | 137.7       |            |            |            |
| 10 20               | 108 | 8.00      | 1.00   | 0.065  | 2.5       | 5.2       | 15.0     | 40.8        | 19.3       | 0.39       | 864        |
| <b>Carol 3m</b>     | 314 | 6.80      | 0.45   | 0.169  | -4.5      | 6.5       | 24.2     | 279.8       |            |            |            |
| 6 20                | 314 | 6.80      | 0.35   | 0.086  | -2.8      | 4.6       | 31.8     | 47.9        | 102.9      | 0.61       | 2135       |
| <b>Scott 3m</b>     | 260 | 7.00      | 0.50   | 0.194  | -5.0      | 5.5       | 20.3     | 344.2       |            |            |            |
| 6 20                | 260 | 7.00      | 0.50   | 0.111  | -2.4      | 3.6       | 20.4     | 59.4        | 104.9      | 0.87       | 1820       |
| <b>Scott 1m</b>     | 314 | 3.00      | 0.50   | 0.093  | -5.7      | 7.3       | 51.4     | 122.3       |            |            |            |
| 6 20                | 314 | 3.00      | 0.50   | 0.051  | -2.9      | 4.3       | 51.5     | 19.8        | 44.6       | 0.31       | 942        |
| <b>BCS 1</b>        | 56  | 7.00      | 0.50   | 0.194  | -5.0      | 5.5       | 20.3     | 344.2       |            |            |            |
| str                 | 56  | 7.00      | 0.50   | 0.111  | -2.4      | 3.6       | 20.4     | 59.4        |            |            |            |
|                     | 64  | 4.60      | 0.95   | 0.139  | -3.7      | 6.0       | 26.2     | 191.3       |            |            |            |
| match               | 64  | 4.60      | 0.65   | 0.079  | -1.8      | 5.6       | 34.2     | 48.5        |            |            |            |
|                     | 96  | 2.20      | 1.40   | 0.084  | -0.5      | 7.3       | 33.6     | 84.2        |            |            |            |
| arc 6 20            | 96  | 2.20      | 0.80   | 0.047  | -1.3      | 7.9       | 66.5     | 34.2        | 49.3       | 0.27       | 730        |
| <b>BCS 2</b>        | 56  | 7.00      | 0.50   | 0.194  | -5.0      | 5.5       | 20.3     | 344.2       |            |            |            |
| str                 | 56  | 7.00      | 0.50   | 0.111  | -2.4      | 3.6       | 20.4     | 59.4        |            |            |            |
|                     | 64  | 4.60      | 0.95   | 0.139  | -3.7      | 6.0       | 26.2     | 191.3       |            |            |            |
| match               | 64  | 4.60      | 0.65   | 0.079  | -1.8      | 5.6       | 34.2     | 48.5        |            |            |            |
|                     | 64  | 2.20      | 1.40   | 0.084  | -0.5      | 7.3       | 33.6     | 84.2        |            |            |            |
| arc 6 20            | 64  | 2.20      | 0.80   | 0.047  | -1.3      | 7.9       | 66.5     | 34.2        | 45.5       | 0.20       | 712        |

# RF and Costs

Ave Gradient = 1 (MV/m)

gives loss of 17.5% from 6 to 20 GeV with frequency modulation

But not being on crest increases losses

|                  | turns | n/n0 | loss<br>% | slip<br>m | V<br>GV | gaps | gap<br>m | SC G<br>MV/m | fill | SC \$<br>M\$ | RF G<br>MV/m | RF \$<br>M\$ | lin \$<br>M\$ | Tot \$<br>M\$ |
|------------------|-------|------|-----------|-----------|---------|------|----------|--------------|------|--------------|--------------|--------------|---------------|---------------|
| <b>10-20 GeV</b> |       |      |           |           |         |      |          |              |      |              |              |              |               |               |
| <b>Japan</b>     | 14    | 1.27 | 13.1      | 1.3       | 1.26    | 360  | 1.75     | 999.0        | 1.00 | 999          | 1.99         | 185          | 25            | 299           |
| <b>Scott</b>     | 17    | 1.08 | 11.3      | 0.4       | 0.86    | 108  | 3.00     | 8.0          | 0.89 | 37           | 3.00         | 107          | 17            | 73            |
| <b>6-20 GeV</b>  |       |      |           |           |         |      |          |              |      |              |              |              |               |               |
| <b>Carol 3m</b>  | 7     | 1.04 | 18.1      | 0.6       | 2.14    | 628  | 3.00     | 6.0          | 0.38 | 104          | 3.00         | 265          | 43            | 250           |
| <b>Scott 3m</b>  | 8     | 1.10 | 19.1      | 0.9       | 1.82    | 520  | 3.00     | 6.0          | 0.39 | 89           | 3.00         | 226          | 36            | 230           |
| <b>Scott 1m</b>  | 16    | 1.05 | 18.3      | 0.3       | 0.94    | 628  | 1.00     | 999.0        | 0.50 | 999          | 3.00         | 117          | 19            | 180           |
| <b>BCS 1</b>     | 20    | 1.06 | 18.5      | 0.3       | 0.73    | 112  | 3.00     | 6.5          | 0.72 | 34           | 3.00         | 91           | 15            | 98            |
| <b>BCS 2</b>     | 20    | 1.04 | 18.1      | 0.2       | 0.71    | 112  | 3.00     | 6.4          | 0.71 | 34           | 3.00         | 88           | 14            | 93            |

\* Frequency modulation required at 200 MHz

† Insufficient space for SC Cavity with field standoff

# Conclusion

- For the same energy increase of 10-20 GeV, The Carol type non scaling FFAG appears significantly cheaper than a scaling design. Its circumference is less, its magnets have smaller apertures and fields, it is sufficiently isochronous as to allow fixed frequency RF and has gaps large probably enough to use Superconducting RF (the required stand off needs study).
- Quoted costs do not include injection, extraction and transfer lines. When these are included, there is likely to be a significant advantage in using fewer rings with more energy increases in each ring. Studies were made for 6-20 GeV. It is found that the cost of a Carol type lattice for this larger energy swing is much higher, because of the larger apertures of the magnets.
- The magnet apertures and costs are less if the lattice is shortened leaving only 1 m gaps for RF and thus requiring the use of conventional RF. The cost is less in this case, despite a substantial increase in RF power cost.
- An better solution (BCS), if it can be designed, is to have a short cell lattice for the arcs and a long cell lattice with 3 m gaps for SC RF, and an adiabatic match between them. Such a match has yet to be successfully designed.
- **WARNING This analysis has not been very carefully checked, and may contain errors**