

An Induction Kicker for Muon Cooling Rings

and other Applications Needing
Very Large Apertures

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Study 2 cooling is 100 m

If Ring is to be cheaper:

Circ \ll 100 m

say 30 m

e.g. Balbakov 4 sided ring,

Palmer 11 cell ring

Balbakov 8 cell (60m) more expensive

Palmer 5 cell (16 m circ) req faster kicker

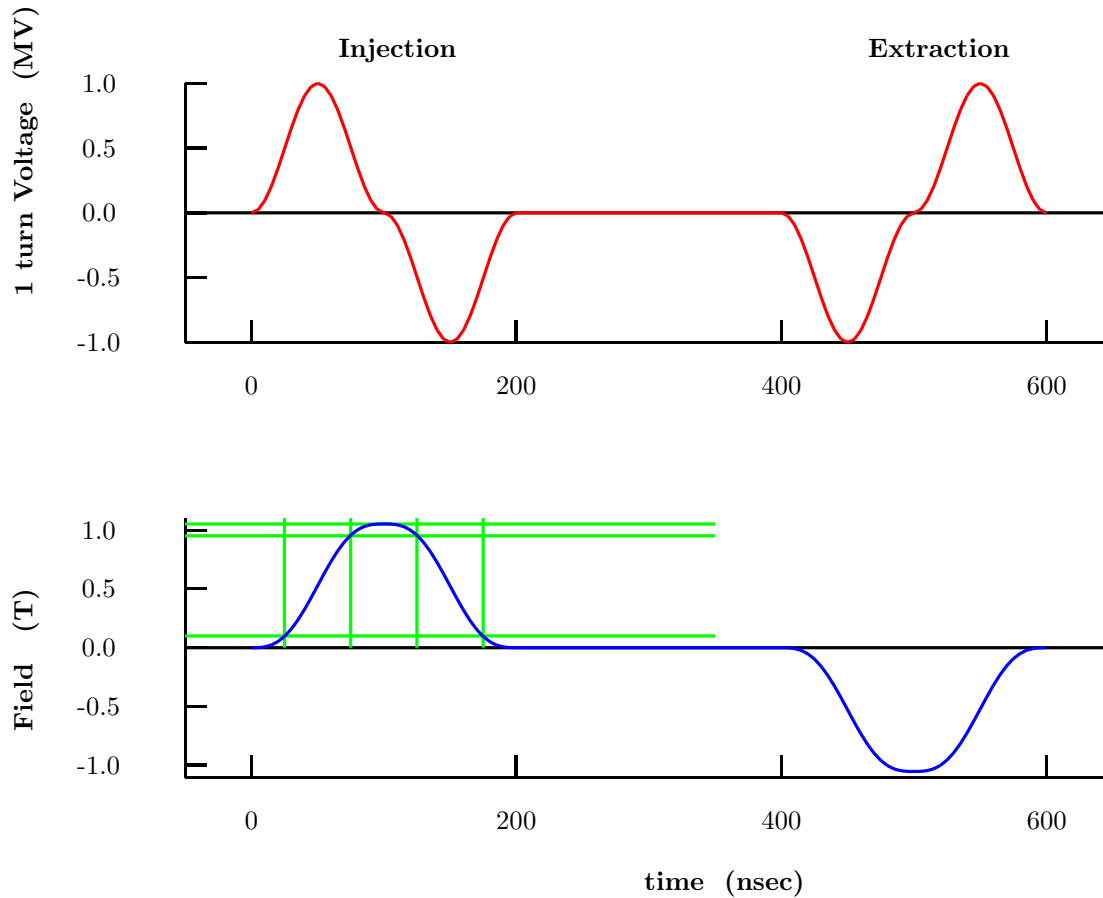
30m is Compromise

Time = 100 nsec

50 nsec for train

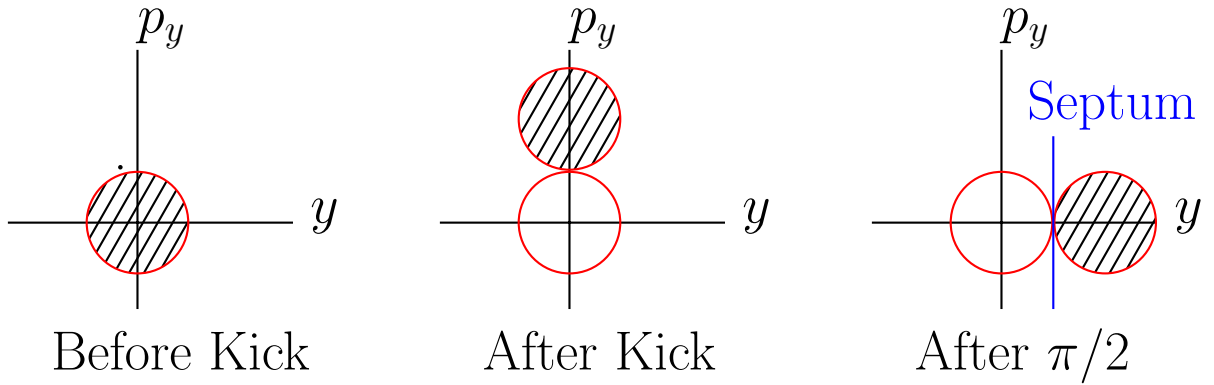
50 nsec for kicker rise

Required Volts and Current



- If req. $\delta B \leq \pm 5\%$
- $\text{circ}/2 = \text{rise } 10\% \text{ to } 90\%$
= 50 nsec

Minimum Required kick



Defining

For Aperture:

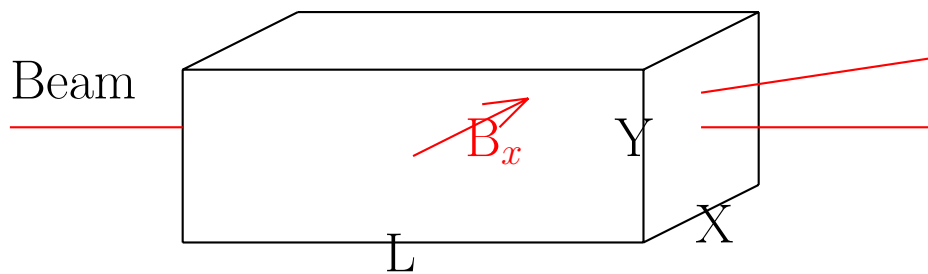
$$f_{\sigma} = \frac{A_p}{\sigma}$$

For leakage flux:

$$\Phi = f_{\Phi} B_x L Y$$

For finite μ 's:

$$\int B dl / \mu = f_{\mu} B X$$



Formulae

$$\Delta p_y = B_x L c = m_\mu 2 f_\sigma \sqrt{\frac{\epsilon_n \beta \gamma}{\beta_y}}$$

$$X = 2 f_\sigma \sqrt{\frac{\epsilon_n \beta_x}{\beta \gamma}}$$

$$R = \frac{Y}{X} \approx \left(1 + \frac{L}{2 \beta_y} \right)$$

$$I = \frac{f_\mu B X}{\mu_o} = \frac{f_\mu 4 f_\sigma^2 m_\mu}{\mu_o c} \frac{\epsilon_n}{L}$$

$$V = \frac{f_\Phi B Y L}{t_{\text{rise}}} = \frac{f_\Phi 4 f_\sigma^2 m_\mu R}{c} \frac{\epsilon_n}{\tau}$$

$$J = f_\mu f_\Phi \frac{B^2 L X Y}{2 \mu_o} = f_\mu f_\Phi \frac{m_\mu^2 8 f_\sigma^4 R}{\mu_o c^2} \frac{\epsilon_n^2}{L}$$

Note

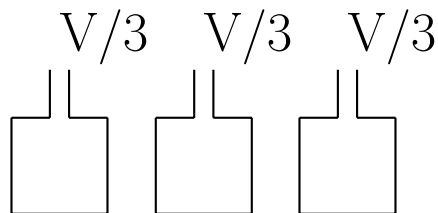
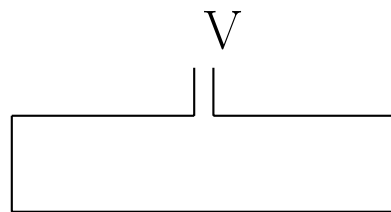
- V independent of E , β_{\perp}
- V & $I \propto \epsilon_n$
- $J \propto \epsilon_n^2$

- muon $\epsilon_n \gg$ other ϵ_n 's
- So muon kicker Joules \gg other kickers
- Nearest are \bar{p} kickers

		μ Cooling	CERN \bar{p}	Ind Linac
f_Φ		1.05		
f_μ		1.05		
f_σ		3		
m_μ	V	$1.05 \cdot 10^8$		
c	m/s	$3 \cdot 10^8$		
ϵ_n	π mm	10		
β_x	m	1.0		
$\int B dl$	Tm	.30	.088	
L	m	1.0	≈ 5	5.0
t_{rise}	ns	50	90	40
t_{pulse}	ns	100	500	100
β_γ		2		
B	T	.30	\approx 0.018	0.6
X	m	.42	.08	
Y	m	.63	.25	
I	kA	105		
$V_{1\text{turn}}$	kV	3,970	800	5,000
U_{magnetic}	J	10,450	\approx 13	8000
n_{parallel}		20	10	32
n_{units}		12	10	10
$I_{\text{p.s.}}$	kA	192		73
$V_{\text{p.s.}}$	kV	182	80	190
$U_{\text{p.s.}}$	kJ	870		800

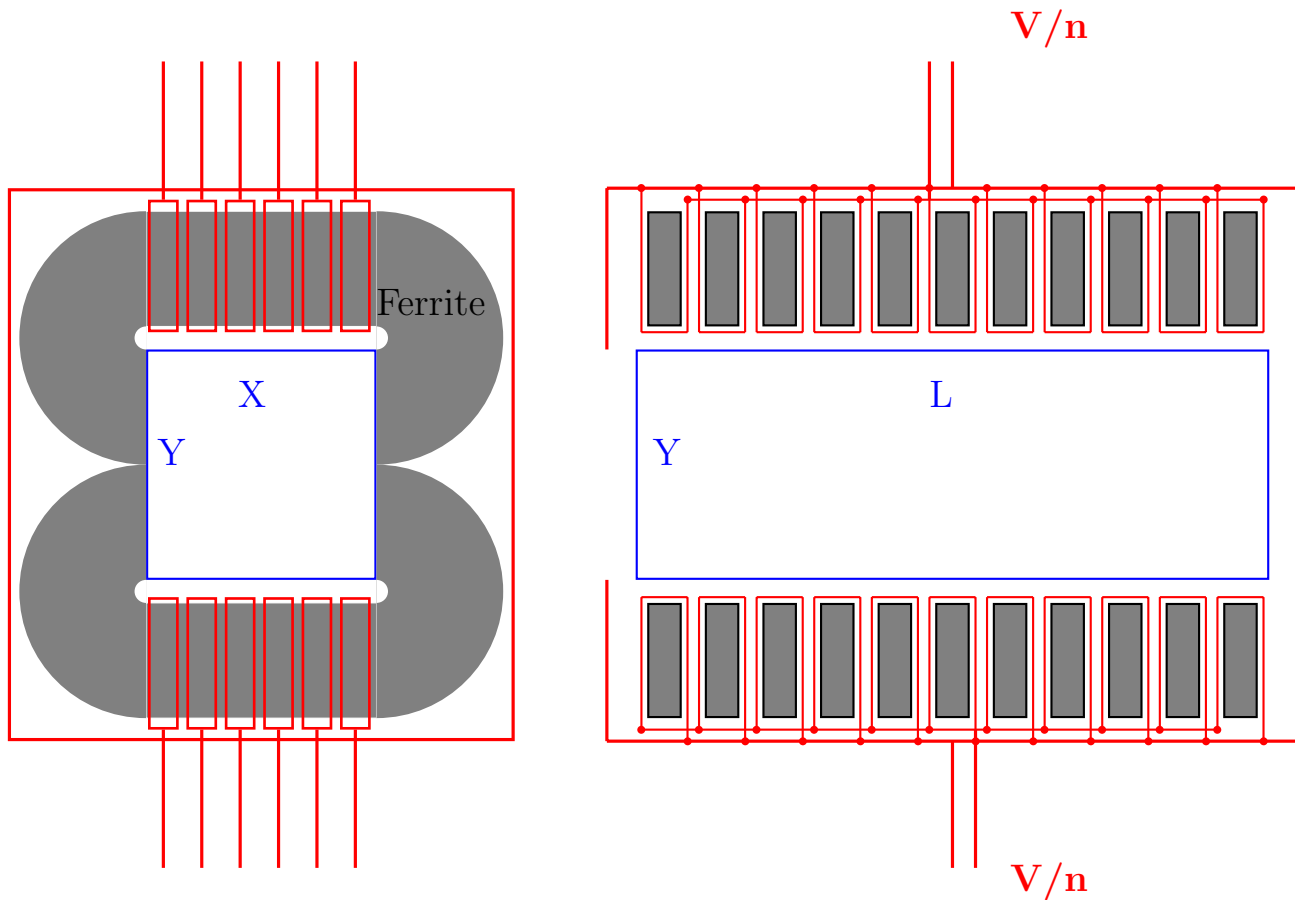
Note

- J is 3 orders above \bar{p}
 - But same order as 5 m Induction
 - And t same order as Induction
 - But V is too High
-
- Because L/X only ≈ 3
Conventional subdivision only /3



New Idea

- Drive Flux Return
- Subdivide Flux Return
- Conducting Box Removes Stray Field Return



End View

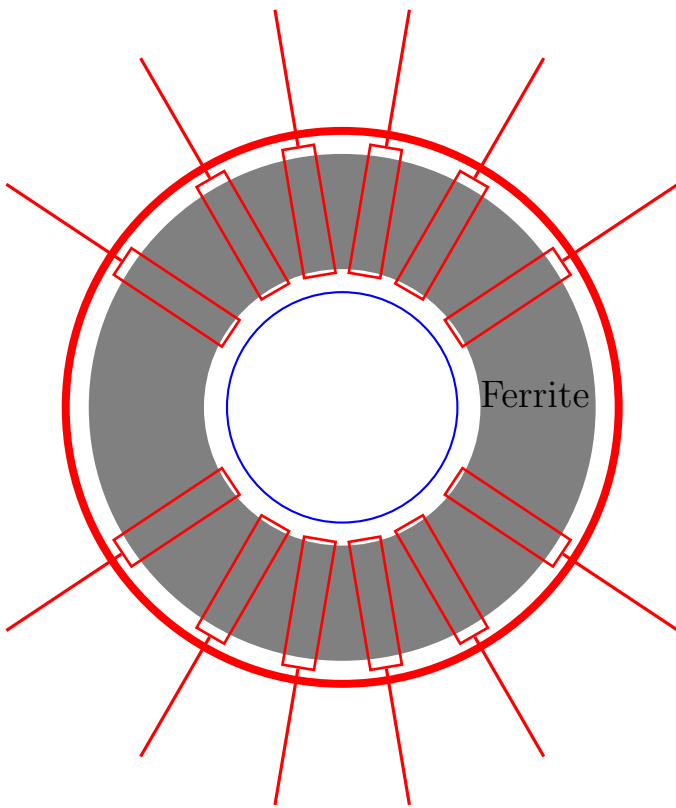
Side View

- Divide yoke by (2×11)
- connect 11 loops in parallel
- $V / \text{loop} = 3970/22 = \mathbf{182 \text{ kV}}$
- $I / \text{side} = 105 \times 11 = \mathbf{1155 \text{ kA}}$
- 6 Drivers per yoke, then:
 - number of drivers = $2 \times 6 = \mathbf{12}$
 - $I / \text{driver} = 1155/6 = \mathbf{192 \text{ kA}}$
 - $U / \text{driver} = 1045/12 = \mathbf{870 \text{ J}}$
 - $U / \text{driver} \approx U / \text{Induction driver}$
 - $V / \text{driver} \approx V / \text{Induction driver}$
 - I is higher from inductive load

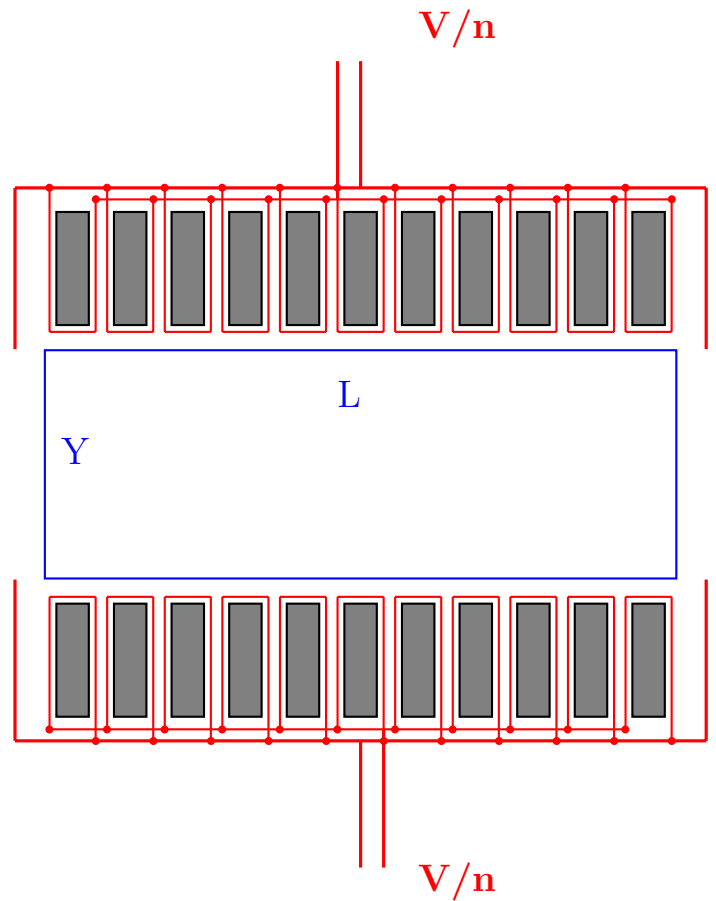
If the load must be made resistive, then the total energy would be 4 times higher ($V \times I \times t_{\text{pulse}}$ vs. $V \times I \times t_{\text{rise}} / 2$).

Cos Theta Version

- $J \approx \times \pi/4$
- V 's not the same for different ϕ 's



End View



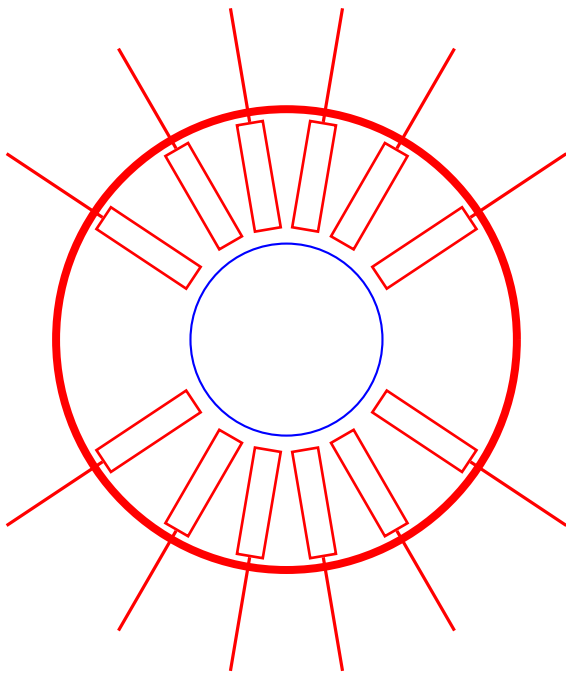
Side View

Works with no Ferrite

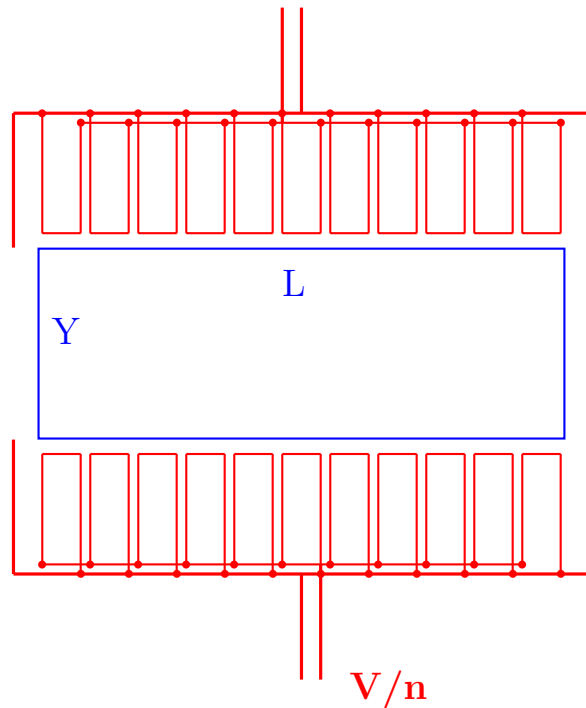
- $V = \text{the same}$
- $J \approx 2\times$
- $I \approx 2\times$

But

- No rise time limit
- Not effected by solenoid fields V/n

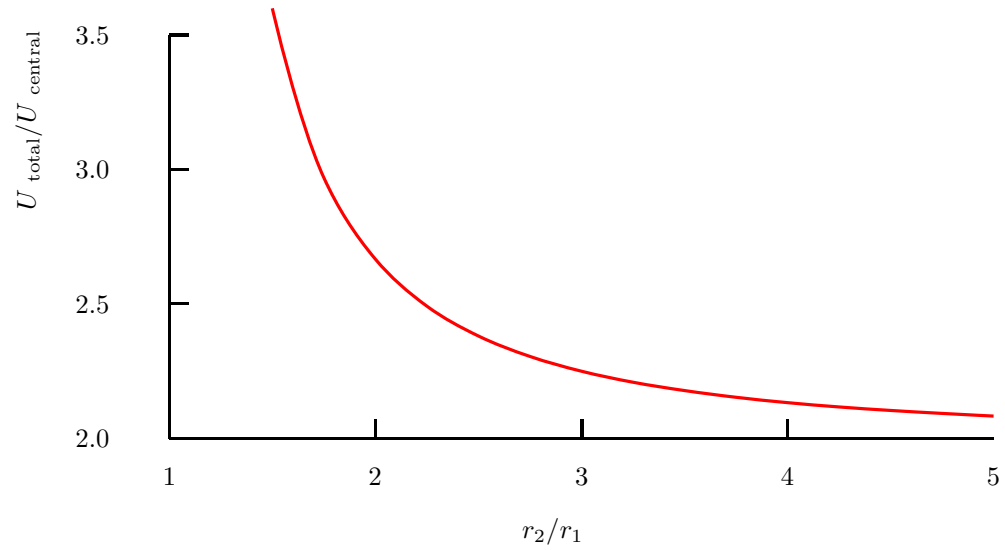


End View



Side View

Stored Energy vs. rad 2



e.g.

$$r_2/r_1 = 3:$$

$$U(\text{no Fe}) = 2.25 \times U(\text{Fe})$$

”Resonant” Mag Amp Driver

Assume:

- A single compression stage;
- Negligible cable distance from driver to kicker;
- A sudden saturation at I_s from an initial large inductance L_1 to a small inductance L_2 ;
- A purely inductive kicker magnet with inductance L ;
- Start the clock at $t=0$ with the drive capacitor C charged to V_o and no current flowing.

Initially: long time constant τ_L

$$\tau_L = \sqrt{(L + L_1)C}$$

$$V_{\text{Capacitor}} = V_o \cos\left(\frac{t}{\tau_L}\right)$$

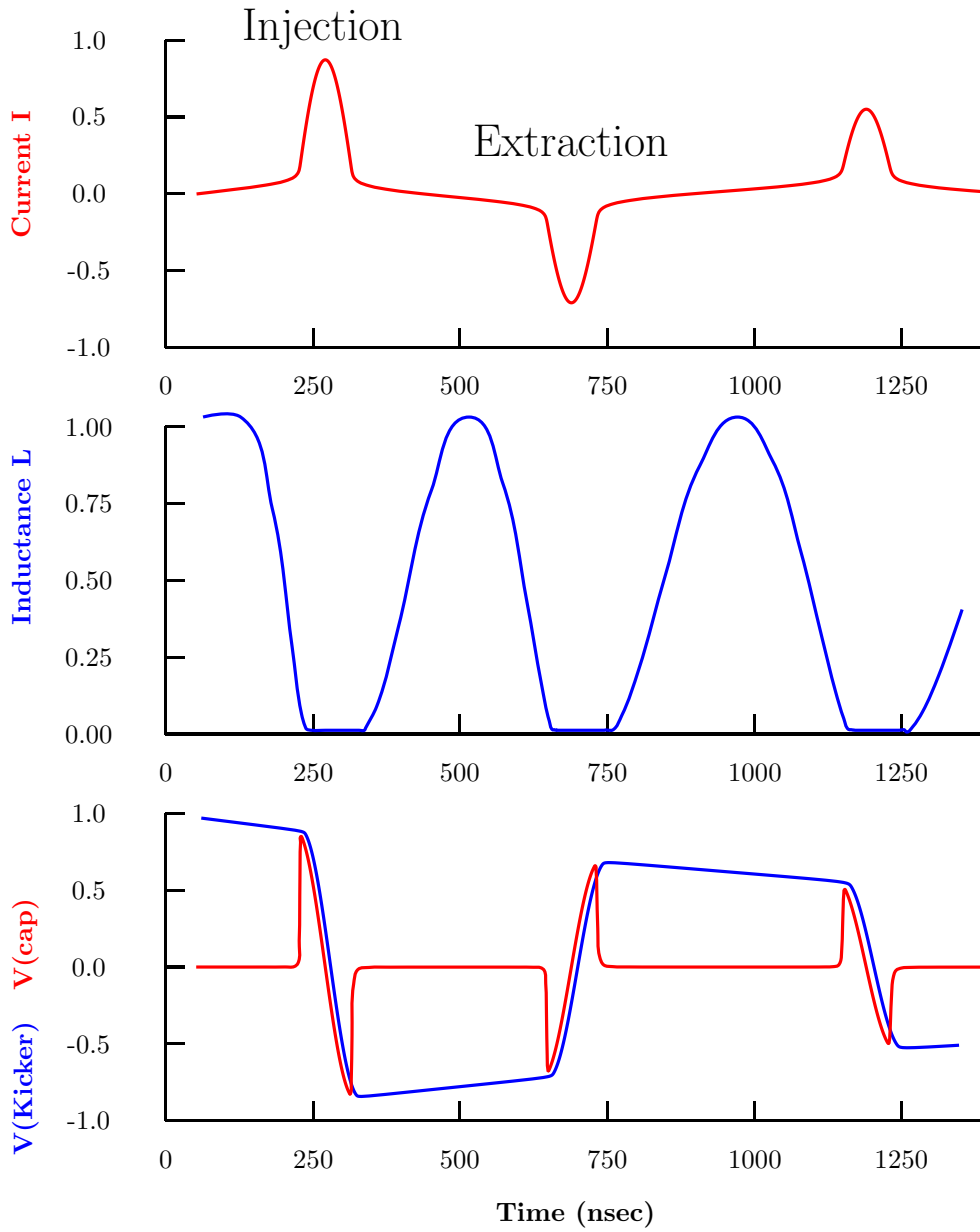
$$V_{\text{Kicker}} = V_1 \left(\frac{L}{L + L_1}\right)$$

$$I = I_o \sin\left(\frac{t}{\tau_L}\right)$$

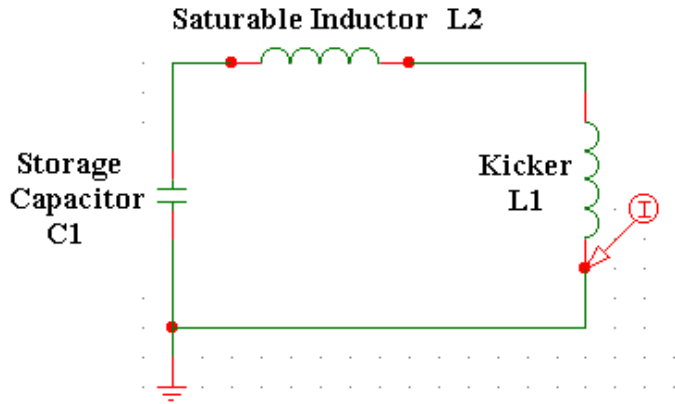
When current = saturation current: Short time constant

$$\tau_S = \sqrt{(L + L_2)C}$$

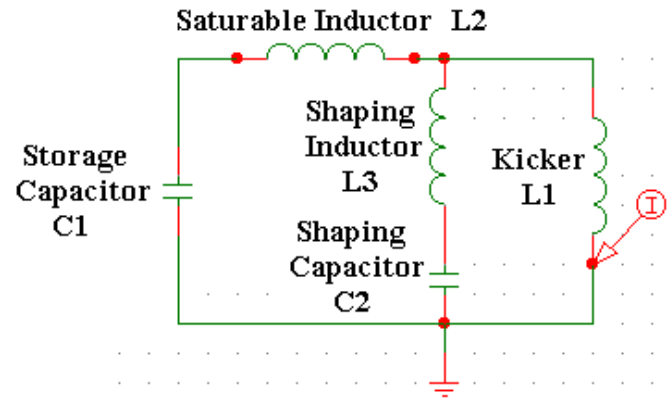
If $\tau_L \approx 100 \times \tau_S$,
Optimistic ?



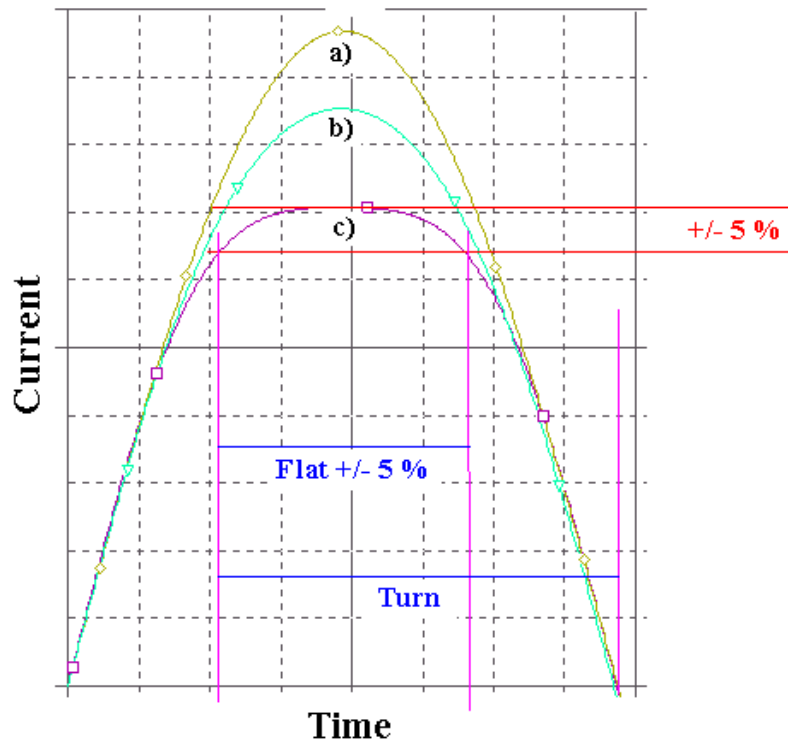
Increased Flat Top



Circuit a)

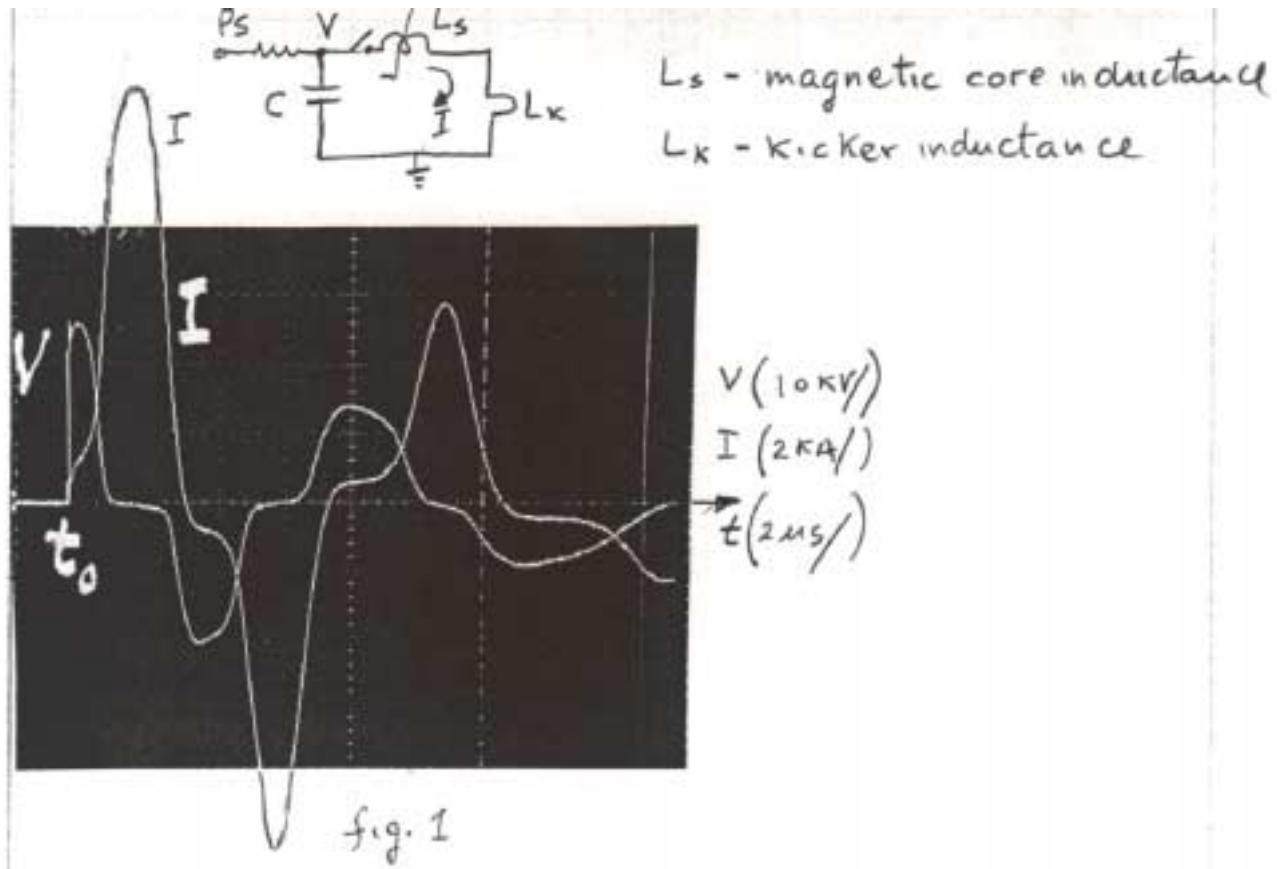


Circuits b) and c)



case	C1	L1	L2	C2	L3	V/Va	U/Ua	flat/turn
a)	142	100	7			1.0	1.0	0.46
b)	120	100	7	20	90	0.88	1.29	0.52
c)	100	100	7	40	53	0.73	1.89	0.57

Circuit Model



- May be hard for many turns
- Not simulated with initial stages

Conclusion

This study suggests that even the first cooling ring injection and extraction problems may be soluble.

But much work remains.

The proposed kicker could also have application in FFAG acceleration of large emittance beams for neutrino factories.