

Open Cavity rf Experiment



Questions

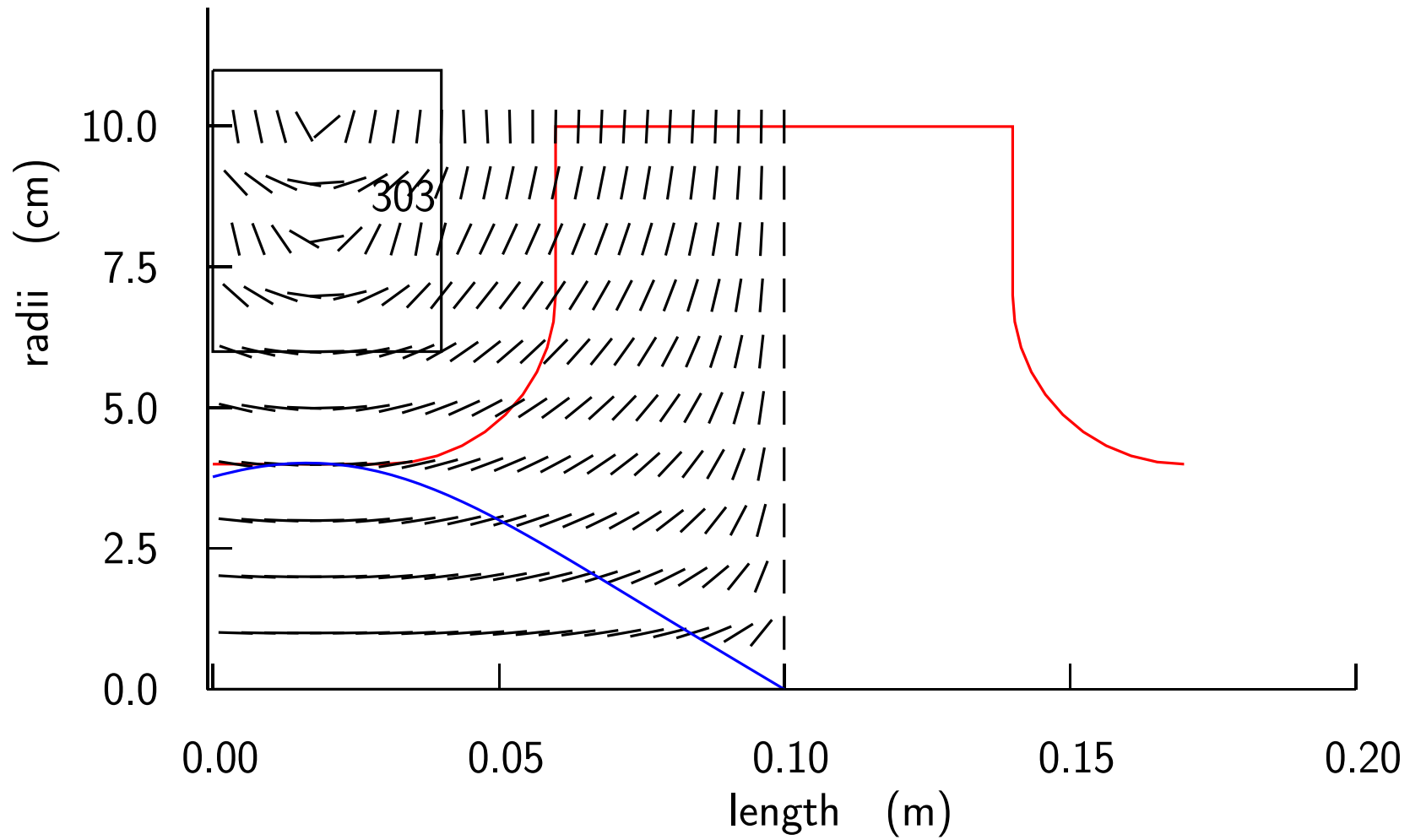
- Joints in exp 4
- tuner
- cooling in Nb₃Sn case
- do we need a cold box?
- minimum gap for super insulation
- winding with ss strips together with sc

R. B. Palmer (BNL)

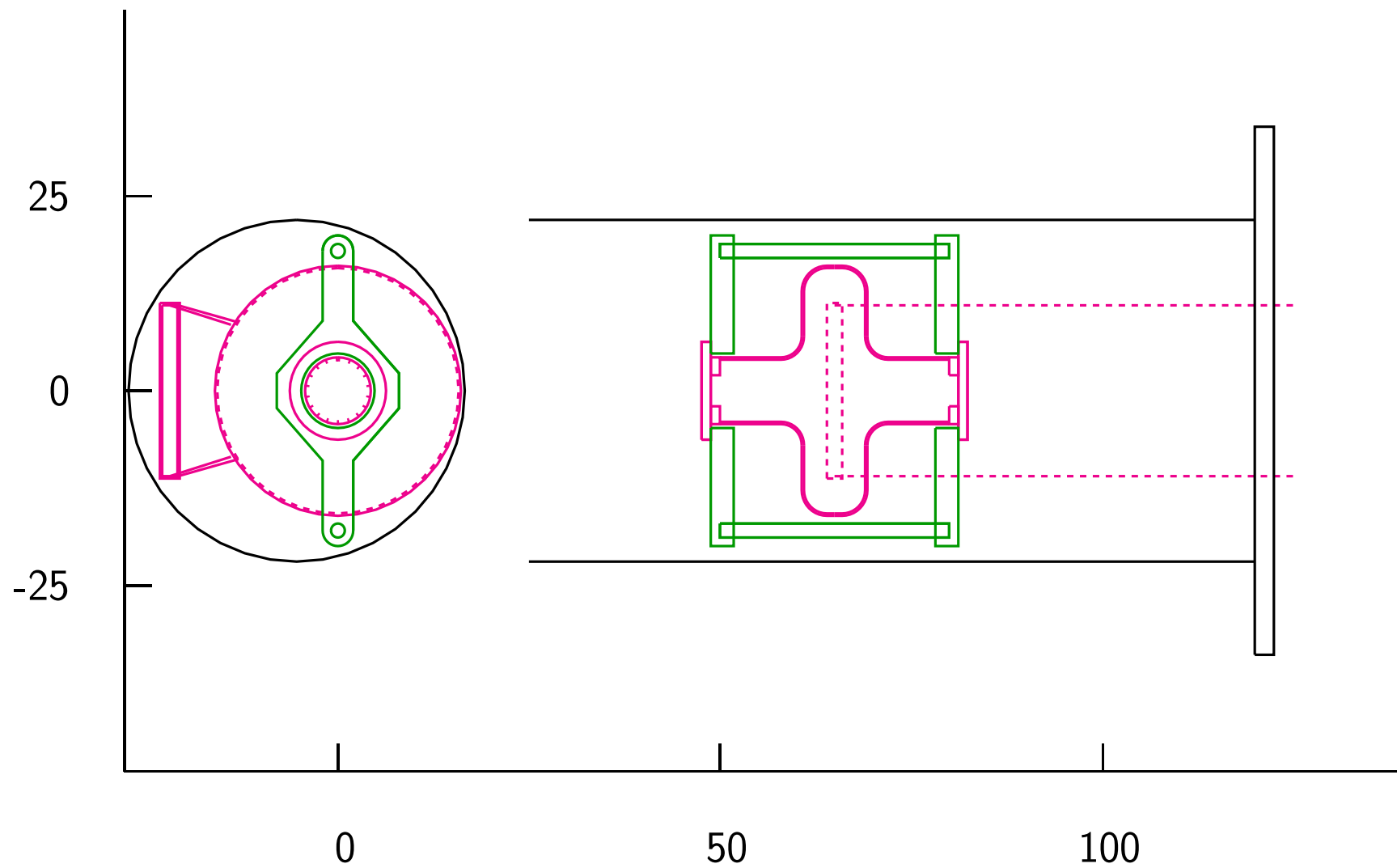
LBNL

Jan 21

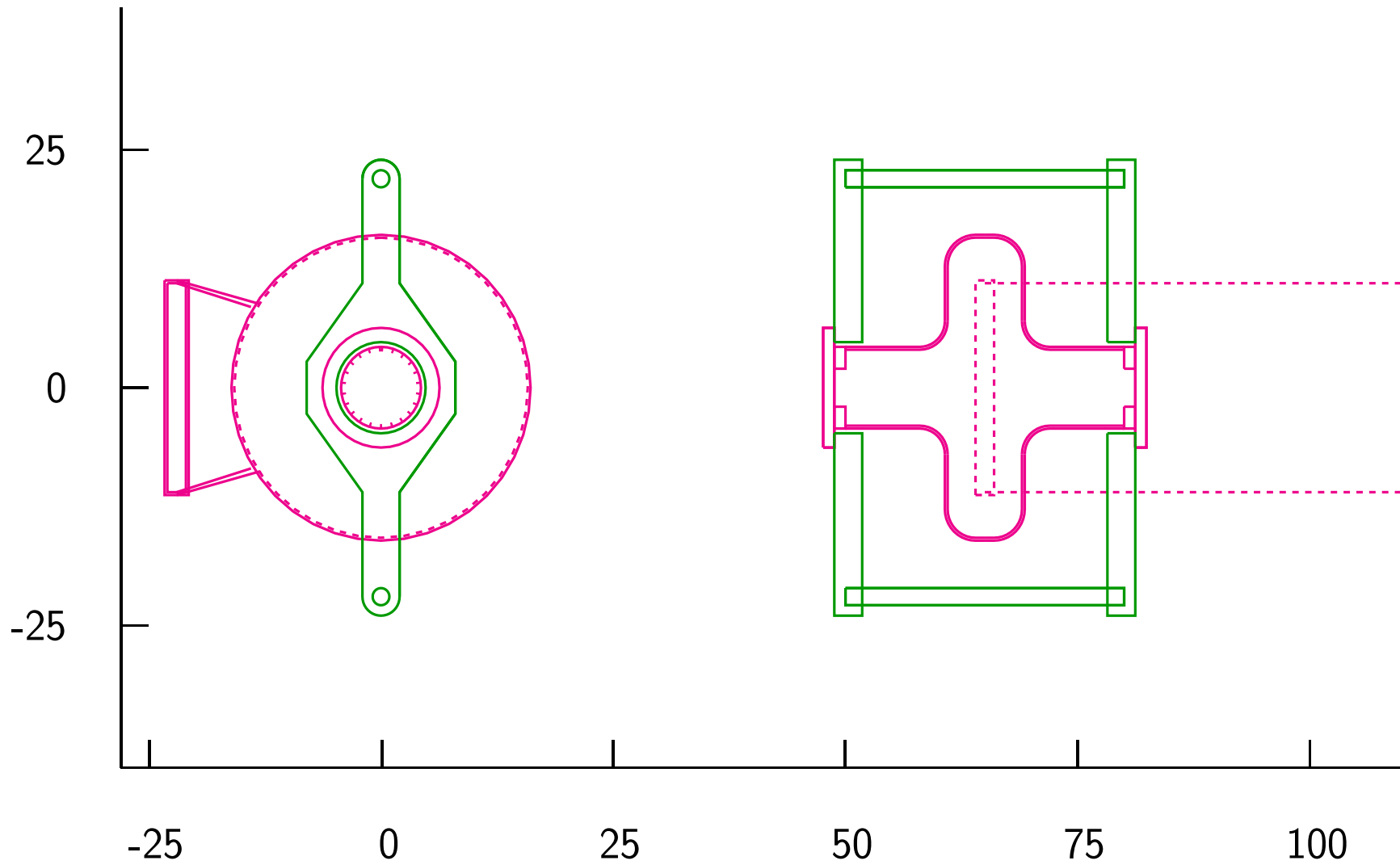
Experiment #1 Single cavity



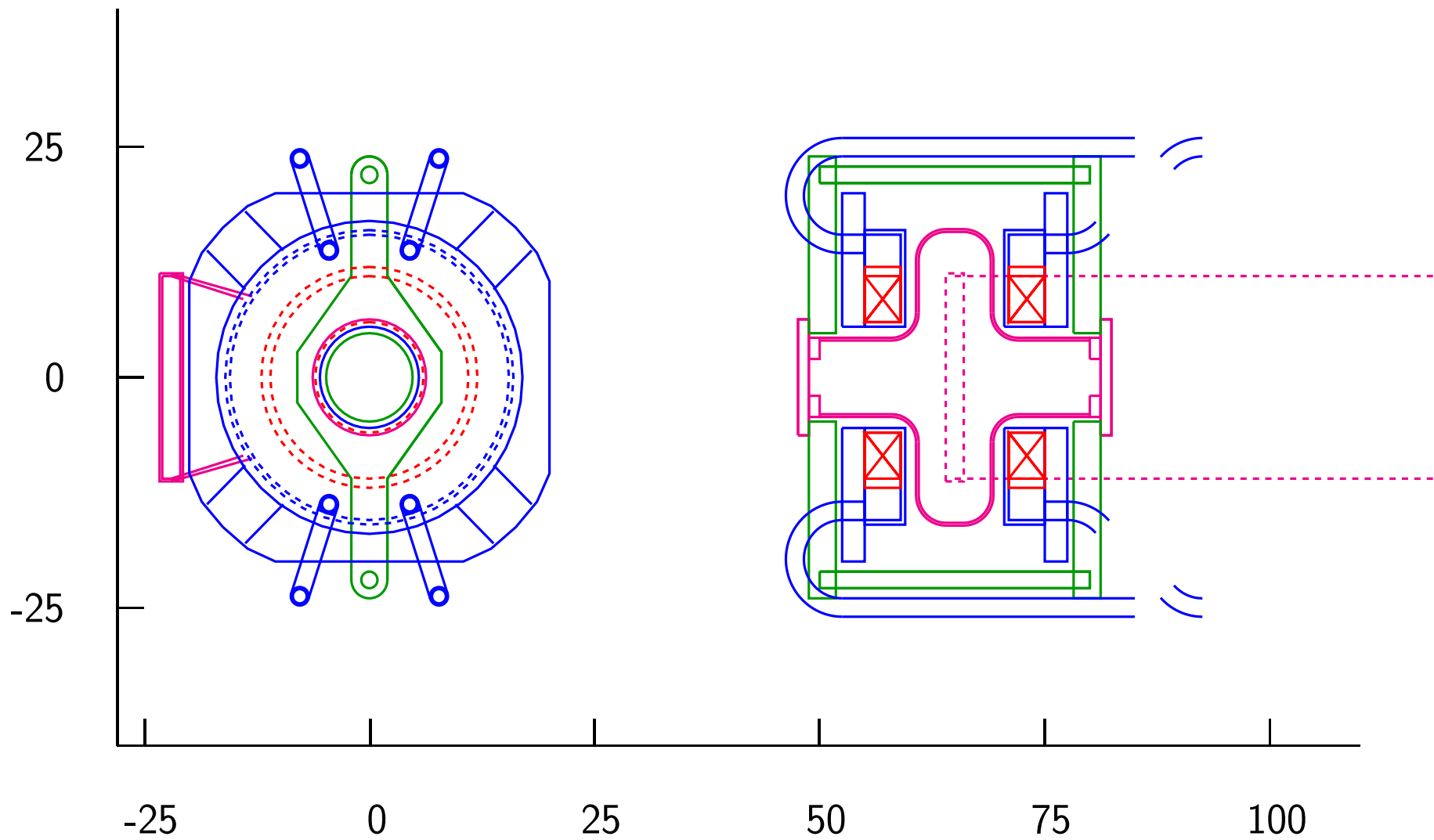
Test in Lag G magnet



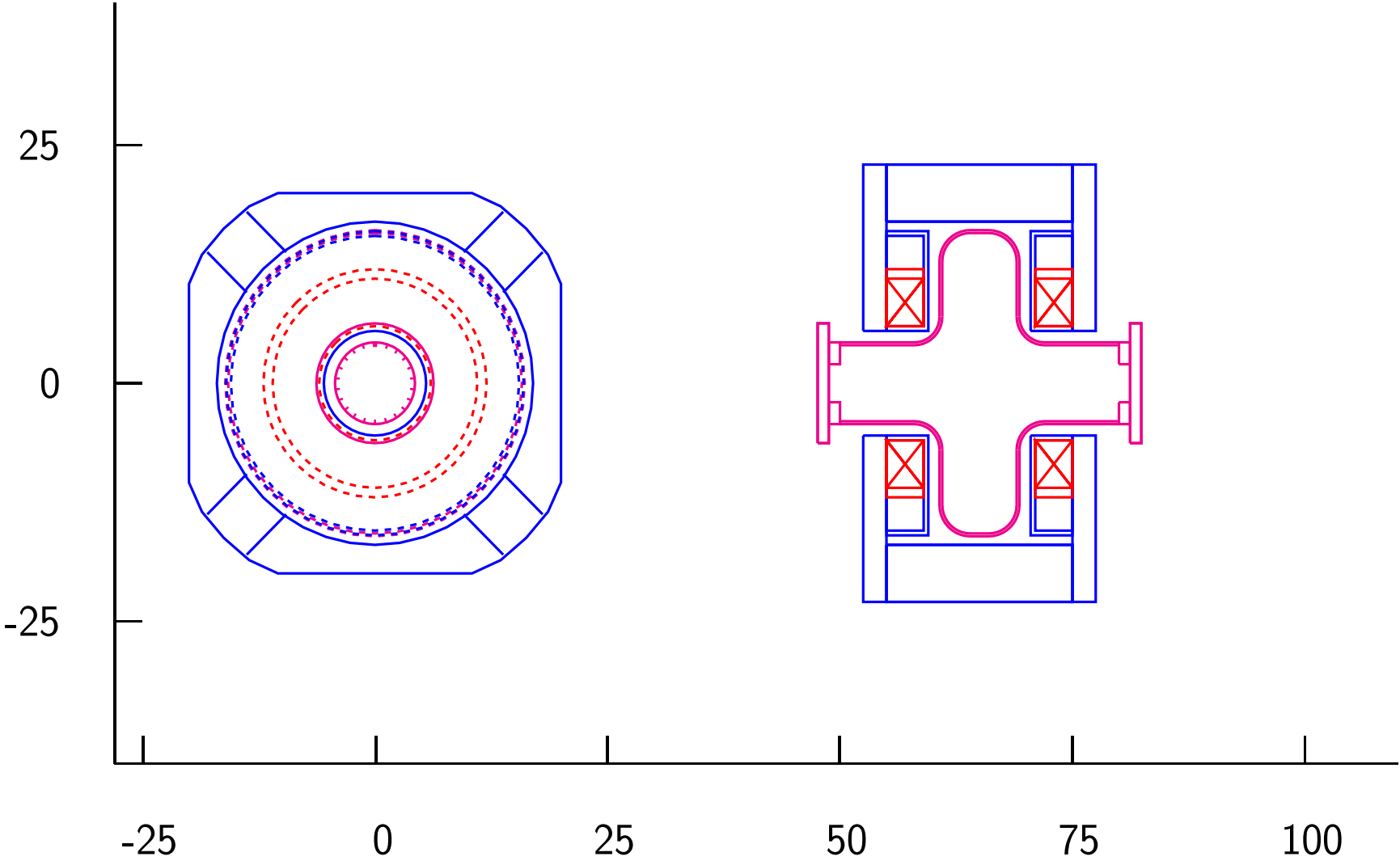
Cavity and Tuner



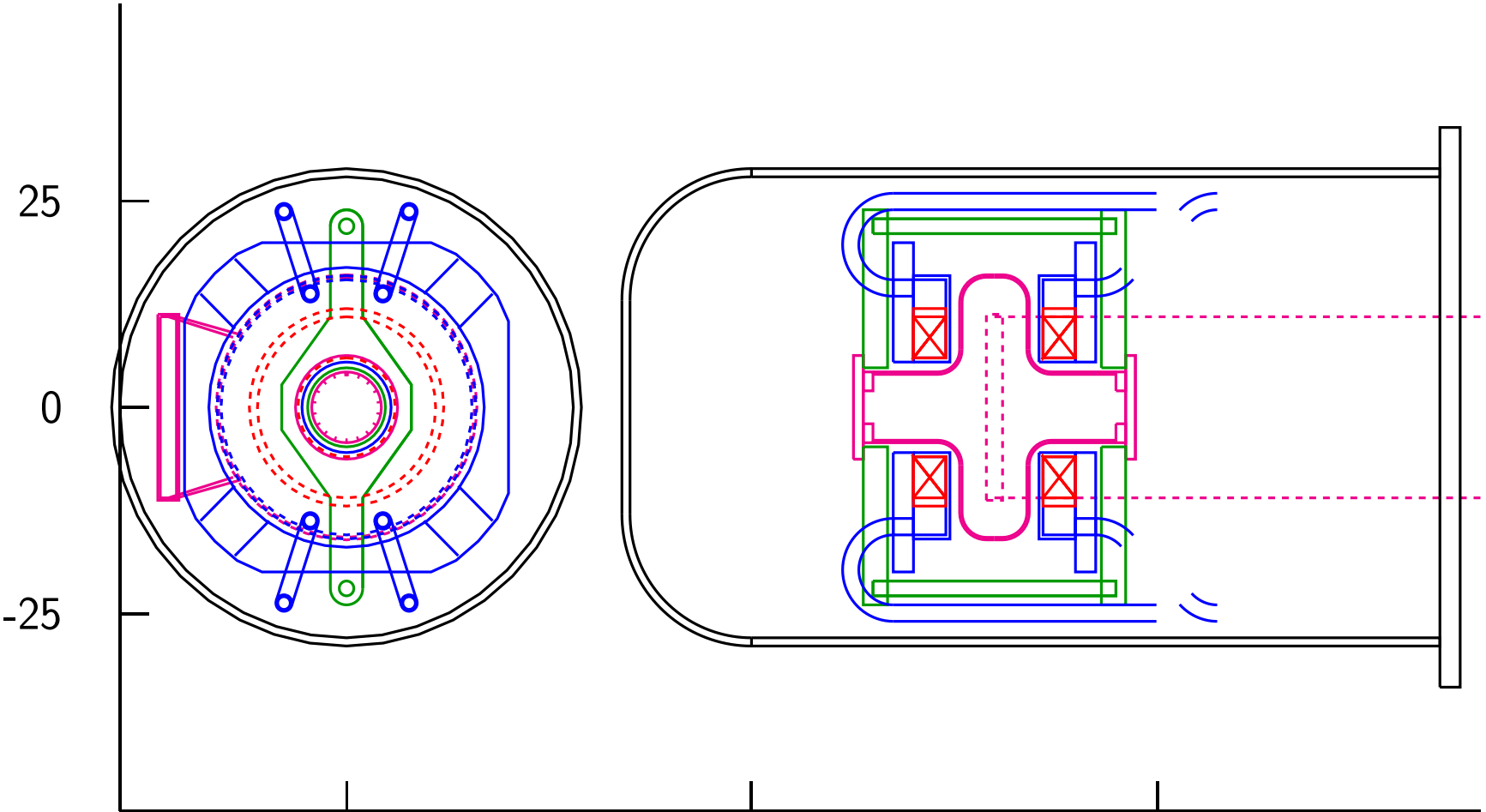
Vertical section of Solenoids



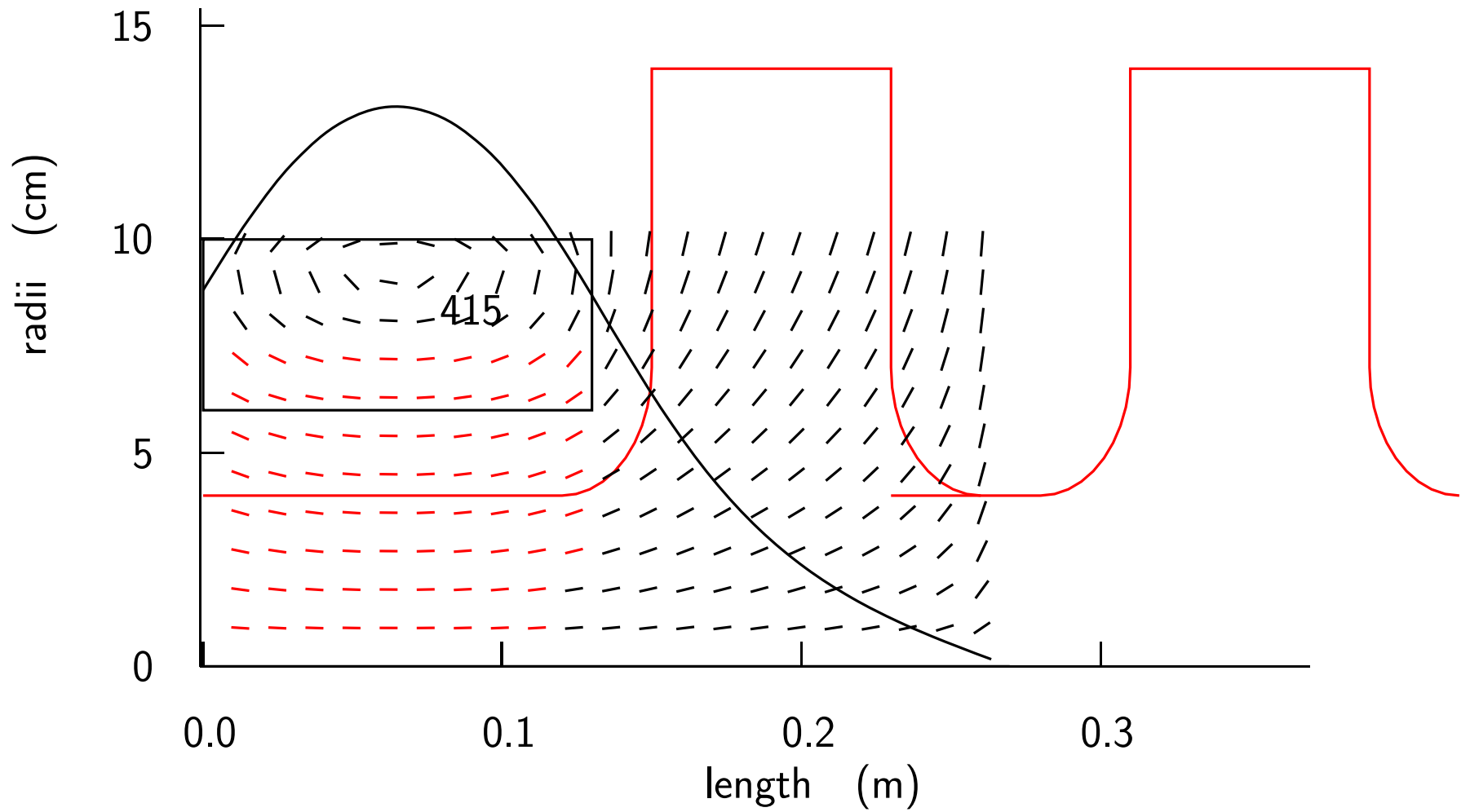
45 degree section of Solenoids

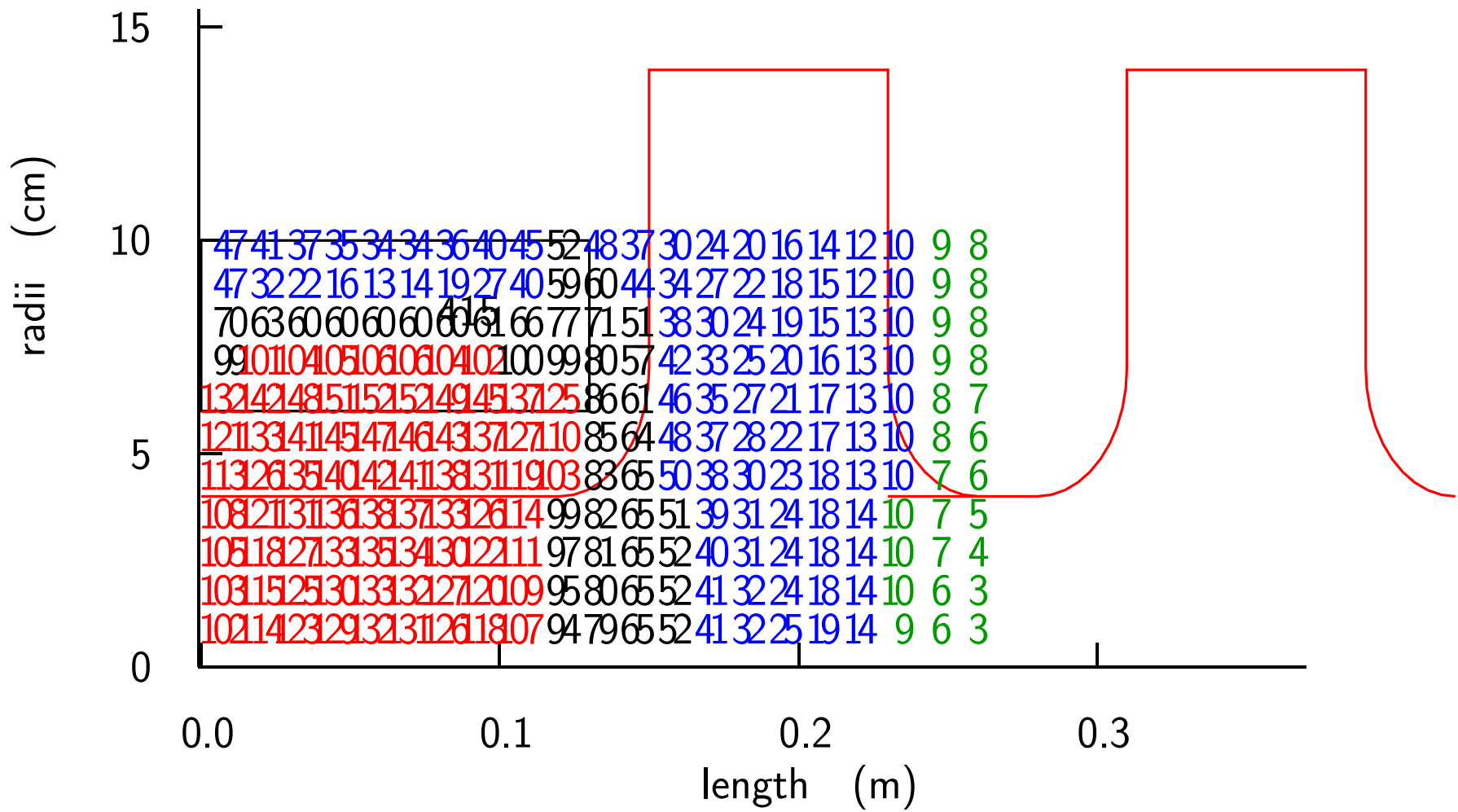


With Vacuum and Mounting Plate

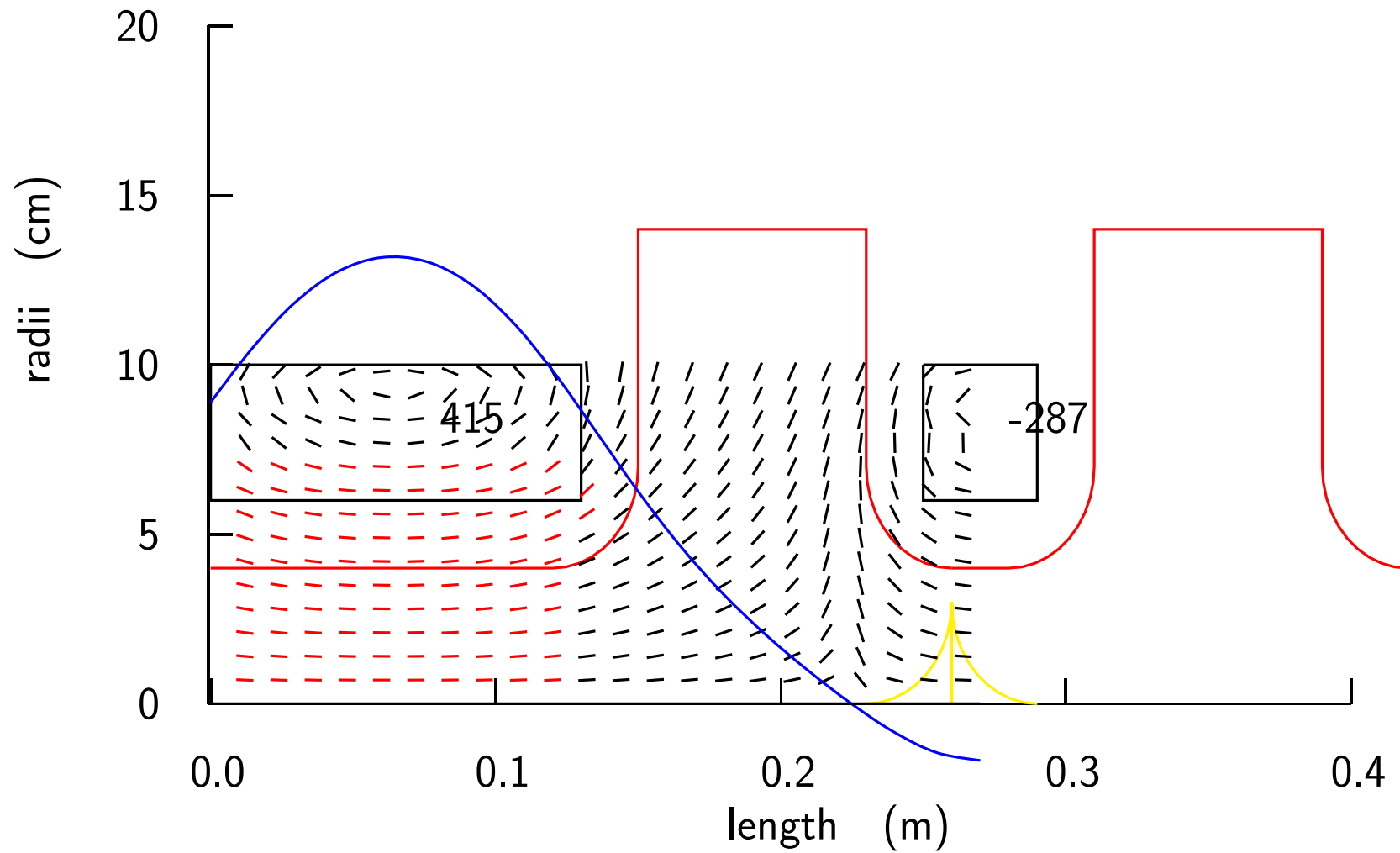


Experiment #2 Double cavity with no center coil

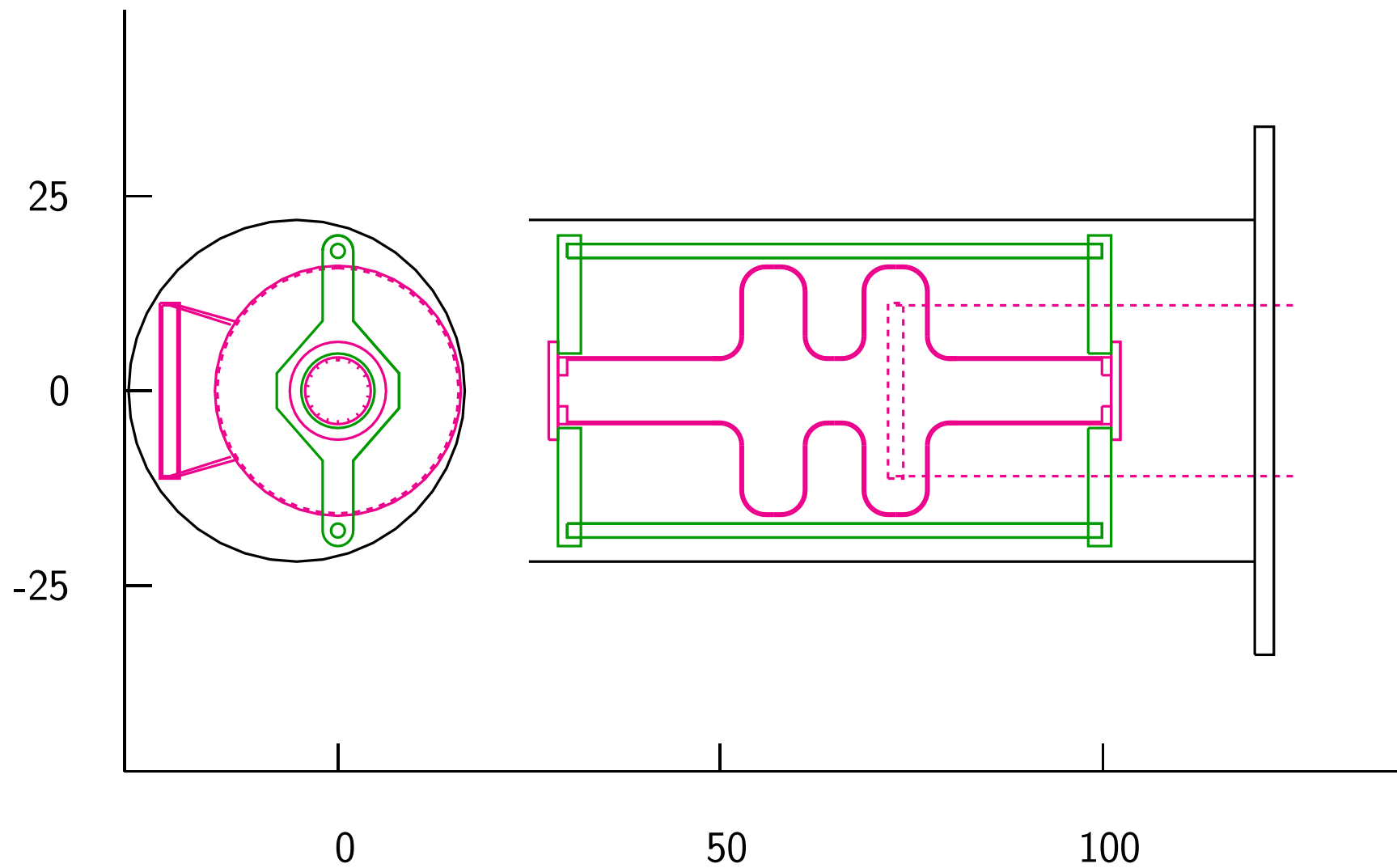




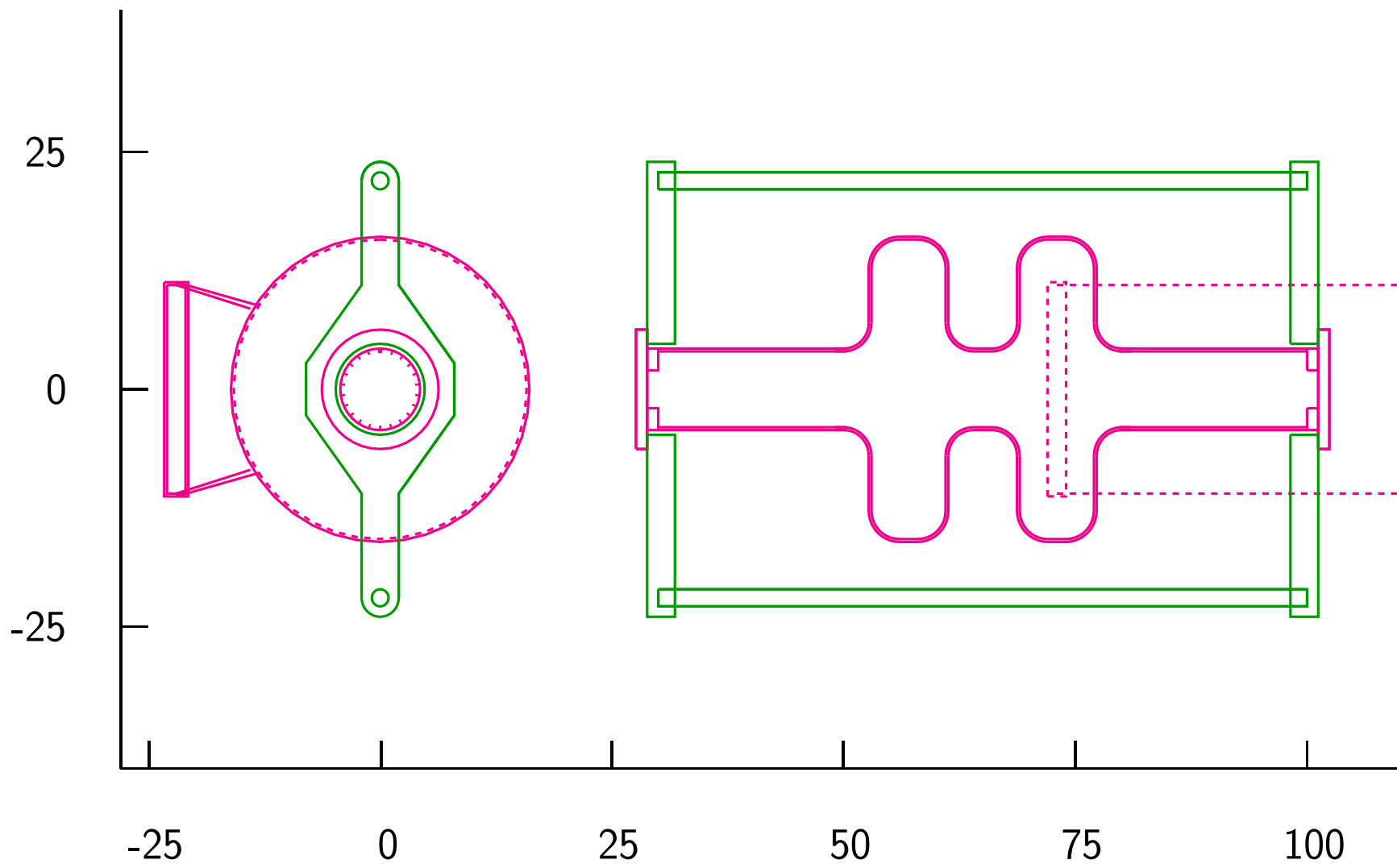
Experiment #4 with opposed center coil



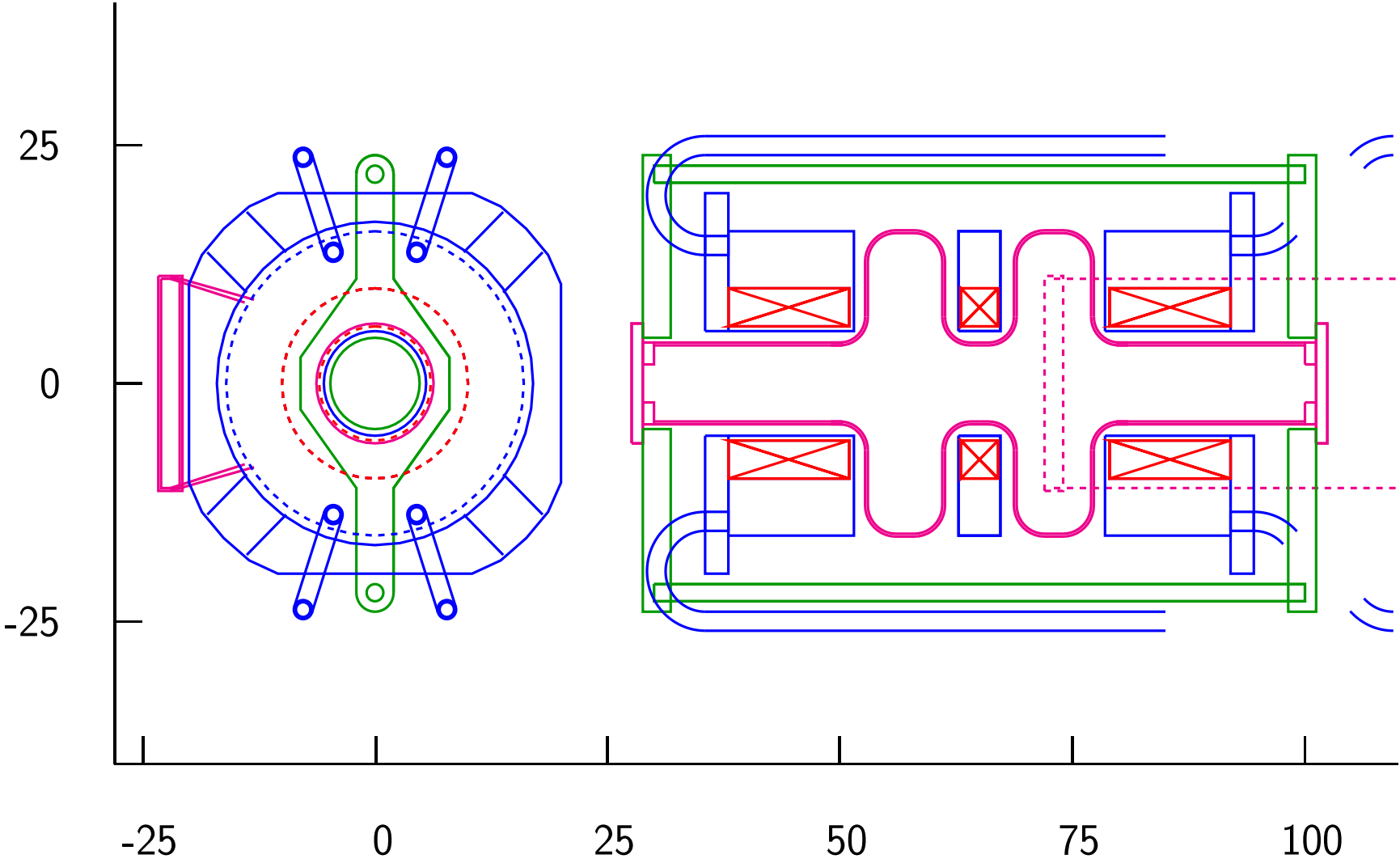
Test in Lag G magnet



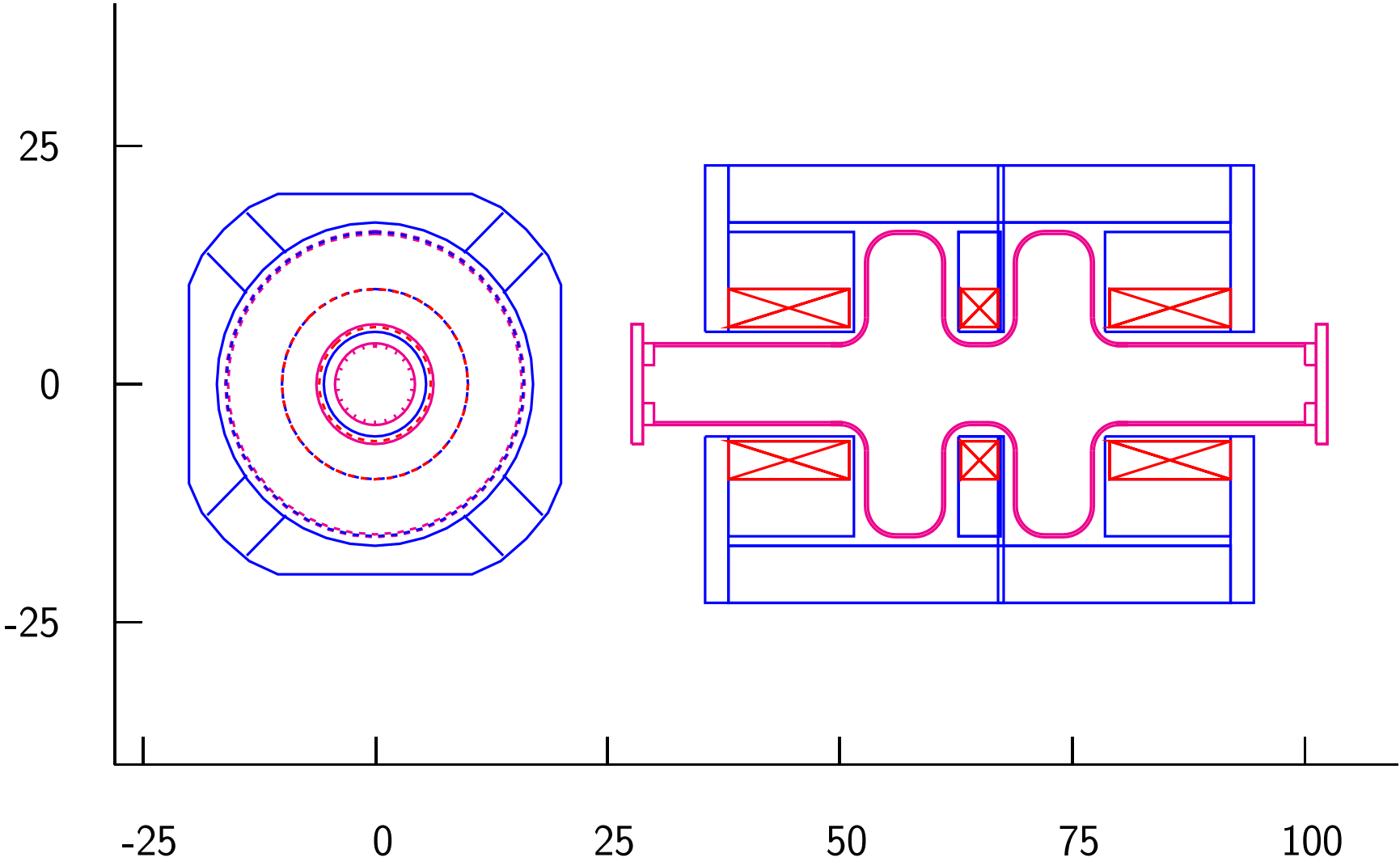
Cavity and Tuner



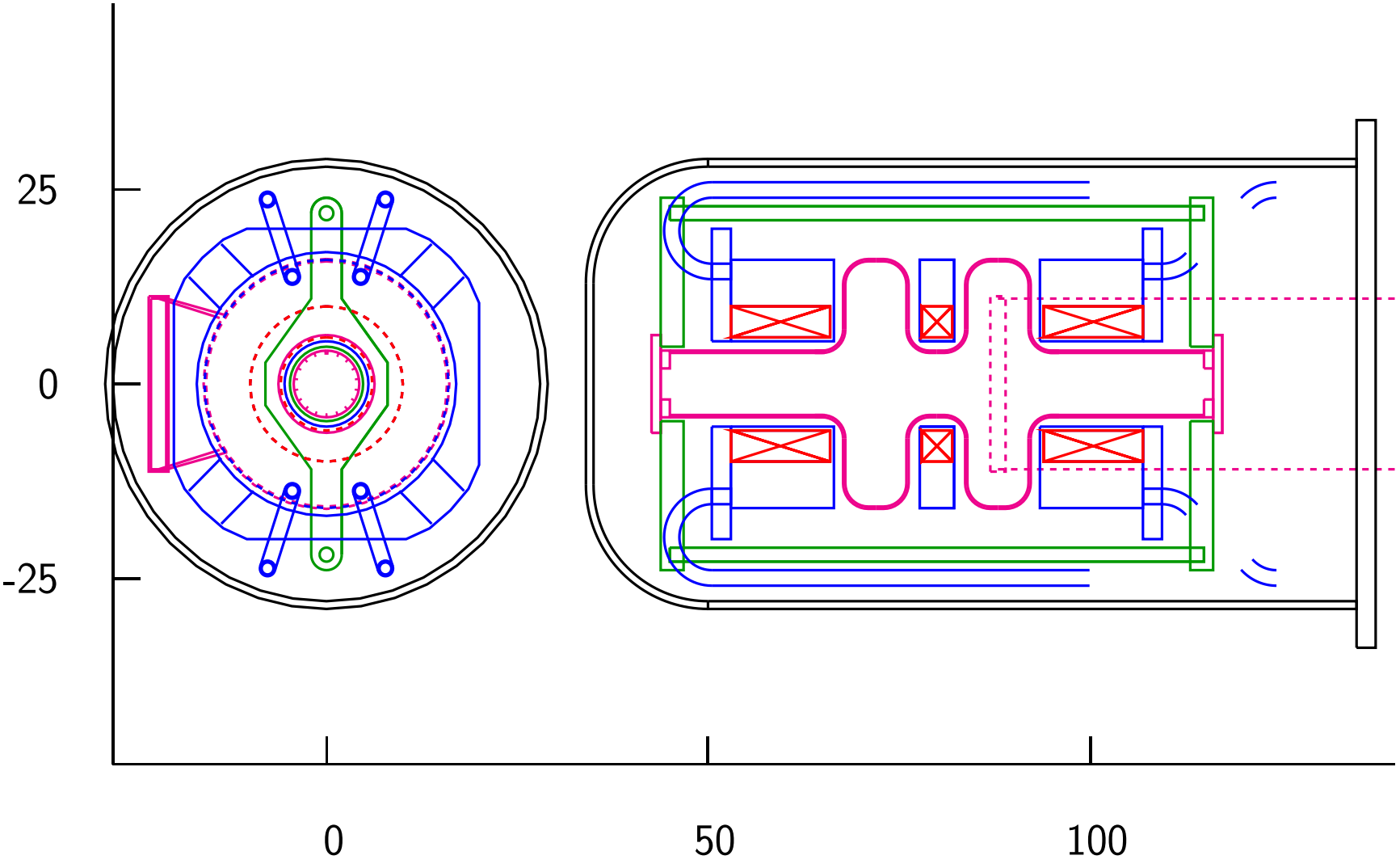
Vertical section of Solenoids



45 degree section of Solenoids



With Vacuum and Mounting Plate



Radial Force Constraint

If radial forces only constrained at outer radius t

$$\frac{dF_r}{dz}_{\max} = \int B(r) j r d\phi dr$$

For a long solenoid $j = \frac{dB}{dr} \frac{1}{\mu_o}$

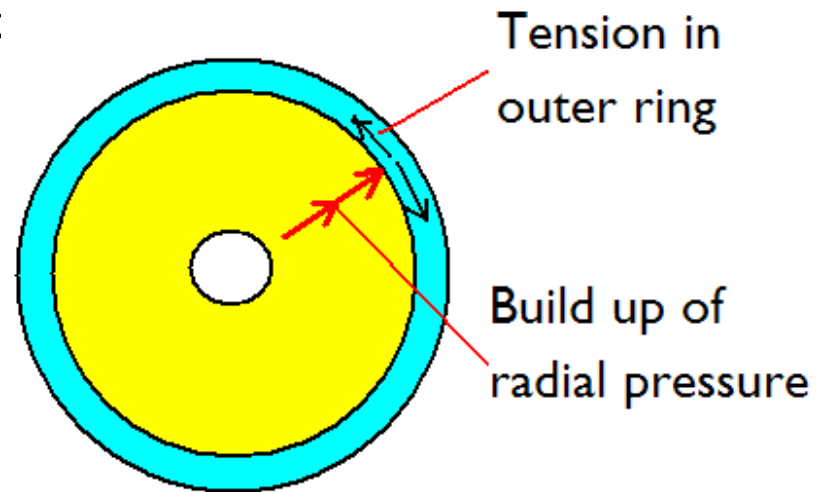
$$B = \left(\frac{r - r_o}{r_2 - r_1} \right) \frac{B}{B_2} \text{ so } r = r_1 + (r_2 - r_1) \frac{B}{B_2}$$

$$\frac{dF_r}{dz} = \frac{d\phi}{\mu_o} \left(r_1 B dB + (r_2 - r_1) \frac{B^2}{B_2} dB \right)$$

$$P_2 = \frac{\int dF_r}{r_2 d\phi} = \frac{B_2^2}{\mu_o} \left(\frac{r_1}{2 r_2} + \frac{1}{3} + \frac{r_1}{3 r_2} \right)$$

For $B = 15$, $r_1/r_2 = 1/2$ and $\mu_o = 4\pi \cdot 10^{-7}$ $P_{r,\max} = 75 \text{ MPa}$

Compared with the compression strength of epoxy filled superconductor stacks of about 130 MPa.



Strain in coil due to stretch of outer constraint

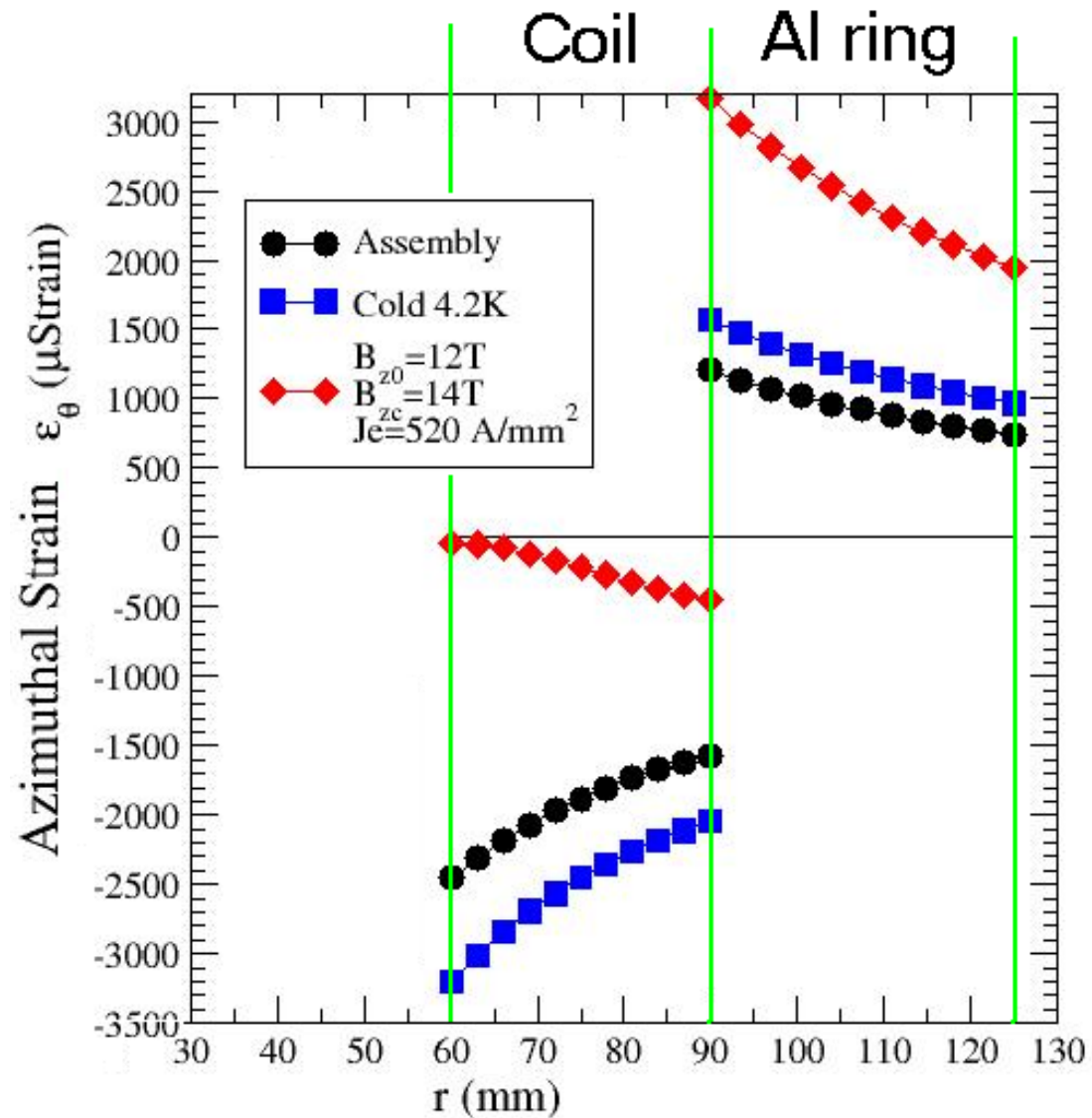
$r=12$ cm $t=2.5$ cm $E=200$ GP (ss)

$$S = P_r \frac{r}{t} \frac{1}{E} = 75 \cdot 10^6 \frac{12}{2.5} \frac{1}{200 \cdot 10^9} = 0.18 \%$$

but with low E coil material the inner layers will move out more and have more strain May need precompression by multiple ss rings, ss wound in with cable, or precompression in Al ring

Shlomo Caspi's analysis

With 100 micron radial precompression that can be supplied by inserting cold coil into warm ring



Coil does not go into tension when powered

Forces between end coils

exp1 single cavity

$r=6$ cm $dr=5$ cm $l=4$ cm c-c= 16 cm $B_{axis}=4$ T $B_{max}=7$ T $j=300$

$B_r=.2$ T $I=300 \times 40 \times 50 = 0.6$ MA $A=2 \pi(.1^2 - .06^2)=.02$ m²

$F \approx IAB_r/\Delta r=60,000$ N integration gave $F=51$ kN

if 8 rods of .5 in dia then Tension= $.051/(8 \pi .006^2)$ 56 MP ok

Deflection of plate $t=3.17$ cm, span= 15 cm, width 15 cm, load $.051/4$ uniform

$$\begin{aligned}\delta &= \frac{5 WL^3}{384 EI} = \frac{5 WL^3 12}{384 Et^3 w} = \frac{5 WL^3 12}{384 Et^3 w} \\ &= \frac{5 .051/4 10^6 .25^3 12}{384 200 10^9 .0317^3 .15} = 32 \text{ } (\mu\text{m})\end{aligned}$$

exp2 Double cavity with no coil at center

$r=6$ cm $dr=4$ cm $L=13$ cm c-c= 39 cm $B_{axis}=13$ T $B_{max}=15$ T $j=400$ B at 3 cm= 0.7 T

$B_r=.04$ T $I=400 \times 130 \times 40 = 2.1$ MA $F=.024$ MN

easier than exp 1

Exp 4 Double cavity with coil at center situation needs calculation

Costs of Nb₃Sn Conductor

- D20 4 deg 12.8 T 5 cm radial thickness
- 12 T 2900 A/mm² 47% Cu Oxford Hight Jc Nb₃Sn
- 15 T 1500
- 1/3 for wire, 15% for space 100 microns for insulation wire 0.7mm cable 1.25 by 2mm (for 6 strand)
- 15\$/m for sleeve, 1100\$/kg=295 m (3.7\$ per m strand, 22.4 \$/m for cable), 20,000\$ for 500 m cable (40\$/m)
- Young's of filled coil 42 GP

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