

Permanent Magnet Diploes and Quadrupoles for FFAGs

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EEC

- (1) Permanent Magnet Overview
- (2) Some Design Considerations
- (3) Radiation Effect
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Overview **Types of Commercial magnets**



(BH)_{max} versus Maximum Operating Temperature

Overview





- (1) Magnetic performance
- (2) Corrosion resistance
- (3) Thermal stability
- (4) Radiation resistance
- (5) Magnetization direction
- (6) Manufacturability
- (7) Cost



- Typical magnetic properties, in terms of energy product, of selected commercial magnets:
- ✓ Sintered Nd-Fe-B magnets: up to 50 MGOe
- ✓ Sintered Sm-Co magnets: up to 32 MGOe
- ✓ Isotropic bonded Nd-Fe-B magnets: up to 10 MGOe
- ✓ Sintered ceramic magnets: up to 4 MGOe
- ✓ Cast Alnico magnets: up to 9 MGOe

Maximum operating temperature of sintered magnets			
Magnets N	Aaximum Operating Temp.*		
NdFeB with _i H _c =12 kOe	80°C		
NdFeB with _i H _c =17 kOe	120°C		
NdFeB with _i H _c =20 kOe	150°C		
NdFeB with _i H _c =25 kOe	180°C		
Conventional SmCo magnets	300°C		
EEC24-T400 magnets (patented & avai	ilable) 400°C		
EEC20-T500 magnets (patented & avai	ilable) 500°C		
EEC16-T550 magnets (patented & avai	lable) 550°C		
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Rare Earth Magnets -- Properties vs. Temperature



Long-term Thermal Stability of SmCo Magnets at 300°C in Air







High temperature magnets

➢ DoD initiated the More Electric Aircraft program, which requires magnets with maximum operating temperature more than 400°C

➢ Funded by the Department of Defense, a series of sintered SmCo 2:17 magnets were developed at EEC with maximum operating temperature as high as 550°C

➤These patented SmCo UHT magnets were introduced to the industry in 1999.



PM Grades	B _r (kG) (kG)	(BH) _{max} (MGOe)	Max. operating temp (°C)
EEC2:17-31	11.6	31	250
EEC2:17-27	10.8	27	300
EEC24-T400	10.2	24.5	400
EEC20-T500	9.3	21	500
EEC16-T550	8.6	17	550



Nd-Fe-B sintered magnets

Key features:

- ≻Highest (BH)_{max} available (up to 50 MGOe)
- Less expensive than Sm-Co magnets
- Corrosion resistance is not good
- >Special coating is required
- ➢ Maximum operating temperature is very low compared to SmCo magnets



PM Grades	B _r (kG) (kG)	(BH) _{max} (MGOe)	Max. operating temp (°C)
N50	14-14.5	48-51	70
N45	13.2-13.8	43-46	70
N45M	13.2-13.6	43-46	100
N42SH	12.8-13.2	40-43	120
N33UH	11.3-11.7	31-34	180

Some Design Considerations



Permeance Coefficient P_c

In the magnetic circuit, a magnet will operate at a specific point on its extrinsic demagnetization curve:

 $P_c = B_d / H_d$



Also known as **load line** or **operating point**

➢ It is related to the dimensions of the magnets and the associated magnetic circuit

Why straight-line demagnetization curves?





The effects of radiation on permanent magnets was studied at EEC under a NASA STTR Contract

>All Samples have a L/D ratio of 1.25

Permanent Magnets Studied:

- EEC T500 and T300 SmCo 2:17 magnets
- ✤ Nd-Fe-B Magnets
- Radiation Source: Ohio State University Research Reactor



OSU Reactor



Samples in quartz tubes







All reports had Neutron E = 0.1-10 MeV. Neutron flux: $4x10^{12}$ (Cost) and $2.1x10^{13} \text{ n/(cm 2.s)}$ (Chen et al)

> C.H. Chen, J. Talnagi, J.F. Liu, P. Vora, A. Higgins and S. Liu, IEEE Trans. Magn. 41(2005)3832 17

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Working Point and Radiation Effect





*J.R. Cost et al, IEEE Trans. Mag.***24** (3), 2016-2018 (1988).

The major radiation damage is caused by radiationinduced thermal spikes

- The dominant factor for radiation tolerance is thermal stability, which is related to the following factors:
- (1) Curie temperature of permanent magnets
- (2) Working point of permanent magnet in the system
- (3) Intrinsic coercivity

Permanent Magnet Dipoles



 A_m =Magnet area perpendicular to the direction of magnetization; B_m =Flux density of the magnet corresponding to the operating point of the demagnetization curve; B_g =Flux density desired in the air gap;

 A_g = Cross section area of the air gap perpendicular to the flux lines.

The Air Gap Flux Density Is A Lot Lower Than The B_r Of The Permanent Magnets

Permanent Magnet Dipoles



Halbach PM Dipole Structures: $B_g = B_r \ln(OD/ID)$

There is no upper limit for air gap flux density in Halbach dipole structures according to above equation. But in reality it would be limited by:

(1) The realistic size

(2) The demagnetization effect



Halbach Dipole Example



Halbach Dipole Structure

R



Flux Density Map

Magnetic Mangles

R







45° Position Vector Plot 5.0000e-01 4.5000e-01 4.0000e-01 3.5000e-01 3.0000e-01 2.5000e-01 2.0000e-01 1.5000e-01 1.0000e-01 5.0000e-02 0.0000e+00

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Magnetic Mangles



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Combination of magnetic mangles and Habach structures can make the air gap flux density adjustable to some degree



Halbach Dipole for FFAGs



 ✓ 4 Tesla PM prototype Halbach cylinder was made in Japan.*

✓ EEC has produced many Halbach structures for a variety of applications.

✓ Sintered SmCo or high H_{ci}NdFeB magnets are good choices

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A Example of Halbach PM Quadrupole



B[T]

1.0000e+00 9.0000e-01 8.0000e-01 6.0000e-01 5.0000e-01 4.0000e-01 3.0000e-01 2.0000e-01 1.0000e-01 0.0000e+00

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Adjustable Magnetic Quadrupoles



Adjustable magnetic quadrupoles as reported by Fermi lab and SLAC*:

Diametrically magnetized SmCo 2:17 tuning rods

➤Tuning rods rotation changes the strength of field gradient

* J. T. Volk et al, PAC2001, p217

Summary

✓ Permanent magnet dipoles and quadrupoles can have high air gap flux density if designed with Halbach principles.

✓ Innovative designs can make the air gap flux density adjustable.

✓ Permanent magnet selection might include tradeoffs between cost and performance.

✓ SmCo magnets are far superior to NdFeB magnets with respect to radiation resistance.

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