

Mesh Resolution Study For Pipe With Nozzle Weld Beads

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Location of the Interested Weld

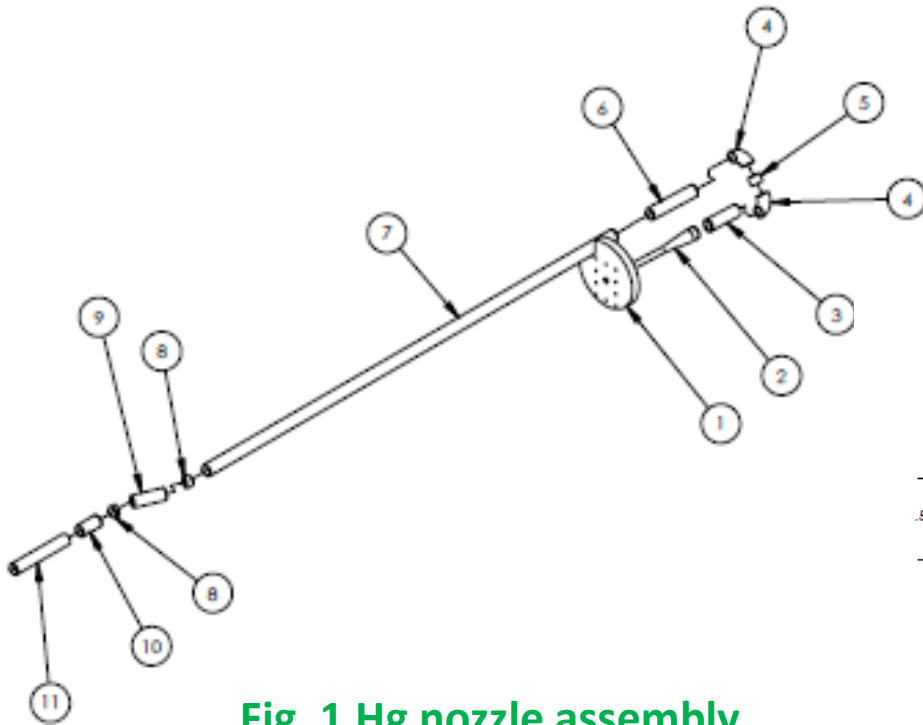


Fig. 1 Hg nozzle assembly

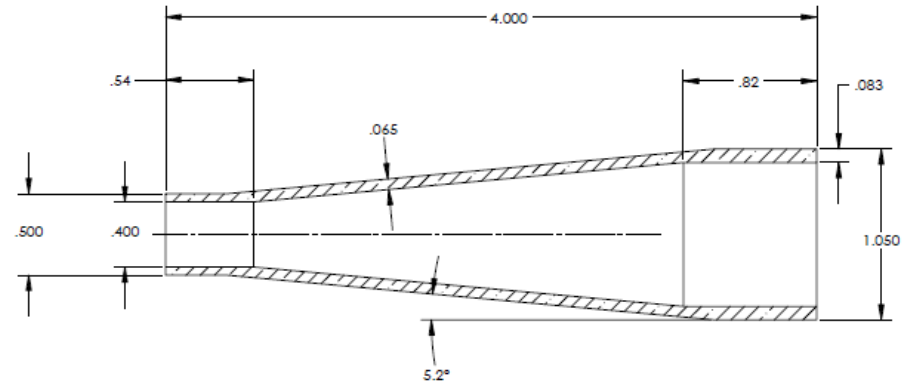


Fig. 2 Dimensions of item 2 (unit: inch)

Location of interests: welded-joint between items 2 and 3;
item 2: Ti-6Al-4V; item 3: Ti Grade 2.

Surface Topology of the Weld Bead

- To understand the effect of bead geometry on the turbulence level of the flow at pipe exit.
 - Flat surface
 - Whole azimuthal weld with semi-circle cross section
 - Major radius = 0.884"
 - Minor radius = 1/16"
 - Partial azimuthal weld with semi-circle cross section
 - only has 30° of azimuth from -15° to +15° relative to “up”

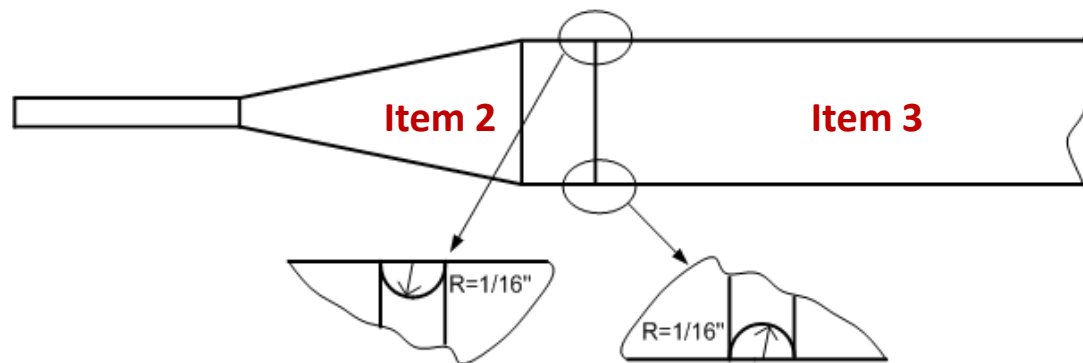
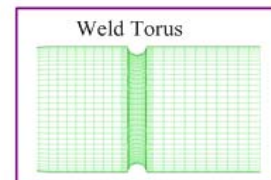
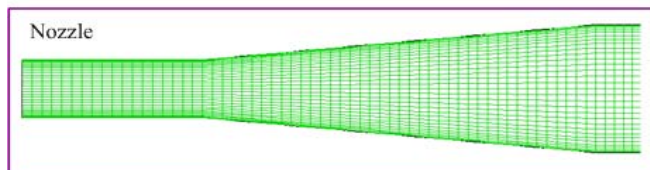
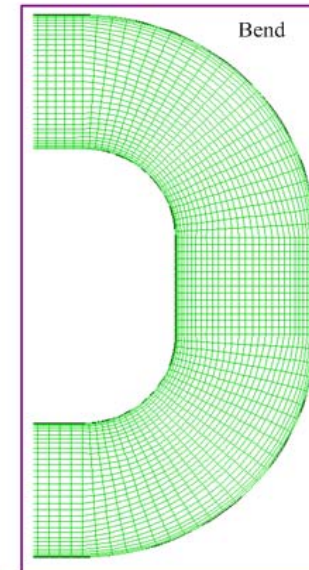
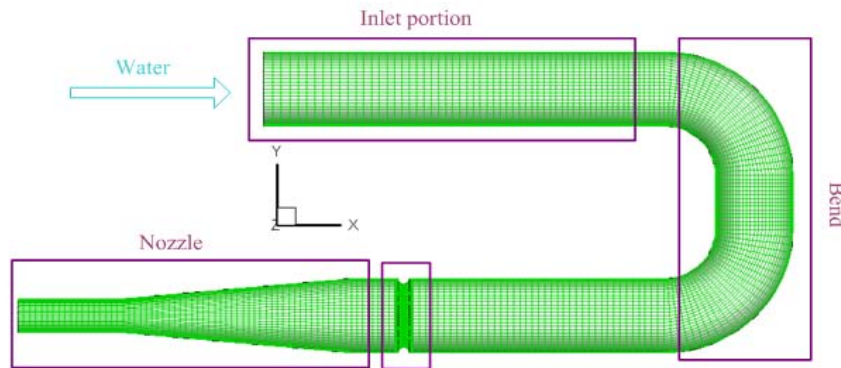
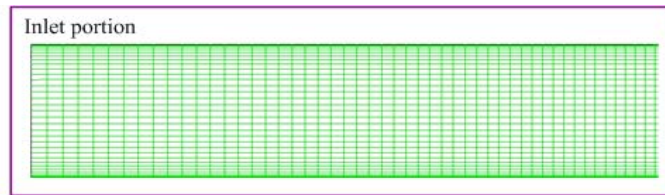


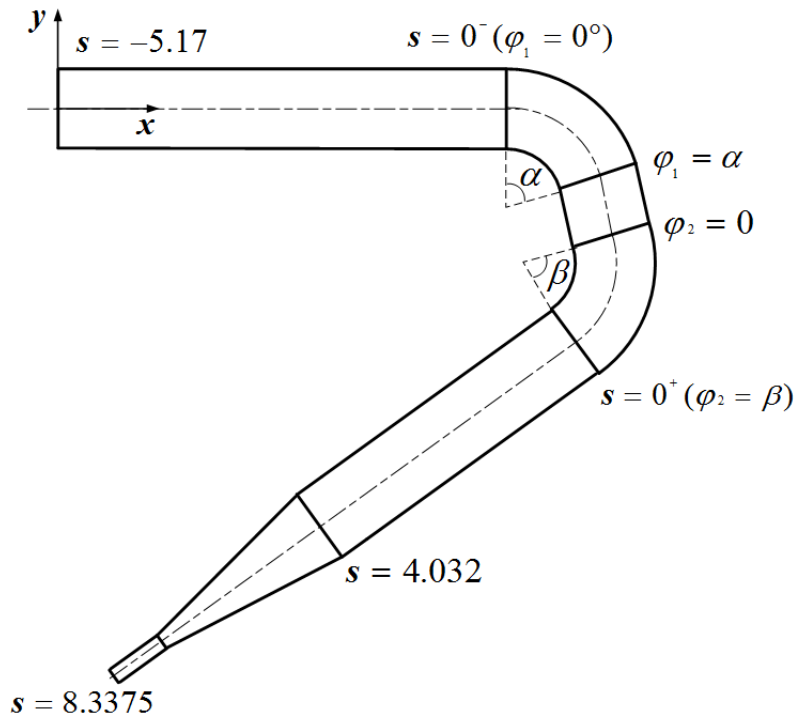
Fig. 3 The semi-circle topology of the Weld

Mesh for the Pipe with Whole Weld

Pipes	Mesh No. (EWT)
Pipe with whole weld	mesh0: $n_{\theta}=32$, $n_r=65$, $n_z=260$, $n_{tot}=5.3248e5$
	mesh1: $n_{\theta}=40$, $n_r=77$, $n_z=274$, $n_{tot}=8.3296e5$
	mesh2: $n_{\theta}=48$, $n_r=90$, $n_z=294$, $n_{tot}=1.255968e6$



Velocity Line Plots for Pipe With Whole Weld



$$U^* = \frac{u}{U_b}$$

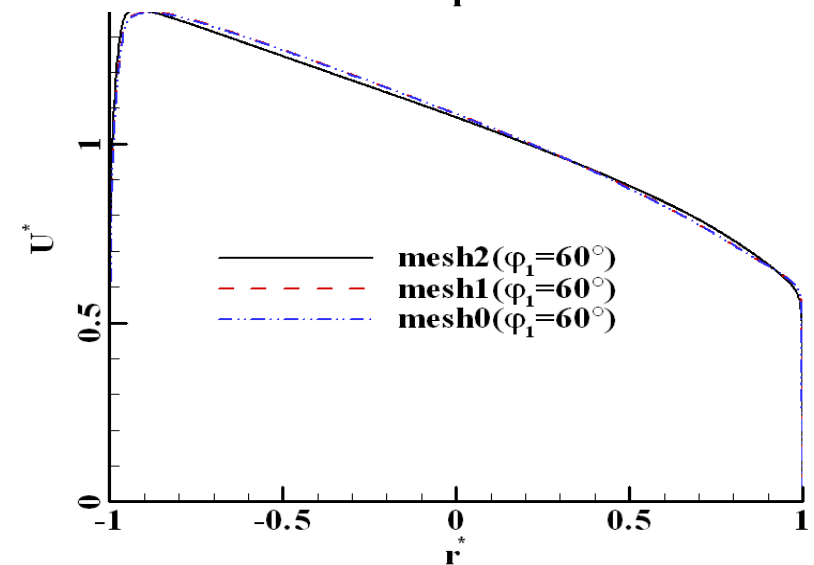
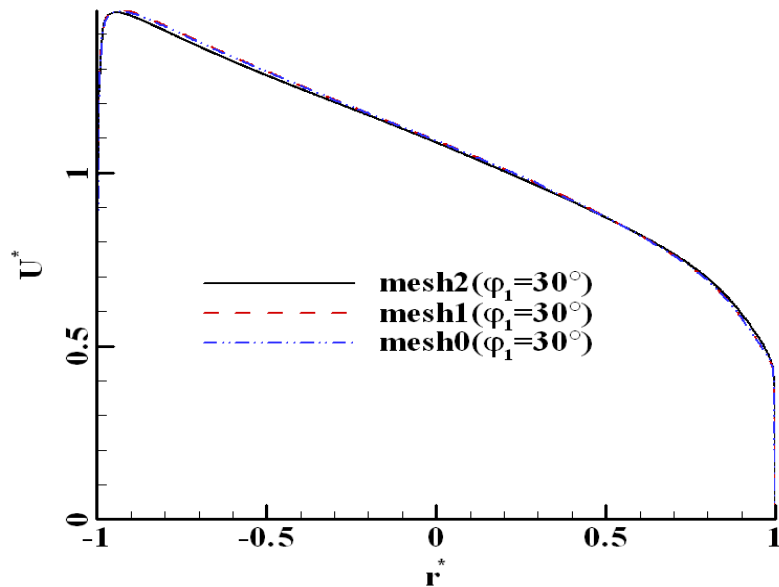
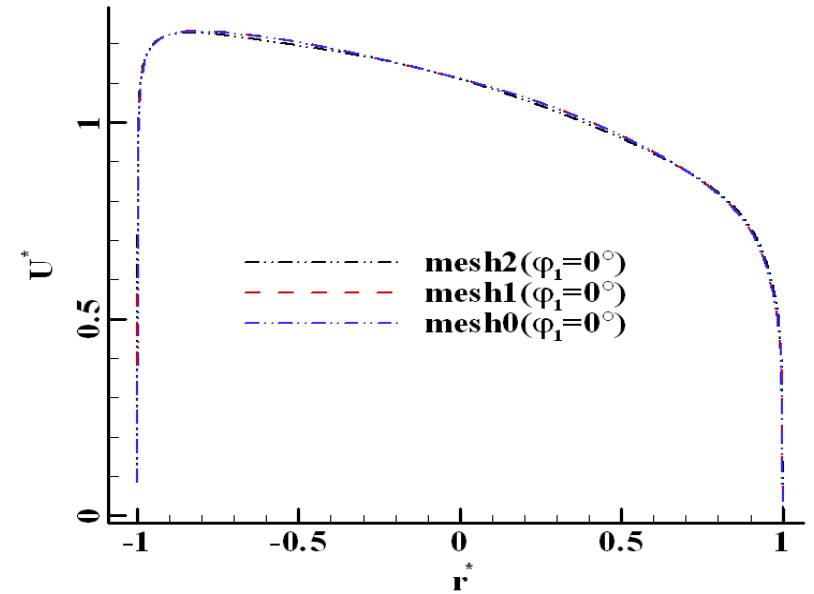
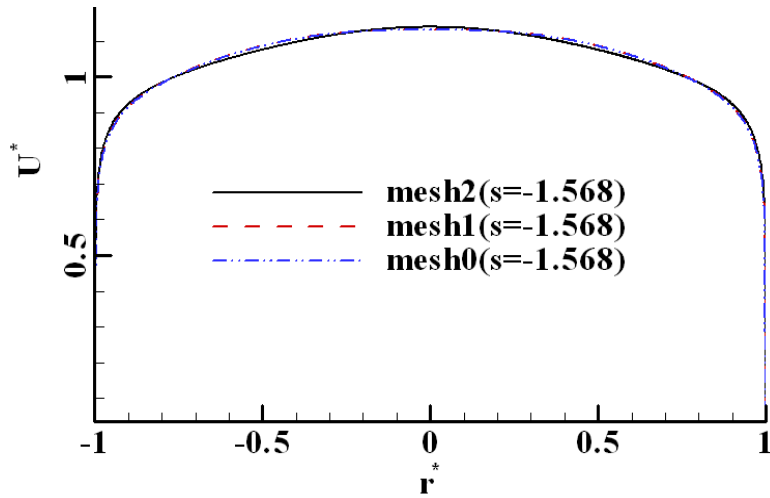
$$\text{where } U_b \equiv \frac{\int u(r, \theta) r dr d\theta}{\int r dr d\theta}$$

Plots of U^* along the axial direction are chosen at $s = -1.568$, $s = 3.36$, $s = 4.032$, $\varphi_{1,2} = 0^\circ$, $\varphi_{1,2} = 30^\circ$, $\varphi_{1,2} = 60^\circ$, $\varphi_{1,2} = 90^\circ$, $s = 6.89$, and $s = 8.3375$.

Portions along the positive flow direction

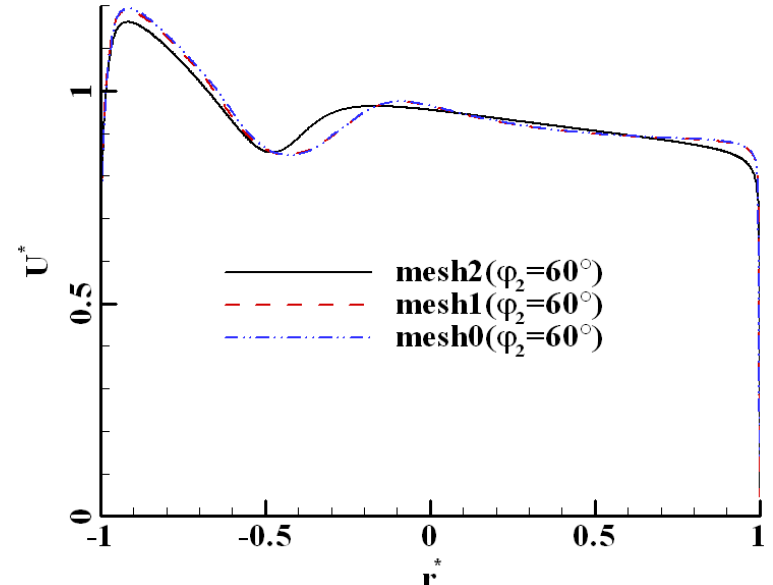
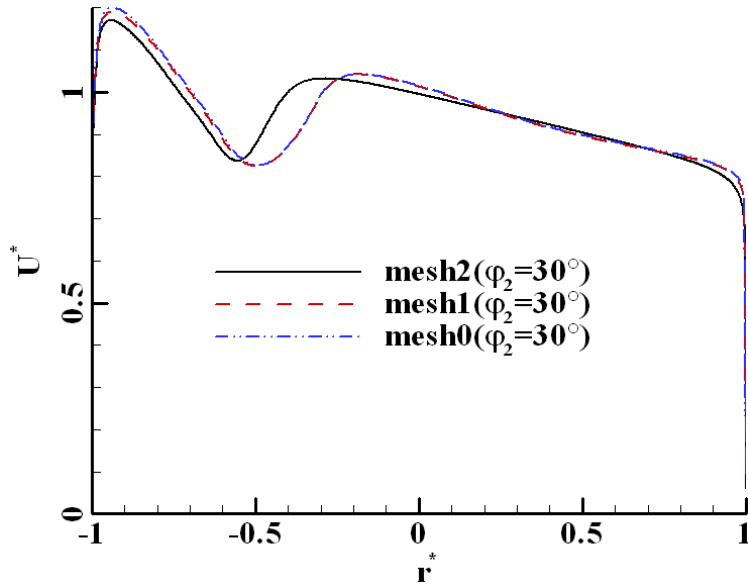
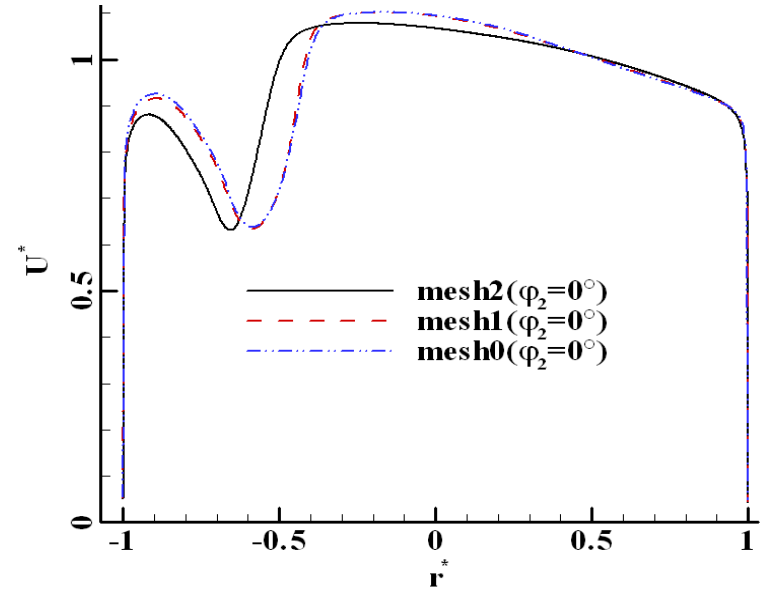
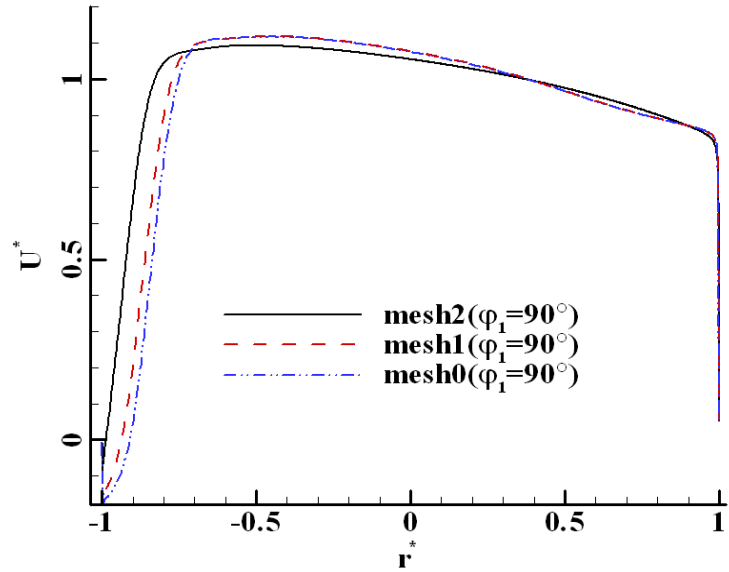
Velocity Line Plots for Pipe With Whole Weld

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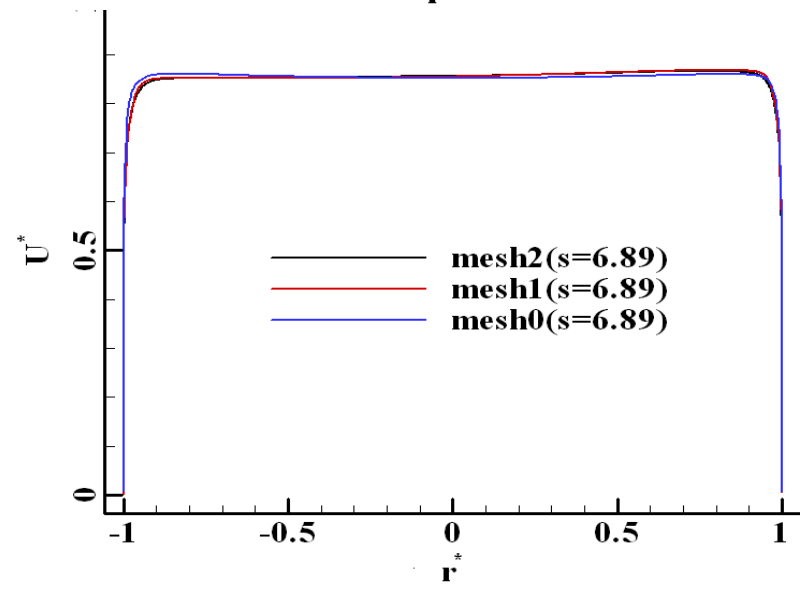
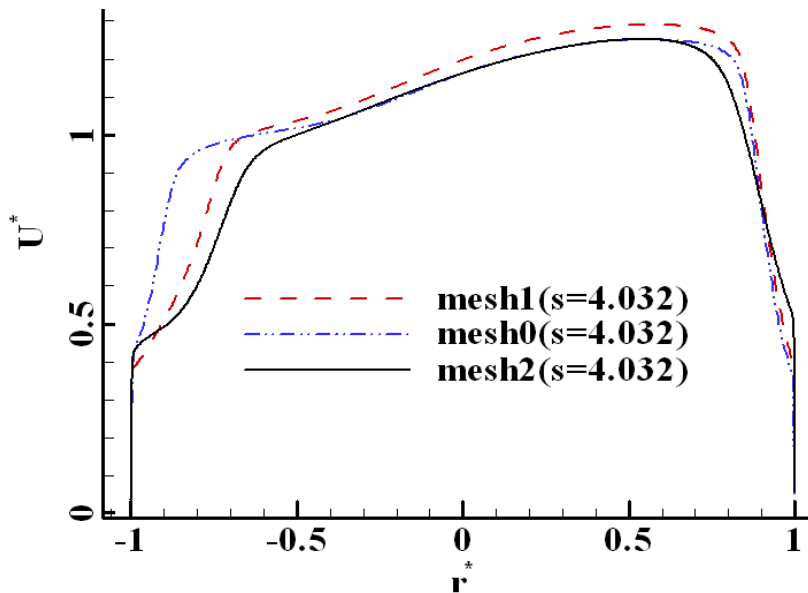
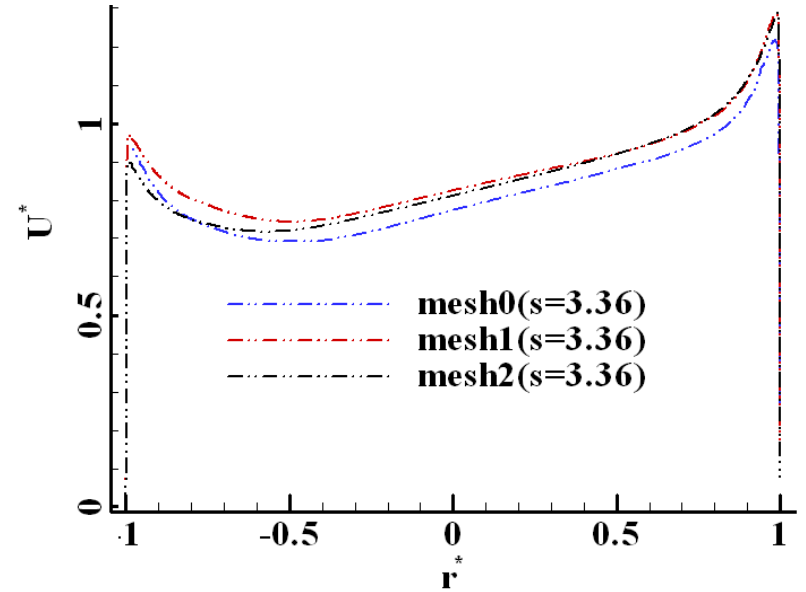
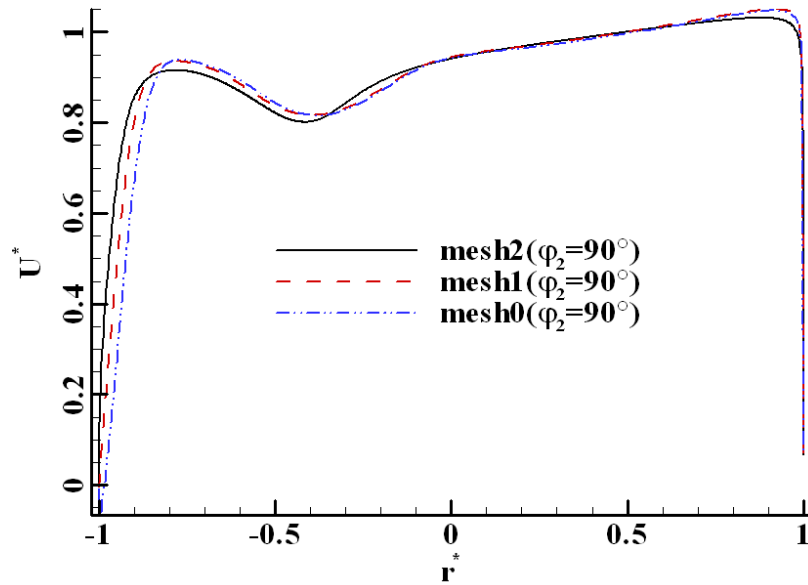
Velocity Line Plots for Pipe With Whole Weld

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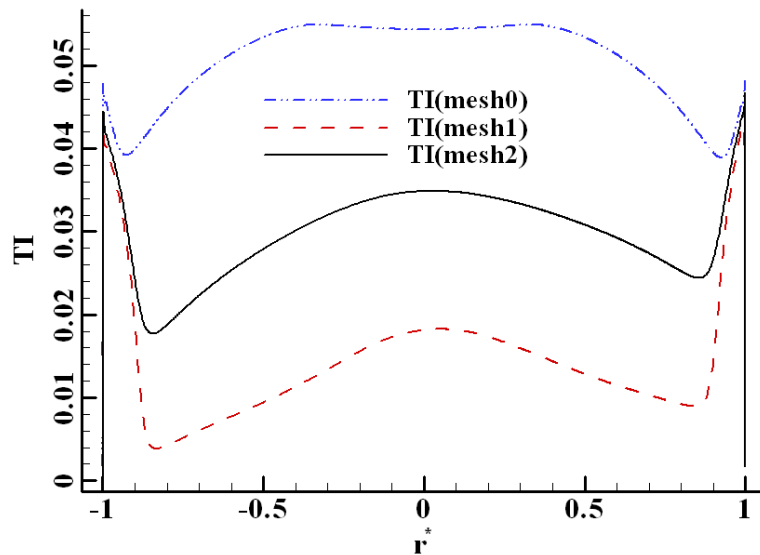
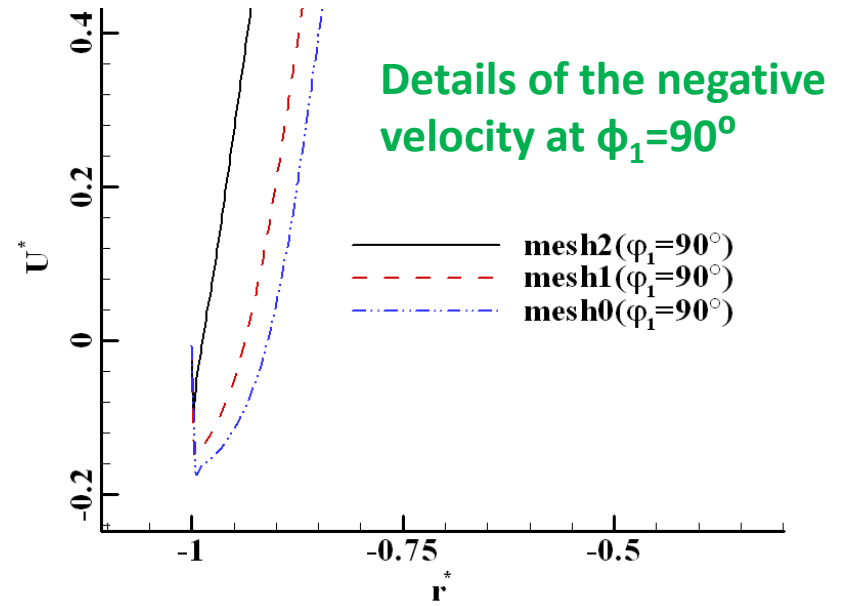
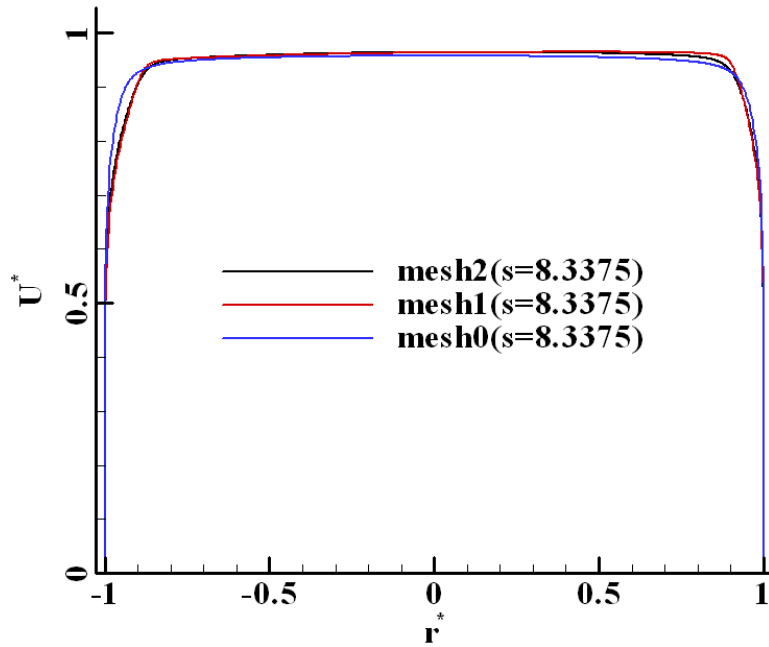
Velocity Line Plots for Pipe With Whole Weld

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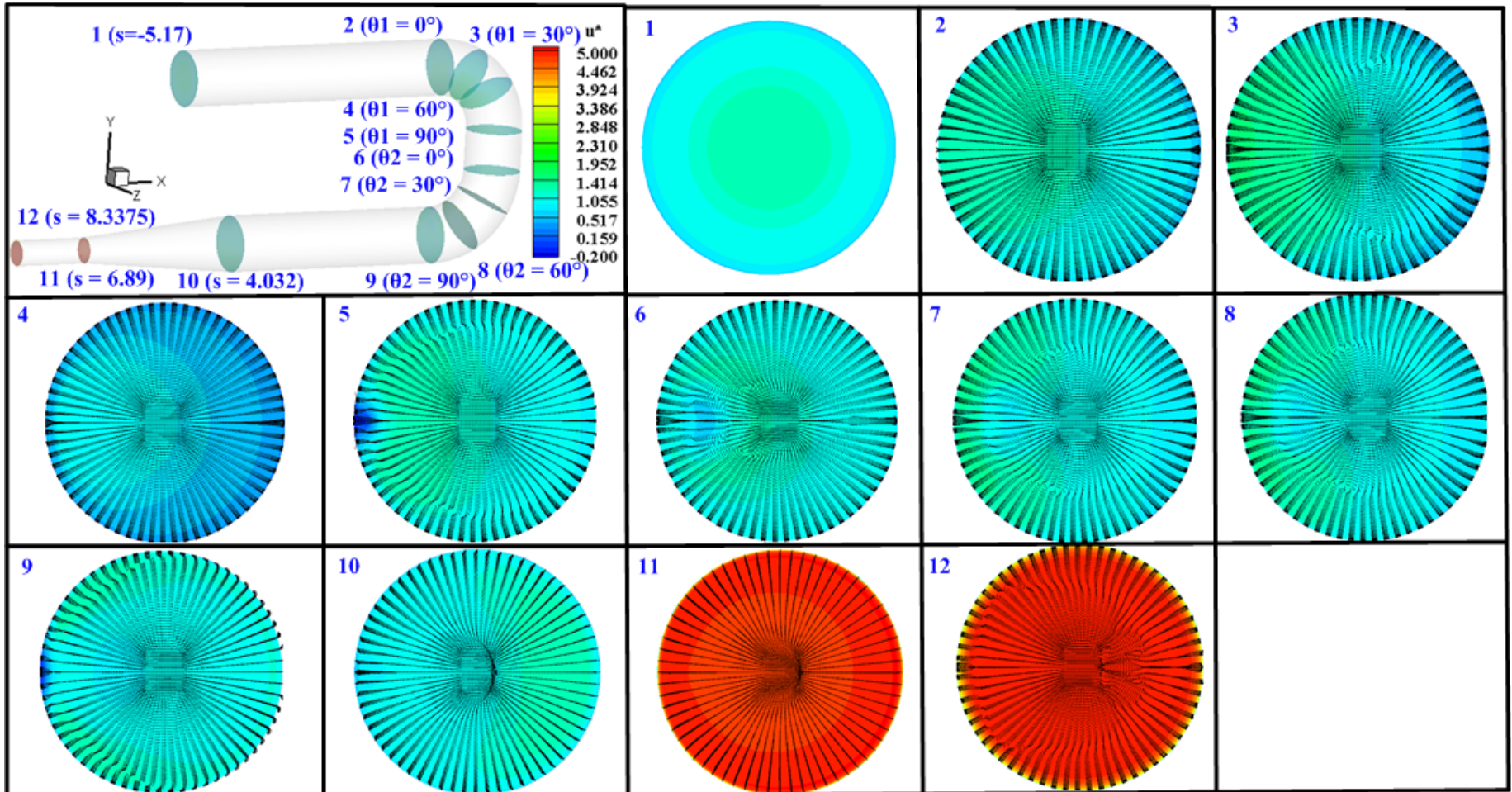


Velocity Line Plots for Pipe With Whole Weld

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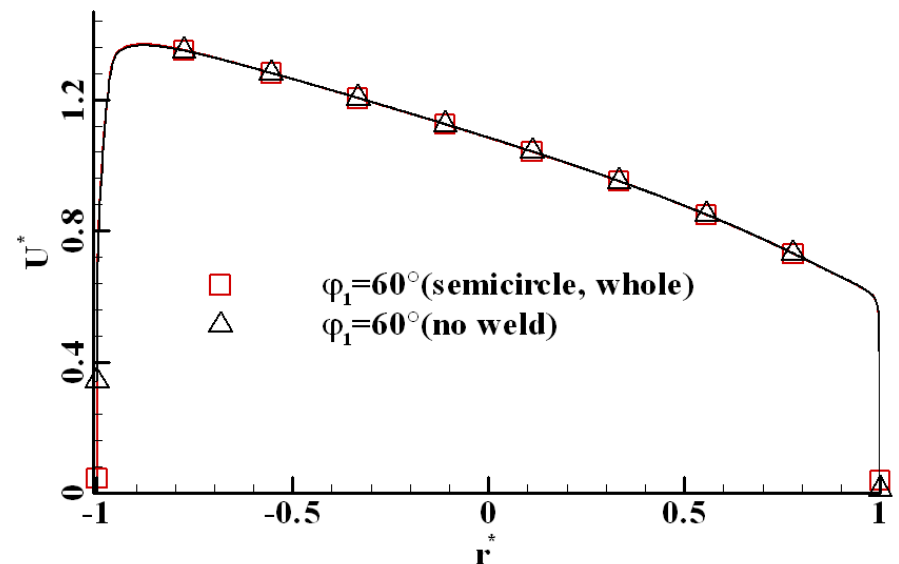
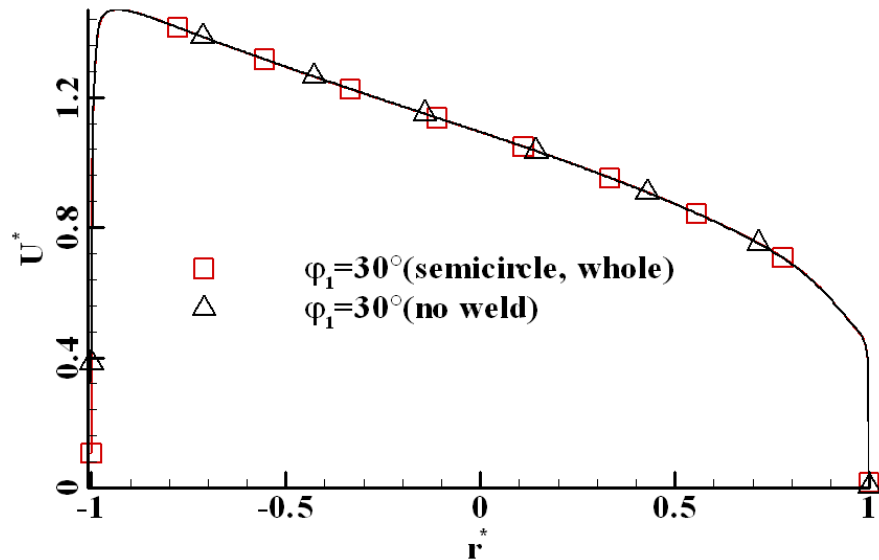
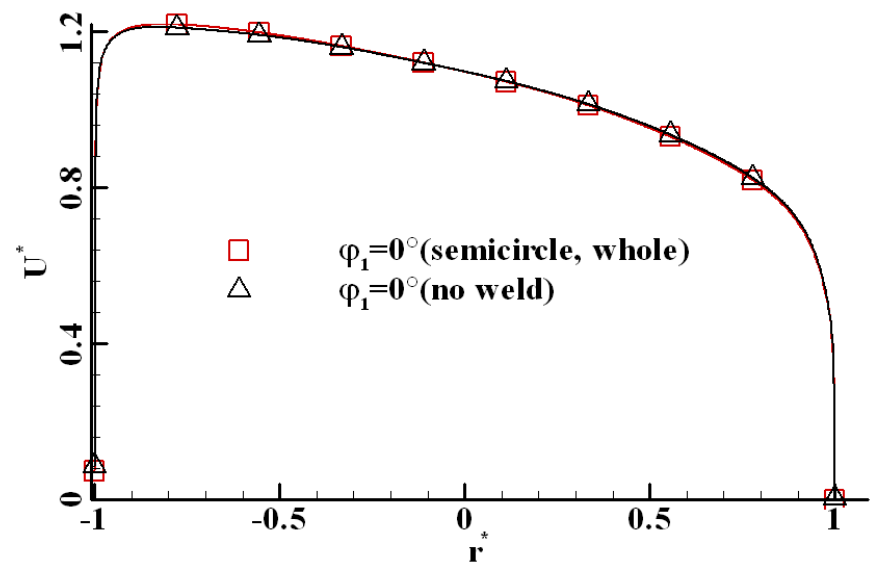
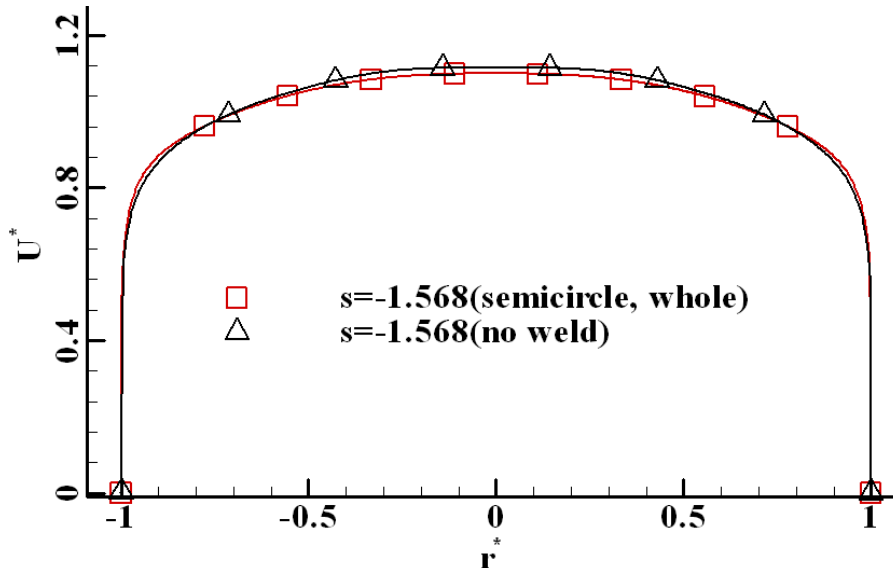


Velocity Contours for Pipe Without A Weld



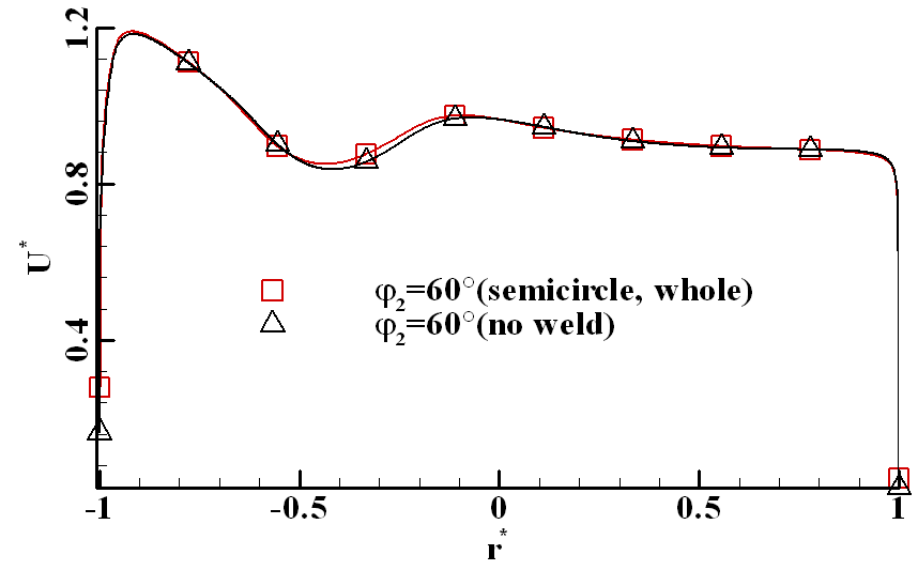
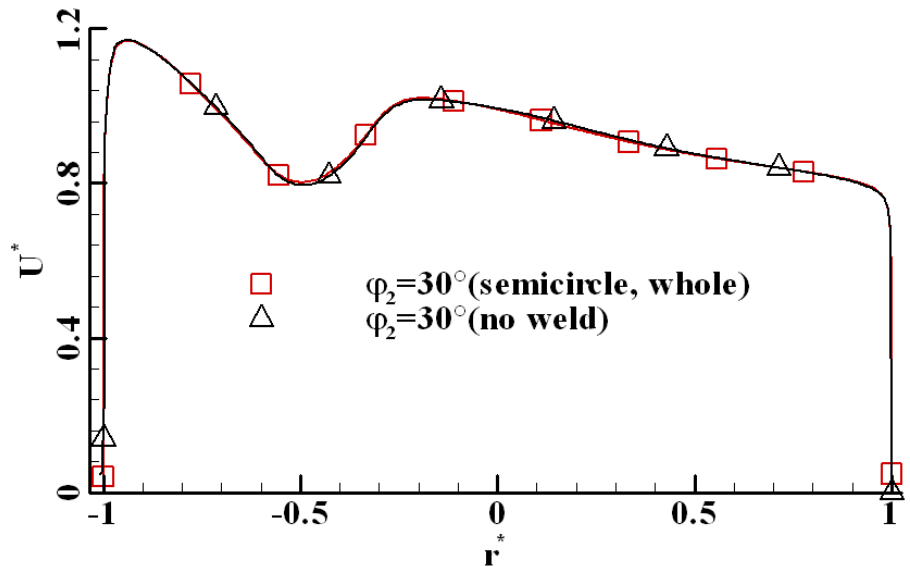
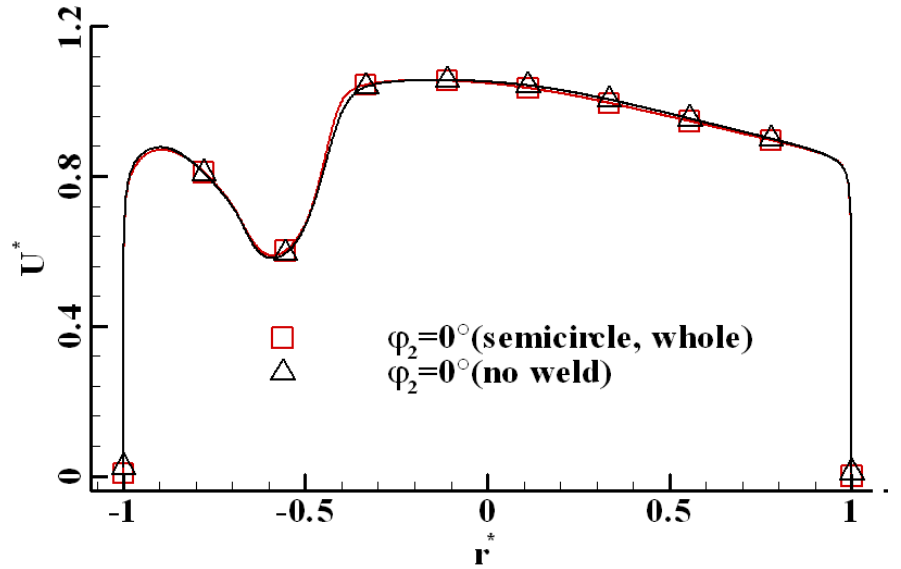
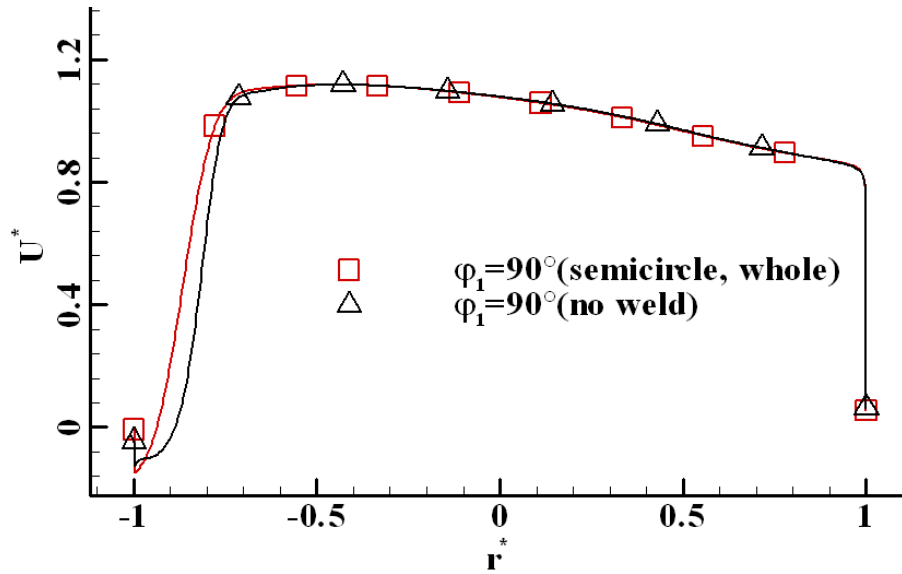
Mercury Flow (Mesh: $n_\theta=34$, $n_r=68$, $n_z=330$, $n_{tot}=7.5174e5$)

Comparisons Between Pipes W/O Weld



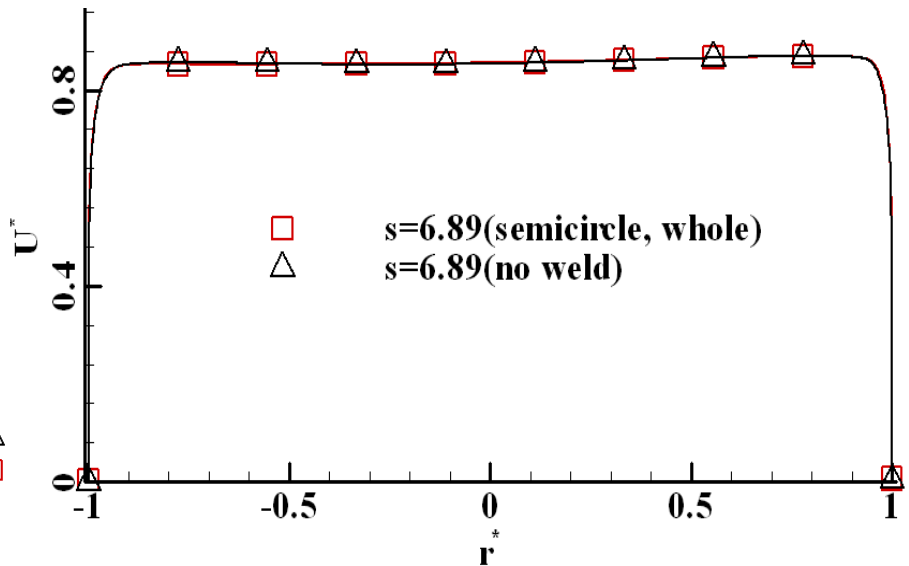
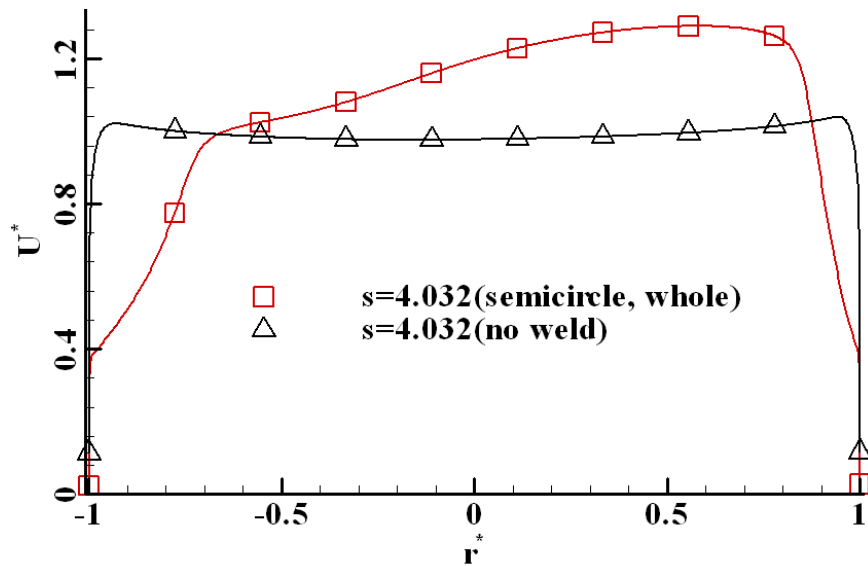
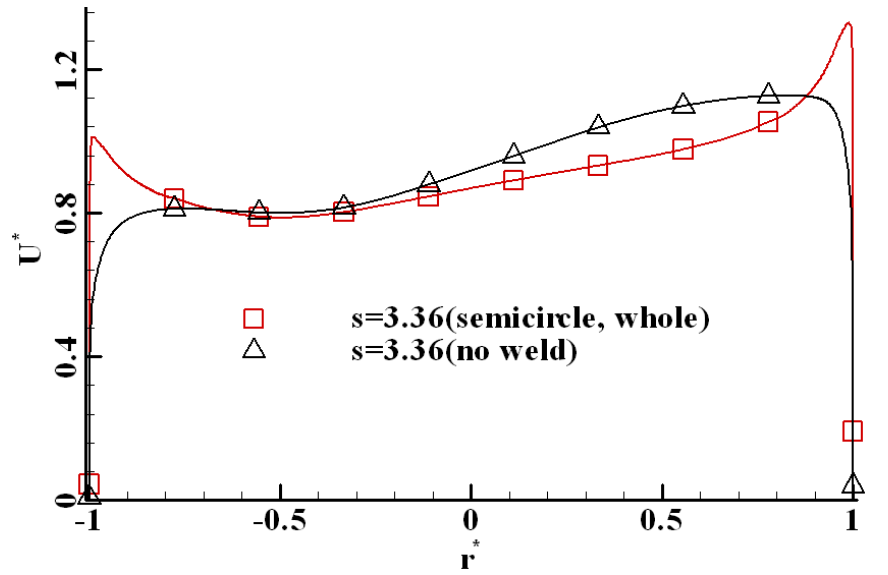
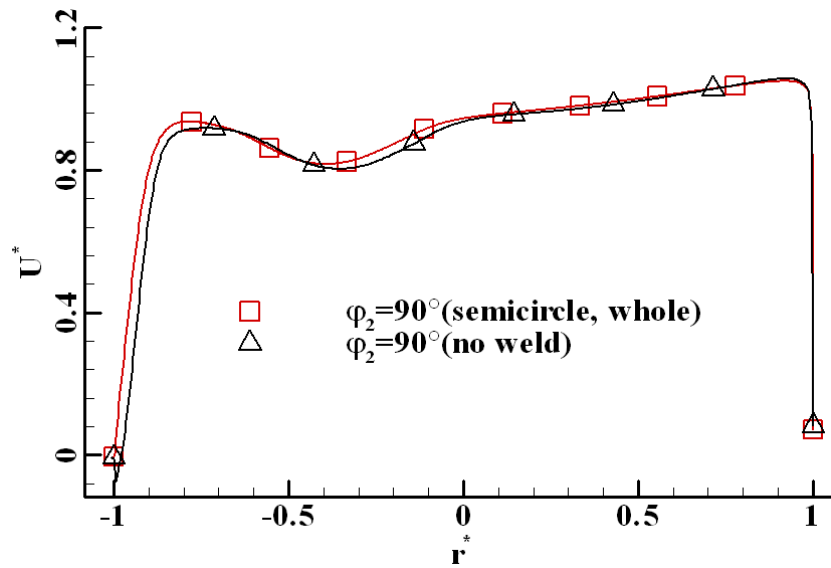
Comparisons Between Pipes W/O Weld

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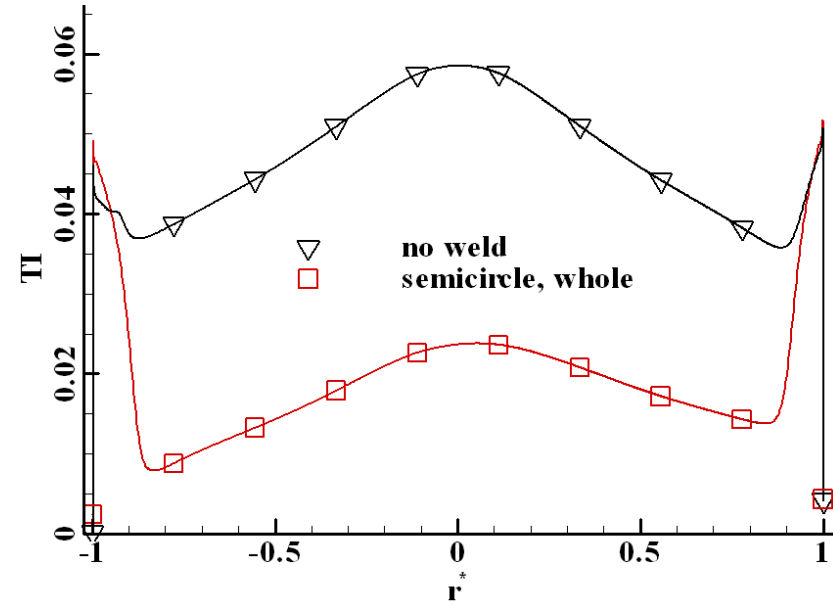
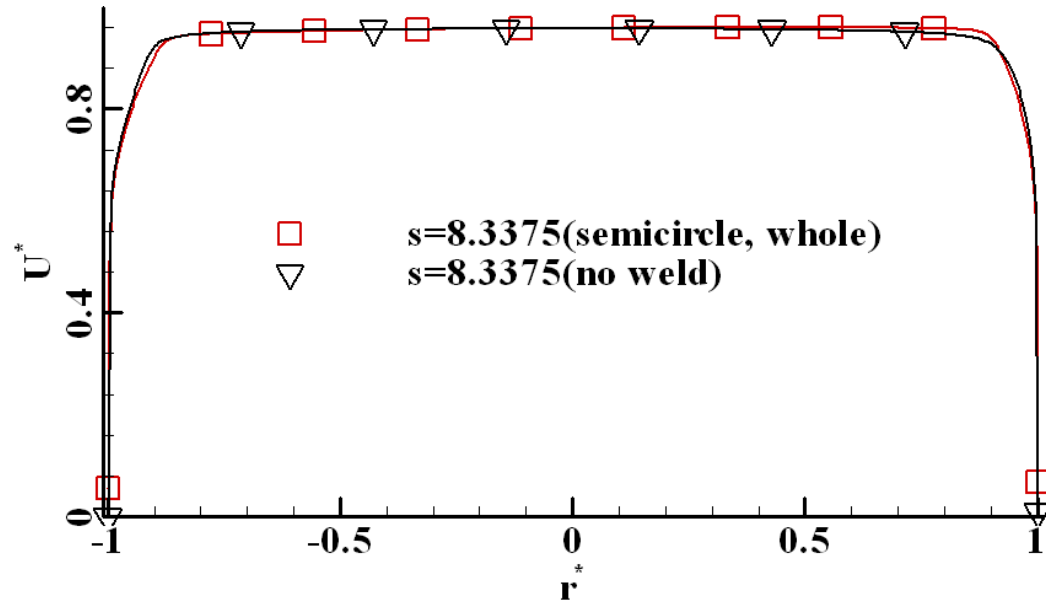
Comparisons Between Pipes W/O Weld

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Comparisons Between Pipes W/O Weld

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Summery

Mesh improvements:

- (1) Denser mesh for the 1st half-bend;
- (2) The mesh1 is good at the 2nd half-bend as well the weld;
- (3) Denser mesh need near the wall region of the taper and the central region is according to the mesh1.

Future plans:

- (1) Collect the size information on the partial azimuthal weld;
- (2) Do the mesh and simulation for partial weld case based on the experience of whole weld case;